Mixed assembly line balancing method in scenarios with different mix of products

Balanceamento de linha de montagem mista em cenários com distintos mix de produtos

Gustavo Reginato¹ Michel José Anzanello¹ Alessandro Kahmann¹ Lucas Schmidt¹



Abstract: A mixed-model assembly line can manufacture different products in the same assembly line, providing flexible production according to demand seasonal behavior. This article proposes a heuristic that aims to balance production lines subjected to several product models in order to attenuate capacity restrictions in workstations and increase the balancing efficiency. The proposed approach was applied to a mixed assembly line composed of seven product models. The results were considered satisfactory when assessed in terms of production capacity, manufacturing cycle time, and assembly line balancing.

Keywords: Mixed-model assembly line; Line balance; Capacity; RPW.

Resumo: Linhas de montagem mista combinam a fabricação de diferentes modelos de produtos em uma única linha de montagem, proporcionando flexibilidade de produção de acordo com a sazonalidade de vendas, evitando a baixa utilização dos ativos. Este artigo propõe uma heurística para balanceamento em linhas de produção sujeitas a distintos mix de produtos com vistas a atenuar as restrições de capacidade nas estações de trabalho e aumentar a eficiência de balanceamento. A abordagem proposta foi aplicada em uma linha de montagem mista com 7 modelos de produtos. Os resultados foram considerados satisfatórios, segundo avaliação de especialistas, quando avaliados em termos de capacidade produtiva, ciclo de fabricação e balanceamento de linha.

Palavras-chave: Linha de montagem mista; Balanceamento; Capacidade; RPW.

1 Introduction

Recent trends in customer demand for customized products encouraged the implementation of mixed assembly lines in many industrial environments (Mendes et al., 2005). Mixed lines can produce more than one kind of product in the same assembly line (AL) (Becker & Scholl, 2006), and different sales cycles may be combined to avoid low asset utilization when low sale of a specific product occurs (Leone & Rahn, 2004). However, in order to mixed arrangements to become viable in high competitive markets, assembly lines designers seek to increase the efficiency by maximizing the income rate and minimizing operating costs. Therefore, the assembly lines project an issue of great industrial interest (Rekiek et al., 2002a).

Aspects of balancing, layout and requested product mix affect the performance of a joint assembly line. The product mix is the quantity of each product being manufactured by AL. However, the lack of parts, machinery and equipment unavailability and non-conformities parts, among others, restrict the production of certain models in certain periods. In such way, changes in mix production are required to ensure that available resources are used. Such utilization, however, typically proves difficult to be carried out as the capacity constraints, imposed by balancing, limit the production rate. Thus, whether AL have conditions to adapt themselves to different product mix without affecting the productive capacity, the use of available resources can be maintained.

This paper suggests a method for mixed AL balancing scenarios subject to change in the product mix, making the AL able to meet the total production demand for the period independent of the produced model. That balancing is operated by an AL mixed moving target balancing heuristic, where tasks are

Received Nov. 14, 2014 - Accepted May 5, 2015

Financial support: None.

¹ Departamento de Engenharia de Produção e Transportes, Universidade Federal do Rio Grande do Sul – UFRGS, CEP 90040-060, Porto Alegre, RS, Brazil, e-mail: reginato 205@yahoo.com.br; anzanello@producao.ufrgs.br; alessandro.kahmann@ufrgs.br; lucasximiti@hotmail.com

allocated to workstations respecting three constraints: (i) meet the equivalent precedence relation from precedence diagram; (ii) allocate tasks to a workstation until the total station weighted average time does not exceed the moving target, and (iii) allocate tasks to a workstation in a way the total time does not exceed the station cycle time. The proposed method was applied in a company presenting a mixed AL that produces 7 different models. The method increased the production capacity by 35% (meeting the required demand for the AL), reduced the products crossing time in AL and improved line efficiency and balancing due to a better distribution of tasks.

This paper is divided into five sections. Section 2 presents the literature review, detailing the assembly line types, its balancing and applicable solutions. Section 3 presents the method stages, and its application in the production environment is in Section 4. Section 5 brings the conclusions.

2 Theoretical background

2.1 Assembly lines

An AL consists of a production arrangement formed by workstations typically distributed over a movement system. The product is sequentially released from station to station, suffering changes until it reaches the final assembly station (Gerhardt, 2005; Becker & Scholl, 2006; Kriengkorakot & Pianthong, 2007).

The assembly lines that produce identical products are call single-model line, or one-model line. When there are differences in the products, two classifications arise. The first is the multi-model line or multi-line model, which shows significant differences in production processes, and different products are manufactured in larger batches than a unit to minimize the setup impacts. The second classification is known as mixed-model line or mixed line, which is apply when there is similarity of productive process and there is no setup for process adjustment. This makes it possible to launch the products in the line in units randomly (Smiderle et al., 1997; Becker & Scholl, 2006). For each model, different processing times are required, so the amount of work at the same operator in the same workstation is uneven. Cases which operator ends the job before the next cycle or not ends the job within the cycle time make AL unbalanced and efficiency is reduced (Sarker & Pan, 1998). Even so, for Askin & Standridge (1993) apud Souza et al. (2003), this production system tends to be one of the most efficient, but requires reliable process and it with low variability in processing time of the workstations (in the practical application context of the methodology proposed, low variability refers to a difference less than 30% of the time variation between models). Figure 1 illustrates the above definitions, where the geometry of the figures refers to different products.

In the AL design, the main issues to deal are: (i) define the cycle time; (ii) determine the number of workstations; (iii) balance the AL; and (iv) determine the models production order. Another concern of AL design is to minimize the lead time (Sarker & Pan, 1998), which means reducing the gap of time between the initiation and completion of the product AL (Marlin, 1986). As shorter is the lead time, greater the potential sale of products (Öztürk et al., 2006). Another premise for the proper functioning of ALs is time the station (S) does not exceed the cycle time, according to Equation 1.

$$\max t_k \le \max S_j \le T_c \le \frac{1}{D} \tag{1}$$

where S_j is the total time of station j (j=1,...,W), representing the sum of performing times tasks allocated to each station in time units; t_k is the processing time of the k^{th} task on time unit; k identifies the task such that k=1,...,N; T_c is the time cycle and D is the product demand rate.

The cycle time (T_c) is the time when a product is released from station to station, defined by the Equation 2.

$$T_c = \frac{available time in \ period \ p}{demand \ in \ period \ p} \tag{2}$$

The number of workstations needed to meet demand varies with the AL settings and restrictions. According Peinado and Graeml (2007), the minimum number of workstations for ALs counting with only one operator can be estimated by Equation 3.

$$Number of workstations = \frac{\sum individual \ tasks \ times}{T_o}$$
 (3)

To balance the tasks, it is essential to know precedence diagram (Figure 2). This diagram shows the order of tasks execution, respecting technological requirements or item production characteristics (Boysen et al., 2007).

In precedence diagram, the numbers within the circles represent tasks, while the arrows joining the circles show the precedence relation. The sum of

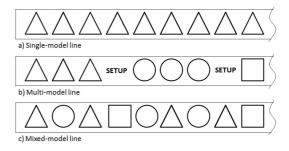


Figure 1. Assembly line types. Source: Adapted from Becker & Scholl (2006).

Figure 2. Exemple of precedence diagram. Source: Adapted from Becker & Scholl (2006).

the tasks times assigned to a station is known as station time.

Each task time can be achieved by chrono-analyse among other methods. The chrono-analyse is a way of measuring the work by means of statistical methods, allowing calculating the standard time. The standard time includes a series of factors, such as operator speed, personal needs and relieving fatigue, among others; such factors can be found in specialized literature in the area. The standard time of performing tasks can also be determined by predetermined times (Peinado & Graeml, 2007).

The task processing times are also used to determine the production capability of a AL. Capacity is the maximum amount of items produced in the AL in a given time interval; to determine the production capacity, it is necessary to identify the bottlenecks in the AL. Therefore, the production capacity is calculated on the basis of working time available and the time of the bottleneck station, as in Equation 4 (Peinado & Graeml, 2007).

$$Production \, capacity = \frac{Available \, time \, in \, period \, p}{Time \, of \, the \, bottleck \, station} \tag{4}$$

2.2 Assembly line balancing

The Assembly Line Balance (ALB) is known as the classic problem of AL balancing, consisting in the allocation of tasks on a workstation in a way that downtime is minimized and the precedence constraints are met (Rekiek et al., 2002b; Becker & Scholl, 2006; Kriengkorakot & Pianthong, 2007). The ALB allows achieve the best use of available resources so that satisfactory production rates are reached at a minimum cost (Wild, 1972, apud Praça, 1996). The balancing is necessary when there are process changes, such as adding or deleting tasks, change of components, changes in processing time (Farnes & Pereira, 2006) and also in the implementation of new processes.

According to Becker & Scholl, 2006, the assembly line balancing problem can be classified into four categories, as shown in Figure 3. This classification is detailed as follows:

(i) DSM – Deterministic single model: This model is considered to assembly lines with only one product model, where the tasks times are known deterministically, with little tasks timing variation (as a result of easy execution and also the operators motivation) (Rekiek et al., 2002a; Becker & Scholl, 2006). Certain efficiency criteria should be otimizated, as idle time station and line efficiency, among others; (ii) SSM – Stocastic single model: In this category, the execution times of activities have resulting human behavior variability, inability of operators, lack of motivation, complex processes and equipment with low reliability, among others; (iii) DMM - Deterministic multi/mixed model: The formulation of the DMM problems considers deterministic tasks times, but with the presence of different products manufactured on the same assembly line. In this context, aspects associated with sequencing, release rate and batch sizes become important when compared to single model lines; and (iv) SMM - Stocastic multi/ mixed model: the tasks times are probabilistic. Learning impacts, skill, tasks delineation and tasks time variation are considered in this approach (Becker & Scholl, 2006).

Another important classification split the line balancing problems into two categories: (*i*) simple assembly line balancing problems, indicating that no restrictions are relaxed; and (*ii*) generic balancing problems, which fit the line balancing problems

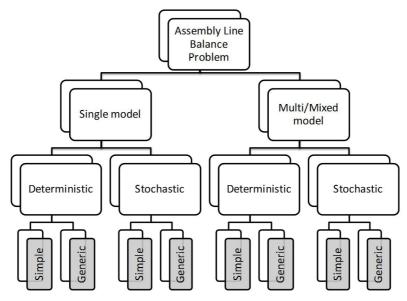


Figure 3. AL balancing problem classification. Source: Adapted from Ghosh & Gagnon (1991).

that aim to solve problems with additional features (Fernandes et al., 2008).

According Van Zante-de Forkket & De Kok (1997) apud Gerhardt (2005), the fundamental difference between a single model line balancing problem for a multi-model is the precedence diagram. Such, many authors, to develop methods to solve multi-model line balancing problems, transform the problem into single model. Two methods can be used: (*i*) equivalent precedence diagram, and (*ii*) adjusting the processing taks time (Gerhardt, 2005).

(i) Equivalent precedence diagramming method: Thomopoulos (1970) apud Gerhardt (2005) assumed that in a mixed line, there are several common tasks to the various models produced and, consequently, a similar set of precedence relationships. Then, the precedence diagrams combination of each individual model can be made by joining the nodes and precedence relations of the respective diagrams for each model, as exemplified by the Figures 4 and 5.

According to van Zante-de Fokkert & de Kok (1997), the balance of AL multi-model based on equivalent precedence diagramming method can be compared to balancing single AL model. However, the allocation of tasks to workstations is performed based on the total shift time duration and not in cycle time, which is used as the basis to balancing AL single model.

(ii) Setting task processing time method: In this method, the processing time is determined by the weighted average of k^{th} task common to

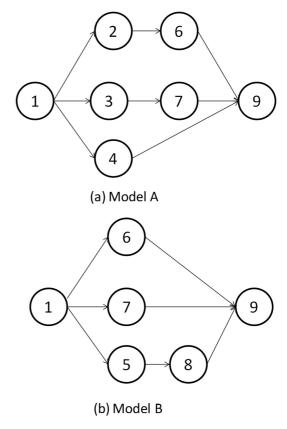


Figure 4. Precedence diagram to the model A (a) and model B (b). Source: Adapted from Gerhardt (2005).

different models, according to the Equation 5 (van Zante-de Fokkert & de Kok, 1997),

$$\overline{t_k} = \sum_{m=1}^{M} p d_m t_{k,m} \tag{5}$$

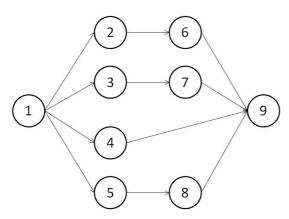


Figure 5. Precedence diagram equivalent models A and B. Source: Adapted from Gerhardt (2005).

where pd_m is the proportion of the model m ahead the other models produced in AL, t_{km} represents the processing time for the k^{th} common task for different models and $\overline{t_k}$ represents the processing time weighted average of the k^{th} common task to different models. An advantage of this method is that it is based on the cycle time, which makes more sense for organizing tasks in a AL (instead using it total shift time). As disadvantages, the method does not determine the sequence in which the models will be produced and does not consider different diagrams of precedence. As such, it is recommended for balancing derivatives models of a basic model, where the tasks have a processing time similar to the basic model (van Zante-de Fokkert & de Kok, 1997).

In turn, Becker & Scholl (2006) emphasizes that both methods (i) and (ii) exhibit inefficiencies resulting from variations in stations processing times, which depend on the production model. Such inconsistencies may generate work overload or idle for operators.

Traditionally, two indicators are used to evaluate balancing quality AL (Driscoll & Thilakawardana, 2001): Balance Delay, which represents a percentage of time that the AL remains idle; and Smoothness Index (softness Index), which measures the difference between the maximum total working time between the stations and the total times of the other work stations (Gerhardt, 2005).

Driscoll & Thilakawardana (2001) introduce alternative ways to evaluate the balance of the AL. The Line efficiency (LE) quantifies the use of AL and has aspects of economic evaluation; Balancing efficiency (BE) quantifies the tasks allocation quality for the workstations, which may consequently cause an increase in the production rate. Both indicators are dimensionless and represented using a scale from

0 to 100%, where 100% represents the best result. They are calculated according to Equations 6 and 7 respectively.

$$LE = \frac{\sum_{k=1}^{N} t_k}{W \times T_c} \times 100 \tag{6}$$

$$BE = \left[1 - \frac{\sum_{j=1}^{W} \left|S_{j} - S_{av}\right|}{W \times S_{av}}\right] \times 100 \tag{7}$$

where S_{av} is the average time of workstations and W the number of workstations.

2.3 Soluctions for ALB

Considering that the ALB problem may be shown on NP-hard combinatorial optimization category, several researches have developed computational or heuristic approaches (Ghosh & Gagnon, 1991). Ghosh & Gagnon (1991) classify methods for balancing ALB as follows: (i) Rank and Assign Methods: In these methods, tasks are sorted based on criteria or rules of priority and assigned to stations relying on an order that does not violate the relationship of precedence constraints and cycle time; (ii) Tree Search Methods: These methods are essentially integer programming relying on the Branch & Bound method. Approaches in this category can also be termed as enumerative methods; (iii) Random Sampling Methods: These methods randomly assign tasks to workstations in view of the precedence constraint and cycle time; and (iv) Other methods: aggregation methods (task elements are grouped into composite tasks), Successive Approximation (a great algorithm is applied successively as a heuristic in a simpler version of the problem), and Learning Methods (based on the premise that the experience acquired minor problem solving is used to solve larger problems).

Cristo (2010), Ponnambalam et al. (1999) and Chow (1990) highlight the following heuristics to ALB troubleshooting: Rank positional weight, Kilbridge and Wester's method, Largest set ruler. The foundations of heuristics above are now displayed.

RPW-Rank Positional Weight: this method was introduced by Hegelson and Birnie in the 60s, having generated satisfactory and fast solutions according Boctor (1995) apud Praça (1996). Its operation consists in calculating the positional weight of each task according to the precedence diagram. The weight is the sum of the task time with the time tasks that predate it. In sequence, the positional weights should be arranged in descending order, and the tasks assigned to the workstations according to the order of the positional weight, respecting the

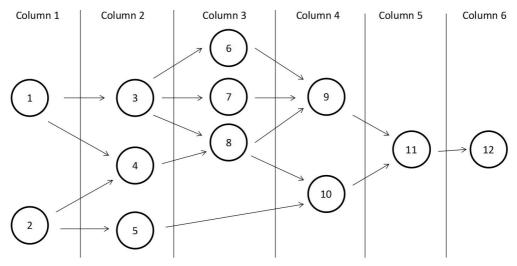


Figure 6. Precedence diagram divided in column by Kilbridge and Wester method. Source: Adapted from Gerhardt & Fogliatto (2004).

precedence constraints. Further details on the method can be found in Chow (1990).

- Kilbridge e Wester Method (KWM): This
 method selection work elements to describe
 the station according to the column Precedence
 Diagramming position as shown in Figure 6.
 In sequence, tasks are arranged in descending
 order of processing time. Finally, tasks are
 allocated to workstations in accordance with such
 order, thus ensuring that the largest elements
 are allocated first and increasing the chance of
 each station time get closer to the cycle time
 (Gerhardt & Fogliatto, 2004).
- Largest Candidate Rule (LCR): This heuristic
 allows obtaining results in less time than the
 positional weights method. Initially, one should
 list tasks in descending order of processing
 time; then the task should be assigned to the
 workstations according to the order of the list
 without violating any precedence constraint or
 exceed the cycle time (Praça, 1996).

3 Method

This section proposes a new balancing heuristics for mixed AL titled target mobile RPW (RPW-MVM), which relies on heuristics of RPW positional weights originally proposed by Helgeson & Birnie. Such proposition focuses on a production environment amenable to changes in product mix, which cause imbalances on the workstations and generate productive capacity constraints in AL, making it unable to meet the required production demand.

The heuristic allows the AL meets the production demands characterized by several product mix composition, without the need for interventions to balancing adjustment or sequencing of actions to launch the products. This requires that the time of each model on all workstations is less than the AL cycle time. In addition, the proposed heuristic innovates in the tasks distribution format to workstations, proposing a target mobile which aims to improve the tasks distribution between the stations compared to the original RPW. The proposed heuristic is now detailed.

3.1 RPW-MVM

The original RPW is fundamentally guided by a pre-established time cycle; therefore, it can be assumed that the amount limiting target of the allocable task to a given workstation is the cycle time, which is fixed. Thus, the tasks allocation to workstations may have an accumulated imbalance in the first workstation, which typically results in significant losses to the AL. It is proposed then a change in this target, which becomes mobile (and called Moving Target - MVM).

The MVM is calculated for each workstation and depends on the number of workstations to be balanced. It serves to improve the tasks distribution between the workstations not balanced according to the time of the not yet allocated tasks. Every changing of the station, the target is recalculated for each model (hence mobile), and then identified the condition that allows allocation of the remaining tasks of the product with longer not yet allocated operations. In other words, MVM allows for each workstation to exchange the entire contents of the working model under review to be distributed evenly among the remaining stations.

Figures 7 and 8 illustrate the RPW without target mobile and with moving target (MVM), respectively.

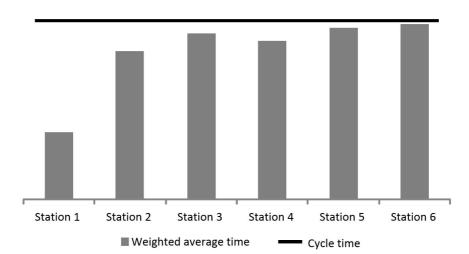


Figure 7. Balancing with RPW and without MVM heuristics. Source: The authors.

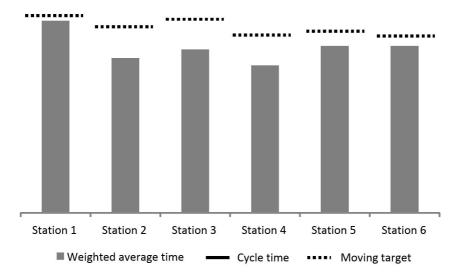


Figure 8. Balancing with RPW and MVM heuristics. Source: The authors.

The MVM yields better smoothness index for AL and, therefore, benefit and ergonomic productive character.

Following are presented the steps to perform the RPW-MVM.

Step 1: Set the diagram/equivalent precedence matrix of all models;

Step 2: Unlike the RPW in AL single model, the RPW-MVM is a balancing in a AL with more than one product model, where each model has its own tasks processing time. So for the average processing time for common tasks to the different models, is needed to define the each model proportion to be produced by the Equation 8

$$pd_m = \frac{d_m}{D} \tag{8}$$

where d_m is the product demand in the period p such that m=1,...,M; and D is the total demand for all models

for the period p. The products demand history or the production plan are reference sources for defining the product number of the model m.

Step 3: Calculate the cycle time (*Tc*) based on total production demand to be met by the Equation 2;

Step 4: As mentioned earlier, the RPW-MVM support in times of an equivalent product of mixed AL. Thus, for the tasks allocation in the RPW-MVM, use the Time Weighted Average $(\overline{t_k})$ and the weighted average total station time $(\overline{S_j})$, calculated using Equations 9 and 10, respectively.

$$\overline{t_k} = \sum_{m=1}^{M} p d_m t_{k,m} \tag{9}$$

$$\overline{S}_j = \sum_{k \in j} \overline{t_k} \tag{10}$$

where $t_{k,m}$ is the processing time of task k in the model m and pd_m is the proportion of model m.

Step 5: Calculate the *RPW* of each task by adding $\overline{t_k}$ to the processing times of all preceding tasks equivalent precedence diagram;

Step 6: Sort the tasks in descending order of *RPW*;

Step 7: Calculate the minimum number of workstations for balancing ALM (MinW) and then set the last workstation (W = MinW) based on the Equations 11 and 12, where CTT_m is the total workload the m model.

$$CTT_m = \sum_{k=1}^{N} t_{k,m} \tag{11}$$

$$\operatorname{Min} W = \frac{CTT_m}{T_c}, \ m = 1, \dots M$$
 (12)

Step 8: Set j = W;

Step 9: Calculate the moving target of the latest workstation for all models $(MVM_{j,m=1,...M})$. The MVM is required for each product model and should be recalculated every new balanced workstation during application of the RPW-MVM. The moving target the j^{th} workstation to the model m ($MVM_{j,m}$) is calculated by Equation 13 based on the not yet allocated workload residue divided by the total workstations still unbalanced for the m model. Equation 14 sets the total charge allocated at station j of the m model ($CTA_{j,m}$).

$$CTA_{j,m} = CTA_{j+1,m} + S_{j,m}$$
 (13)

$$MVM_{j,m} = \frac{CTT_m - CTA_{j+1,m}}{MinW - (MinW - j)}$$
(14)

Step 10: Allocate most task *RPW* to the station j, while respecting the precedence relation of the equivalent diagram of precedence, and the weighted average total station time [so that it does not exceed the largest MVM $(\overline{S_j} \le (major\,MVM_{j,m=1,...M}))$]; Furthermore, pay attention to that the total time m model at the station does not exceed the cycle time $(S_{j,m=1,...M} \le T_c)$;

Step 11: Repeat the process designating the task to stations until there is no feasible task to at least one of the models;

Step 12: Set (j = j - 1) e recalculate $MVM_{j,m=1,...M}$; **Step 13:** Validate the inequality $((major\ AVM_{j,m=1,...M}) \le T_c)$; if met, proceed to the next step; otherwise, return to step 8, reset (MinW = MinW + 1) and restarting the task allocation process; and

Step 14: Repeat steps 10 through 13 until all of the tasks are allocated.

3.2 Balancing assessment generated by the RPW-MVM

The balancing analysis of the resulting RPW-MVM heuristic relies on static indicators, ie without the use of dynamic simulation methods. Thus, in some cases, they are calculated in the AL bottleneck position (g), where production is limited according to Peinado & Graeml (2007). The indicators are: (i) the amount of AL workstations; (ii) capacity in the bottleneck situation (Cap_b) , as depicted in Equation 15; and (iii) crossing time estimated in the bottleneck position $(TCestm_b)$; (iv) Line Efficiency bottleneck situation (LE_b) and (v) balancing efficiency (BE).

$$Cap_b = \frac{available time in the period p}{T_g}$$
 (15)

Where T_g is the bottleneck processing time, defined by the major $S_{j=1,...W,m=1,...M}$.

Likewise, the crossing time estimated by the bottleneck situation ($TCestim_b$), shown in Equation 16 also uses the bottleneck processing time in obtaining it.

$$TCestim_b = (Number of workstations + A) \times T_g$$
 (16)

where A is the number of products not allocated to workstations, but located between the beginning and the end of AL (eg, buffers).

Line Efficiency bottleneck situation (*LEb*) is calculated by Equation 17, whereas the balancing efficiency (*BE*) is given by Equation 18.

$$LE_b = \frac{\sum_{k=1}^{N} \overline{t_k}}{W \times T_a} \times 100 \tag{17}$$

$$BE = \left[1 - \frac{\sum_{j=1}^{W} \left|\overline{S_j} - S_{av}\right|}{W \times S_{av}}\right] \times 100 \tag{18}$$

4 Results and discussion

The method was applied in a AL belonging to a manufacturer of agricultural machines of the type drawn with unit manufacturing lot. The AL is organized into five workstations; in each station there is an operator. Moreover, among the workstations there is a buffering unit that has the function of absorbing excess processing time for some models about the cycle time. Figure 9 illustrates the AL current flow,



Figure 9. AL flowchart with current balance. Source: The authors.

with the number of workstations within the marked blocks and buffers marked with "x" in the center. All computational procedures were performed in spreadsheet. The AL in study manufactures seven models of products, called CL, O, MX, CB, ATI, ATU and CH, which are assembled through up to 29 different tasks depending on the model. Table 1 shows the

Table 1. Performed tasks in the AL for each model.

Work station	Taks	Description	Precedence	CL	o	MX	СВ	ATI	ATU	СН
	1	Tutus 1		37	37	X	37	37	37	
1	1 2	Introduce pre-assembly Preassemble servostat	- 1	X X	X X	Λ	X X	X X	X X	X X
1	_		1	Λ		X		X	X	X
1	3	Mount Steering Column	1	37	X	X	X			
1	4	Preassemble reservoir	1	X	X	37	X	X	X	X
2	5	Preassemble accelerator pedal	1	X	X	X	X	X	X	37
2	6	Place preassembly device at post	2;3;4;5	X	X	X	X	X	X	X
2	7	Preassemble the console structure	6	X	X	X	X	X	X	X
2	8	Preassemble servostat at column	7	X	X		X	X	X	X
2	9	Pre-mount clutch cable	7	X	X	X	X	X	X	
2	10	Pre-mount brake pedals support	7	X	X		X	X	X	
2	11	Mount Valve Brake POWERFILL - 40Km	7							X
2	12	Mount brake valve and reservoir	10	X	X		X	X	X	
2	13	Pre-mount brake sensor	12	X	X		X	X	X	
2	14	Mount switch differential lock	7	X	X	X	X	X	X	X
2	15	Mount clutch pedal	9	X	X	X	X	X	X	
3	16	Mount accelerator pedal	7	X	X	X	X	X	X	X
3	17	Pre-mount plugs from the brake lines	11;12	X	X	X	X	X	X	X
3	18	Mount Steering Column on the console	8		X	X	X	X	X	X
3	19	Assemble Hydraulic Hoses Direction	18	X	X	X	X	X	X	X
4	20	Assemble hoses servostat	8	X	X	X	X	X	X	X
4	21	Assemble hose and return pipe	20;18	X	X		X	X	X	X
4	22	Mount servostat hoses clamp	21	X	X	X	X	X	X	X
4	23	Assemble steering wheel on the console	18	X	X	X	X	X	X	X
4	24	Plase devide in horizontal position	21	X	X	X	X	X	X	X
5	25	Mount firewall plate	24	X	X	X	X	X	X	X
5	26	Mount firewall nuts clips	25	X	X	X	X	X	X	X
5	27	Seal outside on the console	26			X	X	X	X	X
5	28	Plase devide upright	27	X	X	X	X	X	X	X
5	29	Final test	Todas	X	X	X	X	X	X	X

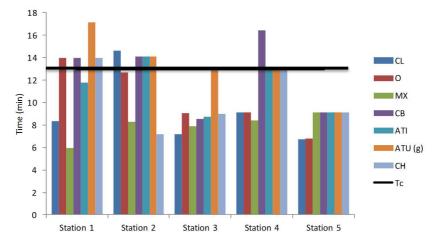


Figure 10. Actual AL balancing. Source: The authors.

product models, the tasks of each workstation and the precedence relationship.

The current AL workload is shown in Figure 10, with the times (in minutes) per workstation and model.

The current planned demand of AL is 37 products per shift, which are thrown randomly into production (no structured sequencing). Each turn consists of 480 minutes of production time, excluding stops for meeting, lunch and breaks.

As can be seen in Figure 10, only the stations 3 and 5 have ability to 37 product/shift for any product, since the time all product models is less than the cycle time. Currently, AL capacity at bottleneck situation is 28 products per shift.

Table 2 presents the mix of products using the company's production plan and the proportion of each model calculated from Equation 8.

Then it was drafted precedence matrix equivalent to all models, as shown in Figure 11.

Based on the total demand of 37 products per turn, we calculated the cycle time (T_c) using Equation 2, which resulted in 12.97 min.

Table 3 shows the time weighted average processing for each task and the *RPW* for each task calculated using Equation 9.

After increasingly ordering the tasks in accordance with the value of the *RPW*, it was determined the number of the last workstation (*W*). To do this, we

calculated the minimum number of workstations for each model (Equation 12), and then it was defined as a worst case model with higher *MinW* (in this case, the ATU model, according to Table 4).

Further, steps 9 were performed by 14 of the method presented in section 3. The values of $MVM_{j,m}$ are shown in Table 5; stands out in bold the value of $MVM_{j,m}$ according to j allocation of tasks to workstations.

The new balance of AL is shown in Figure 12, with the times per workstation and per model.

It can be seen in Figure 12, all workstations have less processing time than the cycle time. Thus, the new balancing provided the AL able to produce 37 products/turn, regardless of the proportion or type of product manufacture. A summary of the tasks allocation to the workstations is shown in Chart 1. As can be seen, there was an increase of 1 workstation

Chart 1. Tasks allocation to workstations for balancing the AL.

Workstation	Task
1	1; 2; 4; 5
2	3; 6; 7; 14
3	8; 9; 10; 12; 16; 18
4	11; 15; 20; 23
5	13; 17; 19; 21
6	22; 24; 25; 26; 27; 28; 29

Table 2. Definition of the production.

	PRODUCT MODEL							т
_	CL	0	MX	CB	ATI	ATU	СН	- I
MIX (quantify for model)	0.8	1.2	0.4	12.5	1.7	20.0	0.4	37.0
Proportion of model	2%	3%	1%	34%	4%	54%	1%	100%

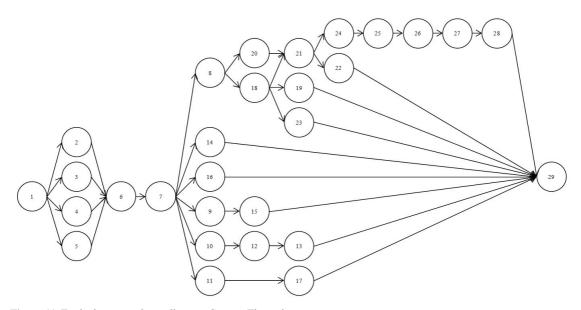


Figure 11. Equivalent precedence diagram. Source: The authors.

Table 3. Weighted average processing time and tasks RPW.

		PRODUCT MODEL								
Taks		CL	0	MX	CB	ATI	ATU	CH	$\overline{t_k}$	RPW
		2%	3%	1%	34%	4%	54%	1%		
1	Introduce pre-assembly	0.37	0.37	0.37	0.37	0.37	0.37	0.37	0.37	0.37
2	Preassemble servostat	4.49	4.49	0.00	4.49	4.49	4.49	4.49	4.44	4.81
3	Mount Steering Column	0.00	5.59	5.59	5.59	3.40	8.77	5.59	7.08	7.44
4	Preassemble reservoir	3.50	3.50	0.00	3.50	3.50	3.50	3.50	3.46	3.82
5	Preassemble accelerator pedal	3.99	3.99	3.99	3.99	3.99	3.99	0.00	3.94	4.31
6	Place preassembly device at post	0.99	0.99	0.99	0.99	0.99	0.99	0.99	0.99	20.28
7	Preassemble the console structure	0.65	0.65	1.25	1.25	1.25	1.25	1.25	1.22	21.50
8	Preassemble servostat at column	3.42	1.47	0.00	2.29	2.29	2.29	2.29	2.26	23.77
9	Pre-mount clutch cable	0.56	0.56	0.56	0.56	0.56	0.56	0.00	0.55	22.05
10	Pre-mount brake pedals support	0.96	0.96	0.00	0.96	0.96	0.96	0.00	0.94	22.44
11	Mount Valve Brake POWERFILL - 40Km	0.00	0.00	0.00	0.00	0.00	0.00	2.08	0.02	21.53
12	Mount brake valve and reservoir	2.08	2.08	0.00	2.08	2.08	2.08	0.00	2.03	24.47
13	Pre-mount brake sensor	0.47	0.47	0.00	0.47	0.47	0.47	0.00	0.46	24.93
14	Mount switch differential lock	0.52	0.52	0.52	0.52	0.52	0.52	0.52	0.52	22.03
15	Mount clutch pedal	0.97	0.97	0.97	0.97	0.97	0.97	0.00	0.96	23.01
16	Mount accelerator pedal	0.93	0.93	0.93	0.93	0.93	0.93	0.47	0.93	22.43
17	Pre-mount plugs from the brake lines	0.80	0.80	0.16	0.80	0.80	0.80	1.58	0.80	25.30
18	Mount Steering Column on the console	0.00	1.89	1.35	1.35	1.52	5.68	1.52	3.68	27.45
19	Assemble Hydraulic Hoses Direction	5.44	5.44	5.44	5.44	5.44	5.44	5.44	5.44	32.89
20	Assemble hoses servostat	3.56	3.56	6.07	10.88	6.07	6.07	6.07	7.55	31.31
21	Assemble hose and return pipe	3.03	3.03	0.00	3.03	4.55	4.55	4.55	3.90	38.89
22	Mount servostat hoses clamp	0.99	0.99	0.82	0.99	0.99	0.99	0.99	0.99	39.88
23	Assemble steering wheel on the console	0.84	0.84	0.84	0.84	0.84	0.84	0.84	0.84	28.29
24	Plase devide in horizontal position	0.68	0.68	0.68	0.68	0.68	0.68	0.68	0.68	39.58
25	Mount firewall plate	2.14	2.18	3.10	3.10	3.10	3.10	3.10	3.05	41.94
26	Mount firewall nuts clips	0.55	0.55	0.55	0.55	0.55	0.55	0.55	0.55	42.49
27	Seal outside on the console	0.00	0.00	1.39	1.39	1.39	1.39	1.39	1.31	43.80
28	Plase devide upright	0.96	0.96	0.96	0.96	0.96	0.96	0.96	0.96	44.76
29	Final test	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	63.03

Table 4. W calculation.

	PRODUCT MODEL							
-	CL	0	MX	СВ	ATI	ATU	СН	
CTT _m	46.0	51.6	39.6	62.1	56.8	66.3	52.3	
T_{c}^{m}	12.97	12.97	12.97	12.97	12.97	12.97	12.97	
MinW	3.55	3.98	3.06	4.79	4.38	5.11	4.03	
Minv				6				
W=j				6				

Table 5. Results of MVM_{j,m}.

		PRODUCT MODEL						
	-	CL	0	MX	CB	ATI	ATU	СН
	MinW	6	6	6	6	6	6	6
	CTT _m	46.0	51.6	39.6	62.1	56.8	66.3	52.3
j = 6	CTA_{j+1}^{m}	0	0	0	0	0	0	0
<i>J</i> – 0	$AVM_{_{III}}$	7.7	8.6	6.6	10.3	9.5	11.0	8.7
<i>j</i> = 5	CTA_{j+1}	8.4	8.5	10.6	10.8	10.8	10.8	10.8
J-S	AVM_{m}	7.5	8.6	5.8	10.3	9.2	11.1	8.3
j = 4	CTA_{j+1}	18.2	18.2	16.2	20.5	22.0	22.0	22.3
<i>J</i> – 4	AVM_{m}	7.0	8.3	5.9	10.4	8.7	11.1	7.5
i – 2	CTA_{j+1}	23.5	23.6	24.1	33.2	29.9	29.9	31.3
j=3	AVM_{m}	7.5	9.3	5.2	9.6	9.0	12.1	7.0
j=2	CTA_{j+1}	31.5	31.5	26.9	41.4	38.2	42.4	35.6
<i>J</i> – 2	AVM_{m}	7.3	10.1	6.4	10.4	9.3	11.9	8.4
	CTA_{j+1}	33.6	39.2	35.3	49.7	44.4	53.9	44.0
j=1	AVM_{m}^{J}	12.3	12.3	4.4	12.3	12.3	12.3	8.4

from the current balance; however, all workstations have processing time less than the cycle time, which ensures a production capacity of 37 products/shift for any model.

Another observed improvement refers to buffers which become dispensable for no longer exists over processing time in relation to the cycle time for any model. Thus, the amount of product in the new AL will not exceed the number of workstations (6); this situation differs from the current balance, which allows up to 9 products in the AL. So you can see

a 33% reduction of inventory in process. Table 6 presents the variables and indicators used to assess the current state of the AL compared to new balance.

The results presented in Table 6 indicate significant improvements from the point of view of the company's experts. The ability of 37 products/shift exceeded the capacity index of the current state by 35% for the AL bottleneck model. This increase is due to the new distribution of tasks. Furthermore, the new balancing allows the release of the products in

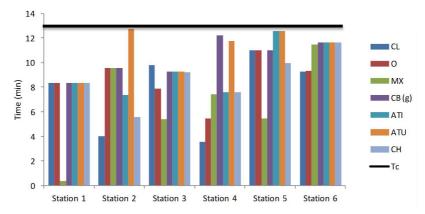


Figure 12. New balance of AL. Source: The authors.

Table 6. Variables and Indicators (Current × RPW-MVM).

		Current balancing	New balancing
	Time available in the period p (min)	480	480
	Demand (parts)	37	37
	Cycle time (min)	12.97	12.97
VARIABLE	Number of buffers	4	0
	Model bottleneck	ATU	CB
	$T_{_{\sigma}}(min)$	17.12	12.69
	CTT_{g} (min)	66.3	62.1
	Amount of AL workstations	5	6
	Cap _g (parts)	28.0	37.8
INDICATOR	TCestim _g (min)	154.08	76.14
	Line efficiency bottleneck situation $(LE_{_{g}})$	63%	83%
	Balancing efficiency (BE)	85%	94%

Table 7. Variables and Indicators (RPW-MVM × RPW).

		New balancing	New balancing
		RPW-MVM	RPW
	Time available in the period p (min)	480	480
	Demand (parts)	37	37
	Cycle time (min)	12.97	12.97
VARIABLE	Number of buffers	0	0
	Model bottleneck	CB	СН
	$T_{_{\sigma}}(min)$	12.69	15.28
	ČTT _g (min)	62.1	52.32
	Amount of AL workstations	6	5
	Cap _g (parts)	37.8	31.4
INDICATOR	TCestim _g (min)	76.14	76.38
	Line efficiency bottleneck situation (LE_{o})	83%	82%
	Balancing efficiency (BE)	94%	98%

AL without particular sequence, which gives great flexibility to the system.

The crossing time estimated in the bottleneck situation was reduced by 50%, which represents that a product can reach the customer 78 minutes faster than today. Finally, the line Efficiency bottleneck situation showed an improvement of 32% under the influence of reduction in processing time bottleneck station (due to rebalance). The balancing efficiency improved 11% (from 85% to 94%), resulting in a better balanced distribution of tasks between the workstations about to the current balance.

Finally, a comparison was performed between the resulting RPW-MVM balancing against traditional RPW applied to mixed-AL, according to Table 7. The flexibility of precondition for a demand for 37 products per shift was not met for the case of balancing proposed by traditional RPW, as capacity in the bottleneck situation was 31.4 products/ shift. Moreover, a reduction in line efficiency at bottleneck situation was observed, despite the reduction of a workstation having occurred, along with the increase in 4% balancing efficiency.

5 Conclusion

This article presents a solution to the mixed AL balancing problem caused by product mix change. The proposed heuristic aims to reduce capacity constraints on workstations within a defined total demand for varied mix without the need for sequencing to launches of products in the AL. To do so, the proposed AL mixed target mobile balancing heuristic (RPW-MVM) is based on three constraints: (i) meet precedence relation equivalent precedence diagram; (ii) allocate the tasks to a workstation so that the total mean time weighted station does not exceed the moving target, and (iii) allocate the tasks to a workstation until the total m model time in the station does not exceed cycle time.

The RPW-MVM heuristic was applied to the AL from a company's agricultural segment. The AL analyzed is currently organized into five different workstations which are manufactured seven models of products (CL, O, MX, CB, ATI, ATU and CH) mounted through up to 29 different tasks. However, the capacity of the bottleneck situation is 28 product/turn, not satisfying the demand for products 37/turn. When applied to the system in question, the RPW-MVM heuristic allowed an increase in production capacity for the bottleneck model by 35% as a result of better distribution of tasks due to increased number of workstations (from 5 to 6). It was also confirmed dispensability sequenced the launch of products in AL. The crossing time significantly reduced the bottleneck situation of AL, requiring 78 minutes less than the old arrangement. The line Efficiency at bottleneck situation showed an improvement of 32%, while

balancing efficiency increased by 11% due to the better distribution of tasks among the workstations. Finally, a comparison of the RPW-MVM and RPW traditional heuristic applied to the mixed AL was held; we observed an improvement in the balance efficiency by 4% with reducing a workstation. However, the flexibility condition was not supported by traditional RPW, concluding that only the RPW-MVM meets the assumptions made in this scenario.

It is suggested for further development the evaluating of the proposed balance by the heuristic through dynamic simulation with the aid of computer software; it aims to identify issues not covered by the current analysis, as the line Efficiency behavior according to the change in product mix. It is suggested further adaptation to balancing AL single model using the concept of moving target proposed here.

References

- Becker, C., & Scholl, A. (2006). A survey on problems and methods in generalized assembly line balancing. *European Journal of Operational Research*, 168(3), 694-715. http://dx.doi.org/10.1016/j.ejor.2004.07.023.
- Boysen, N., Fliedner, M., & Scholl, A. (2007). A classification of assembly line balancing problems. *European Journal of Operational Research*, 183(2), 674-683. http://dx.doi.org/10.1016/j.ejor.2006.10.010.
- Chow, W. M. (1990). Assembly line design: methodology and applications. New York: Marcel Dekker, Inc.
- Cristo, R. L. (2010). Balanceamento de linhas de montagem com uso de algoritmo genético para o caso de linhas simples e extensões (Dissertação de mestrado). Universidade Federal de Santa Catarina, Florianópolis.
- Driscoll, J., & Thilakawardana, D. (2001). The definition of assembly line balancing difficulty and evaluation of balance solution quality. *Robotics and Computer-integrated Manufacturing*, 17(1-2), 81-86. http://dx.doi.org/10.1016/S0736-5845(00)00040-5.
- Farnes, V. C. F., & Pereira, N. A. (2006). Balanceamento de linha de montagem com o uso de heurística e simulação: estudo de caso na linha branca. *Gestão da Produção*, 2, 125-136.
- Fernandes, F. C. F., Godinho, F. M., Cutigi, R. A., & Guiguet, A. M. A. (2008). O uso de programação interia 0-1 para o balanceamento de linhas de montagem: modelagem, estudo de caso e avaliação. *Produção*, 18(2), 210-221.
- Gerhardt, M. P. (2005). Sistemática para aplicação de procedimento de balanceamento em linhas de montagem multi-modelos (Dissertação de mestrado). Universidade Federal do Rio Grande do Sul, Porto Alegre.
- Gerhardt, M. P., & Fogliatto, F. S. (2004). Otimização do balanceamento de linhas de montagem multi-modelo para produção em pequenos lotes. In *Anais do XXIV Encontro Nacional de Engenharia de Produção* (pp. 466-473). Florianópolis: ABEPRO.

- Ghosh, S., & Gagnon, R. J. (1991). Advances in manufacturing assembly systems. *Control and Dynamic Systems*, 46, 355-405. http://dx.doi.org/10.1016/B978-0-12-012746-7.50014-6.
- Kriengkorakot, N., & Pianthong, N. (2007). The assembly line balancing problem. KKU Engineering Journal, 34(2), 133-140.
- Leone, G., & Rahn, R. D. (2004). Fundamentos de la manufactura de flujo. Bouldder: Flow Publishing.
- Marlin, P. G. (1986). Manufacturing lead time accuracy. *Journal of Operations Management*, 6(2), 179-202. http://dx.doi.org/10.1016/0272-6963(86)90024-0.
- Mendes, A. R., Ramos, A. L., Simaria, A. S., & Vilarinho, P. M. (2005). Combining heuristic procedures and simulation models for balancing a PC câmera assembly line. *Computers & Industrial Engineering*, 49(3), 413-431. http://dx.doi.org/10.1016/j.cie.2005.07.003.
- Öztürk, A., Kayalıgil, S., & Özdemirel, N. E. (2006). Manufacturing lead time estimation using data mining. *European Journal of Operational Research*, 173(2), 683-700. http://dx.doi.org/10.1016/j.ejor.2005.03.015.
- Peinado, J., & Graeml, A. R. (2007). *Administração da produção: operações industriais e de serviços*. Curitiba: UNICENP.
- Ponnambalam, S. G., Aravindan, P., & Naidu, G. M. (1999). A comparative evaluation of assembly line balancing heuristics. *International Journal of Advanced Manufacturing Technology*, 15(8), 577-586. http://dx.doi.org/10.1007/s001700050105.

- Praça, I. C. C. S. (1996). Balanceamento e simulação de linhas de fabrico manuais (Dissertação de mestrado). Faculdade de Engenharia, Universidade do Porto, Porto.
- Rekiek, B., Delchambre, A., Dolgui, A., & Bractcu, A. (2002a). Assembly line design: a survey. In *Proceedings* of the XV Triennial World Congress (pp. 1-12). Barcelona, Spain: IFAC.
- Rekiek, B., Dolgui, A., Delchambre, A., & Bratcu, A. (2002b). State of art of optimization methods for assembly line design. *Annual Reviews in Control*, 26(2), 163-174. http://dx.doi.org/10.1016/S1367-5788(02)00027-5.
- Sarker, B. R., & Pan, H. (1998). Designing a mixed-model assembly line to minimize the costs of idle and utility times. *Computers & Industrial Engineering*, 34(3), 609-628. http://dx.doi.org/10.1016/S0360-8352(97)00320-3.
- Smiderle, C. D., Vito, S. L., & Fries, C. E. (1997). A busca da eficiência e a importância do balanceamento de linhas de produção. In *Anais do XVII Encontro Nacional de Engenharia de Produção* (pp. 1-8). Gramado: ABEPRO.
- Souza, M. C. F., Yamada, M. C., Porto, A. J. V., & Gonçalves, E. V., Fo. (2003). Análise de alocação de mão-de-obra em linhas de montagem multimodelo de produtos com demanda variável através do uso de simulação: um estudo de caso. *Revista Produção*, 13(3), 63-77. http://dx.doi. org/10.1590/S0103-65132003000300006.
- van Zante-de Fokkert, J. I., & de Kok, T. G. (1997). The mixed and multi model linebalancing problem: a comparison. *European Journal of Operational Research*, 100(3), 399-412. http://dx.doi.org/10.1016/S0377-2217(96)00162-2.

Erratum

In the article "Mixed assembly line balancing method in scenarios with different mix of products", DOI http://dx.doi.org/10.1590/0104-530X1874-14, published in Gestão & Produção, volume 23, número 2, p. 294-307, on page 294,

where it reads:

Gustavo Reginato¹, Michel José Anzanello¹, Alessandro Kahmann¹

¹Departamento de Engenharia de Produção e Transportes, Universidade Federal do Rio Grande do Sul – UFRGS, CEP 90040-060, Porto Alegre, RS, Brazil, e-mail: reginato205@yahoo.com.br; anzanello@producao.ufrgs.br; alessandro.kahmann@ufrgs.br

it should be read:

Gustavo Reginato¹, Michel José Anzanello¹, Alessandro Kahmann¹, Lucas Schmidt¹

¹Departamento de Engenharia de Produção e Transportes, Universidade Federal do Rio Grande do Sul – UFRGS, CEP 90040-060, Porto Alegre, RS, Brazil, e-mail: reginato 205@yahoo.com.br; anzanello@producao.ufrgs.br; alessandro.kahmann@ufrgs.br; lucasximiti@hotmail.com