Soil Physical Quality in Agricultural Systems on the Cerrado of Piauí State, Brazil

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ABSTRACT

Soil quality is essential for maintaining the sustainability of agro-ecosystems and ecosystem services provided by this natural resource. The present study aimed to assess the physical quality of soil through the characterization of the physical properties in grain production systems in the Southwest region of Piauí State, Brazil. The study was carried out in the Cerrado region of Piauí in four cities in areas of expansion of the agricultural frontier of the state: Baixa Grande do Ribeiro, Sebastião Leal, Uruçuí and Bom Jesus. Soil samples were collected in April 2012, in areas of grain production under conventional and no-tillage systems. Adjacent areas with native vegetation were also sampled as reference. Bulk density, effective saturation, hydraulic conductivity, penetration resistance, porosity and aggregation were measured. Regardless of the type of soil management used, agricultural systems degrade soil physical quality. No-tillage showed higher bulk density, penetration resistance and aggregation, with lower total porosity, macroporosity and hydraulic conductivity. The physical quality of soil in the agricultural areas of the Cerrado region of Piauí was dependent on the soil texture, while silt, clay and organic matter were determinant for soil aggregation, mechanical resistance, total porosity and microporosity.

Key words: sustainable intensification, no-tillage, porosity, aggregation, Oxisols.

INTRODUCTION

No-till farming (NT) was proposed by the Brazilian government to comply with the country’s voluntary commitment to reduce greenhouse gas (GHG) emissions by 36%. The goal is to increase the area planted under no-till by eight million hectares until 2020 (Mapa 2012). This goal, which is part of the Low Carbon Agriculture program (ABC in Portuguese), is one of the top Brazilian public policies, aimed to mitigate GHG emissions.
and increase carbon stocks in agricultural soils (Corbeels et al. 2016).

No-tillage, as well as crop rotation, mulch-till system and no plowing is considered as conservation agricultural practices that can bring several benefits, especially greater efficiency in the control of water erosion (Panachuki et al. 2011, Islam and Reeder 2014). The formation of stable aggregates in water contributes to the improvement of soil physical quality, restoring its porosity, affecting water infiltration processes and contributing to groundwater recharge (Vicente et al. 2012).

The Southwest of Piauí is inserted in the region called “Matopiba” because it is made up of the states of Maranhão, Tocantins, Piauí and Bahia and is the main agricultural frontier of the Cerrado biome. This region extends over an area of 12 million hectares, of which 12% is currently destined for grain production (Conab 2016). Over the last three decades, there has been a significant increase in agricultural activities in this Cerrado region, with increasing replacement of native vegetation by cultivated areas, especially for food, fiber and energy production (Santos et al. 2016).

Since the site of the present study is a region of expansion of the agricultural frontier, few studies for assessment of the impact of soil management on the conversion of natural areas into agricultural areas were carried out. In the Matopiba region, light-textured soils account for 20% of the territory and are mainly constituted by Neossolos, Latossolos and Argissolos (Donagemma et al. 2016). The incorporation of these areas is usually done by conventional soil management, with the purpose of incorporating residues and soil correctives for later conversion to no-till. In an attempt to reduce the original porosity detected in native areas, inappropriate agricultural practices, particularly under conventional tillage, have led to soil degradation (Marchão et al. 2008, Sena et al. 2017). Although chemicals are used in the beginning of the process to correct soil acidity, not all agricultural practices are adopted to prepare the soil for long-term no-till farming. Also, significant investments were made in large, high-performance agricultural machinery, which not always ensure an appropriate agricultural management and observation of soil conservation practices (Borghini et al. 2016). In general, soil cultivation is minimized, without crop rotation or succession planting, and soil preparation, although superficial, is a common practice in the region, leading to soil physical degradation, as a result of changes in physical, chemical and biological properties of these soils caused by excessive soil disturbance and lack of effective mulch cover (Berisso et al. 2012).

In a study conducted in this region, Pragana et al. (2012) reported that replacement of native vegetation by monoculture-based farming systems causes abrupt ecological changes, often marked by degradation of ecosystem services and soil quality. In the Cerrado of Piauí, few studies addressed the effect of soil management systems on soil properties. In a study conducted in the Uruçuí-PI region, in a medium-textured Oxisol, Fontenele et al. (2009) reported that no-tillage did not improve soil aggregation compared to conventional tillage, and the authors attributed this result to the short time period that has elapsed since the implementation of the system.

Since this region is an area of expansion of the agricultural frontier, the characterization of the impact of conversion of native areas into agricultural systems on soil physical quality is still incipient, and further studies are needed. Our hypothesis is that the no tillage promotes better soil physical quality even recently after the conversion of conventional tillage. The importance of soil physical quality and the relationship between soil physical attributes is also emphasized in this paper. Finally, this study aimed to assess soil physical quality by characterizing the soil physical properties in no-till, by comparing its evolution.
from the conventional and reference Cerrado native vegetation areas in four municipalities of the Southwest region of Piauí.

MATERIALS AND METHODS

The study was carried out in the Southwest region of the state of Piauí in grain-producing farms located in four municipalities of the Cerrado (Figure 1): Baixa Grande do Ribeiro (07°48’10”S and 45°00’60”W, altitude 600 m), Sebastião Leal (07°39’14”S and 44°02’37”W, altitude 450 m); Uruçuí (08°14’07”S and 44°38’09” W, altitude 550 m); and Bom Jesus (09°10’35”S and 44°50’36”W, altitude 600 m).

The climate of the region is Aw (tropical savanna climate), according to Köppen climate classification, with predominance of rainy season between October and April and annual average precipitation of 1200 mm. The Matopiba region is mostly formed by light-texture soils and in all sampled areas the soil profiles were classified as Latossolo Amarelo Distrófico típico (Santos et al. 2013) or Ferralsols (WRB 2015). The original Cerrado vegetation was composed of remnant semi-deciduous seasonal forest (Pragana et al. 2012). Analysis of the soil granulometric distribution of the areas was performed according to Claessen (1997), and the results are shown in Table I. The selection of areas and farms aimed to contemplate areas with different soil textures. Table II shows history data of the selected farms.

The sampling was performed in April 2012, in areas of grain production under conventional tillage (CT) and no-tillage (NT) and in remnants of native Cerrado vegetation (NV), used as reference. The sampling points in each of the selected farms were defined after demarcation, with the aid of GPS equipment, of a one-hectare (100 m x 100 m) plot containing 25 points equidistant from each other in a regular mesh. Subsequently, five points were drawn among the twenty-five demarcated points, to compose the five repetitions of each area. A trench was opened at each point, and between the sowing lines four subsamples were collected, at 0-0.10, 0.10-0.20 and 0.20-0.30 m depths. The soil samples were collected with a stainless steel core-soil with an approximate volume of 95 cm³. The deformed samples were packed in plastic bags. In native vegetation areas, sampling was carried out in three randomly demarcated trenches, at least 25 meters apart from each other, and with a minimum distance of 50 meters from the edges.

Bulk density (BD in Mg m⁻³) was calculated by the core-soil method according to Equation 1, described in the manual of soil analysis methods (Donagemma et al. 2011).

\[ BD = \frac{M}{V} \]  

(1)

Where: BD - is bulk density (Mg m⁻³); M - is the mass of the dried sample at 105° C (g) (Mg); V - is the core-soil volume (m³).

| TABLE I | Results of the particle size analysis and soil organic matter contents, averages of the 0-0.3 m layer in the sampled areas located in the Southwest Piauí State, Brazil. |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Baixa Grande do Ribeiro | 618 | 125 | 70 | 187 | 257 | 27.1 |
| Bom Jesus       | 216 | 33  | 108 | 643 | 751 | 11.1 |
| Sebastião Leal  | 319 | 67  | 145 | 470 | 615 | 12.8 |
| Uruçuí          | 187 | 24  | 147 | 642 | 789 | 10.3 |
Effective saturation (ES, in m$^3$ m$^{-3}$) was determined according to Marchão et al. (2007) and Santos et al. (2011) through Equation 2.

$$ES = \theta_s - \theta_{15,198.75}$$ (2)

where: $\theta_s$ is soil moisture at saturation; $\theta_{15,198.75}$ is soil moisture measured in the potential -15,198.75 hPa.

Hydraulic Saturated Conductivity ($K_{sl}$, in mm h$^{-1}$) was obtained in laboratory according to Donagemma et al. (2011), which is based on the rate at which water flows through soil. The soil samples were saturated for 24 hours in a core-soil, with the inflow of fluids maintained at a constant head. Darcy’s law was used in the measurement of hydraulic conductivity. From the four subsamples, three core-soil were selected whose $K_{sl}$ values were considered homogeneous and closer to the average for use in the determination of the other physical properties.

Determination of penetration resistance (PR) was performed with impact penetrometer, with a 4 kg mass plunger (standard), calculated according to Equation 3 (Stolf 1991).

$$PR = \frac{Mg + mg \times \left(\frac{Mg \times h}{x}\right)}{A}$$ (3)

where: PR - penetration resistance, kgf cm$^{-2}$; M - mass of the apparatus without plunger (3.2 kg) (mg = 3.2 kgf); h - plunger drop height (40 cm); x - penetration of the apparatus stem, cm$^{-1}$ impact, and A - cone area, 1.29 cm$^2$. PR values were multiplied by factor 0.098 to obtain PR in MPa. Measurements were randomly made at six points around the trenches. Six readings were taken to obtain an average value per point, totaling 18 replicates per area, as described by Marchão et al. (2007).

Penetration resistance was measured concomitantly in same day, at the same soil moisture content, in each of the areas, for the two soil management systems (CT and NT) and native vegetation, to allow comparison between the soil management systems.

The average PR values were classified according to the Soil Survey Staff (1993), which proposed the following PR classes of soils: extremely low (<0.01 MPa); very low (0.01 - 0.1 MPa); low (0.1-1.0 MPa); moderate (1.0-2.0 MPa); high (2.0-4.0 MPa); very high (4.0 - 8.0 MPa) and extremely high (> 8.0 MPa).

Based on the saturation of the sample, total porosity (TP, in m$^3$ m$^{-3}$) was determined according to Donagemma et al. (2011), calculated using the equation below (4):

$$TP = \frac{V_{sat}}{V}$$ (4)

Where: $V_{sat}$ is the volume of water contained in the pores of saturated soil obtained by the difference between the weight core-saturated soil and core-dry soil at g 105 ºC (m$^3$), V is the soil volume obtained from the core-soil volume ($\pi r 2 h$), expressed in m$^3$.

Soil macroporosity (MaP; in m$^3$ m$^{-3}$) was computed as the difference between total soil water content at saturation (Rogowski 1971, Silva and Azevedo 2002) (PT, m$^3$ m$^{-3}$), considered as the saturated water gravimetric content, and volumetric water content after equilibrium has been reached with soil water potential of -60 hPa (Equation 3) were obtained by centrifuge method (Freitas Jr. and Silva 1984) after previous saturation of the samples through the procedure described by Silva and Azevedo (2002). This potential was regarded as the upper limit of microporosity (MiP).

$$MaP = PT - \theta_{-60}$$ (5)

Microporosity (MiP; m$^3$ m$^{-3}$) was considered as the gravimetric content at -60 hPa.

Soil aggregate characterization was determined with wet sieving apparatus (Yoder 1936), as described in the Manual of Methods of Soil Analysis of Embrapa (Donagemma et al. 2011), in
which the quantity and size distribution of water stable aggregates are calculated, and are related to the aggregates that did not disintegrate by sieving.

The calculation of the percentage of aggregates retained in each sieve was expressed in the following order: >2.00mm (AG1); 2.00-1.00mm (AG2); 1.00-0.50mm (AG3); 0.50-0.25mm (AG4) and <0.25 (AG5), through Equation 6.

$$AG = \frac{A}{B}$$

Where: AG - is the percentage of aggregates in each sieve; A - weight of the aggregate retained in each sieve at 105 °C; B - weight of the sample dried at 105 °C. The aggregate content <0.25mm was obtained by subtracting the total weight of the aggregates retained in the sieves of the total weight of the dried sample at 105 °C. Aggregates smaller than <0.25mm (AG5) were obtained by the difference between the sum of the aggregates retained in the sieves and the total mass of the dried sample at 105 °C.

Macroaggregation (MaA) and microaggregation (MiA) were also calculated by equations 7 and 8, respectively:

$$MaA = 100 \frac{AG > 0.25}{\Sigma AG}$$

Where: MaA - is macroaggregation in %; AG>0.25 is the sum of the aggregates larger than 0.25 mm; \(\Sigma AG\) - is the sum of the total aggregates of the sample.

$$MiA = 100 \frac{AG > 0.25}{\Sigma AG}$$

Where: MiA - is microaggregation in %; AG > 0.25 - is the number of aggregates smaller than 0.25 mm; \(\Sigma AG\) - is the sum of the total aggregates of the sample.

The distribution of aggregates per diameter class, according to Donagemma et al. (2011) was expressed by the geometric mean diameter (GMD) according to equation (9).

$$GMD = \exp \left( \frac{\sum_{i=1}^{n} n \log X_i}{\sum_{i=1}^{n} W_i} \right)$$

Where: Xi - is the mean diameter of the classes (mm); Wi - is the ratio of each class to the total; N - is the percentage of stable aggregates in each class.

The data were organized according to the management system and depth, and descriptive statistics was performed using box-plot graphs to present the measures of central tendency, dispersion, discrepant and extreme values.

In order to verify the relationships between soil physical properties in each one of the sampled areas, conditioned to soil texture and organic matter, a principal component analysis (PCA) was performed in a matrix of 36 lines (three areas/systems, four farms and three soil layers) by 10 columns (physical properties). PCA was performed using the CANOCO statistical program, version 4.5 (Food and Agriculture Organization of the United Nations, New York), where soil texture and organic matter data were plotted as explanatory variables (canonical correlation) not included in the analysis as a dependent variable in the statistical model.

**RESULTS AND DISCUSSION**

Figures 2, 3 and 4 show the box-plot graphs constructed for each soil management system by depth, where arithmetic, median, maximum, minimum, general data dispersion and atypical (spurious) samples are observed.

The areas under no-tillage (NT) had bulk density (BD) values ranging from 1.02 and 1.75 mg m\(^{-3}\) with means of 1.43, 1.52 and 1.52 Mg m\(^{-3}\) m for 0-0.1, 0.1-0.2 and 0.2-0.3 m layers, respectively (Figure 2). The areas under conventional tillage (CT) ranged BD between 0.90 and 1.68 Mg m\(^{-3}\),
with means of 1.27, 1.40 and 1.43 Mg m\(^{-3}\) for 0-0.1, 0.1-0.2 and 0.2-0.3 m layers, respectively. No-till showed higher bulk density (BD) at all the depths investigated when compared to conventional tillage, whose values were closer to the values found in the areas under native vegetation (NV), with means ranging between 1.22 to 1.36 Mg m\(^{-3}\). The higher bulk density in no-tillage is explained by the absence of plowing associated with traffic of machines and implements, especially in moist soil conditions (Souza et al. 2015, Sá et al. 2016). The average values for bulk density in no-tillage are within the range of 1.36 to 1.72 reported by Silva et al. (2014) also in the Cerrado of Piauí, while the values obtained for native vegetation and no-tillage are lower than that obtained by the referred authors. These differences are related to the higher sand content in the soils studied by the referred authors (higher than 75%), while in the present study some soils had higher clay content, e.g. in Baixa Grande do Ribeiro, with 275 g kg\(^{-1}\) of sand (Table I), which may have contributed to the lower average value obtained in the present study. Most of the variation in bulk density is due to differences in total pore volume (Llanillo et al. 2006). Beutler et al. (2012) also reported higher bulk density in no-tillage compared to conventional tillage. The values obtained for no-tillage are higher than the value considered critical to proper plant development proposed by Arshad et al. (1996), which is 1.40 Mg m\(^{-3}\). In a study conducted in Cerrado soils, Sá et al. (2016) obtained as a limiting value for bulk density of 1.33 Mg m\(^{-3}\), but only for very clayey soils.

In all soil layers, no-tillage system showed average effective saturation (ES) values of 0.16 to
Figure 2 - Averages with their respective confidence intervals for bulk density (BD), effective saturation (ES), laboratory hydraulic conductivity (Ksl) and soil penetration resistance (PR) in conventional tillage (CT), no-tillage (NT) and native vegetation (NV) at three depths.
0.21 m$^3$ m$^{-3}$, between the depths, lower than those obtained in conventional tillage, which ranged between 0.21 and 0.30 m$^3$ m$^{-3}$, as shown in Figure 2. The higher ES content suggests that conventional tillage, due to its greater macroporosity (MaA), has higher water retention capacity between saturation and the permanent withering point (Castro et al. 2010). Santos et al. (2011) found similar saturation values between 0.12 and 0.32, in clayey Oxisol under integrated crop-livestock system in the Cerrado of Goiás, Brazil. However, although the ES content in conventional tillage system is similar to the values found in native vegetation at all soil layers, the effect of mechanical management practices that involve the use of farm implements to break up and smoothing out soil surface and subsoilers cannot effectively control compaction, requiring periodic mechanical interventions, as reported by Chamen et al. (2015).

In no-tillage system, hydraulic conductivity values ($K_{sl}$) were lower than 75 mm h$^{-1}$, i.e., lower than the value of 163 mm h$^{-1}$ obtained in conventional tillage (Figure 2). Conventional tillage was the system with $K_{sl}$ value most similar to that of native vegetation in all soil layers. Such data corroborates the findings of Silva et al. (2005) and Kamimura et al. (2009) who also reported a higher $K_{sl}$ value under conventional tillage compared to no-tillage. Soil mobilization may have increased water-borne macropores raising $K_{sl}$, although this effect is temporary (Soracco et al. 2012). In no-tillage, one of the causes of $K_{sl}$ reduction may be the effect if soil compaction, which reduces the number of water-conducting pores, and is consistent with the present study and also with Stone et al. (2002). These authors reported that compaction reduced the number of water-conducting pores, i.e., the pores with larger diameter. According to Drescher et al. (2016), $K_{sl}$ is one of the most sensitive soil properties for assessing the duration of mechanical decompaction.

Soil penetration resistance (PR) has always been measured concomitantly with soil moisture, in each area, for both soil management systems (CT and NT) and native vegetation. Since there was no significant change in water content between the areas, the differences were attributed to the effect of the soil management systems. No-tillage showed higher PR values (between 4.52 and 6.36 MPa in the layers) at all depths when compared to conventional tillage (Figure 2), and the highest value (6.36 MPa) was found at the 0.1-0.2 m depth, i.e. classified as a very high level of penetration resistance according to the Soil Survey Staff (1993). The lower mean values obtained with conventional tillage (between 0.14 and 2.25 MPa) are attributed to the effect of soil plowing for the incorporation of residues and in the process of planting, which is classified as low to moderate PR, according to Soil Survey Staff (1993). However, the values obtained for this layer suggests that the so-called “plow pan” layer tends to remain even after implementation of no-tillage, possibly due to an unsuccessful no-tillage stage or even failure to comply with all the requirements of this practice, such as deep rooted crops, subsurface correction, crop rotation, and mulch cover (Berisso et al. 2012).

The values of penetration resistance (PR) in no-tillage at all soil depths, in native vegetation at depths greater than 0.1 m, and in conventional tillage at a depth of 0.2-0.3 m were greater than 2 MPa, reported by Tormena et al. (1998) as critical to proper plant development. In the Cerrado of Piauí, Barbosa et al. (2016) also found PR values higher than 2 MPa at the 0.2-0.3 m depths and similar values for native vegetation. The higher resistance penetration in native vegetation at depths greater than 0.1 m indicates that this value does not prevent root development. According to Tavares Filho et al. (2001), PR values described in the literature as critical to root development (1 to 3.5 MPa), maybe did not restrain root development of maize in no-
tillage and conventional tillage systems, though it affected root morphology.

Total porosity (TP) results showed an inverse behavior of BD under native vegetation and conventional tillage, with higher averages compared to no-tillage (Figure 3). In soil management systems, TP distribution was more asymmetric at a depth of 0.1-0.2 m. At this depth, data is mostly concentrated in the second quartile, indicating a tendency to lower TP values for both soil management systems compared to native vegetation where the interquartile was more symmetrical. According to the referred data, the higher values for bulk density in no-tillage are detected in the first stage of the process, in conventional tillage, and is explained by the cumulative effect of subsurface compaction, called “plow pan” or “tillage pan” (Cortez et al. 2011).

Conventional tillage had total porosity values of 0.42, 0.34 and 0.32 m$^3$/m$^3$ at 0-0.1, 0.1-0.2 and 0.2-0.3 m layers, respectively, and these results were similar to those obtained for native vegetation at all soil layers. Due to soil disturbance caused by constant plowing, conventional tillage promotes increase in TP, but such increase cannot be maintained after plowing, as reported by Bortoluzzi et al. (2008) and Chamen et al. (2015). Thus, over the years, with the implementation of no-tillage system, the greater availability of organic matter, the absence of soil disturbance and the use of crop rotation is expected to improve soil physical properties. Marcolan and Anghinoni (2006) found higher TP in no-tillage systems.
after eight and twelve years of implementation of the practice compared to a period of four years of no-tillage practice. In a study conducted in the Cerrado of Piauí, Pragana et al. (2012) obtained a lower value of total porosity in no-tillage compared to native vegetation, and attributed these results to the heavy traffic of farm implements, which reduces aggregate stability, reduces macroporosity (MaP), increases microporosity (MiP), resulting in a denser soil matrix. The traffic of agricultural machinery and implements in conventional tillage leads to soil compaction and impacts soil structure, reducing total porosity, especially at deeper soil layers (Barbosa et al. 2016). Possibly, as a result of these soil disturbance practices in conventional tillage, soil compaction tends to persist even after the implementation of no-tillage farming in a region where crop rotation cannot be performed and mulch cover is scarce because rainy seasons are shorter than in other agricultural regions of the Cerrado.

The behavior of macroporosity (MaP) was similar to that of total porosity, with conventional tillage showing means similar to those obtained in native vegetation and mean values higher than those of no-tillage farming (Figure 3). At 0.1-0.2 m and 0.2-0.3 m depths no-tillage showed MaP values of 0.06 and 0.08 m$^3$ m$^{-3}$, respectively, which are lower than the values obtained in conventional tillage, namely, 0.16, 0.11, 0.12 m$^3$ m$^{-3}$. On the other hand, no-tillage showed average values below the limit considered critical for medium-texture soils, of 0.10 m$^3$ m$^{-3}$, which may affect plant development. Possibly, the higher MaP levels reported in conventional tillage are associated to the recent plowing of soil performed in this soil management system (Table II). These results are consistent with those obtained by Tormena et al. (2002) who reported increases in TP and MaP in conventional tillage and minimum cultivation compared to no-tillage, and attributed these results to the use of rake and scarifiers. Andreotti et al. (2010) obtained a linear correlation between soil physical properties (MaP, MiP, PT and BD) and soybean yield and concluded that MaP at the 0-0.10 m layer was the best indicator of physical quality regarding soybean yield in no-tillage, in Cerrado soils. Although conventional tillage exhibits a higher MaP in the first stage of the process, over time soil particles are expected to rearrange themselves to form a more compact structure due to the traffic of agricultural machines and implements. This natural rearrangement caused by frequent soil tillage may impair the future implementation of no-tillage, generating compacted soil layers (Figueiredo et al. 2008).

Microporosity (MiP) showed equal means in the two soil management systems and native vegetation, ranging from 0.20 to 0.25 m$^3$ m$^{-3}$ (Figure 3). Araújo et al. (2010) also did not find differences in MiP values between soil management systems in the Cerrado of Piauí. These results corroborate the findings of Bertol et al. (2004), who inferred that this variable is more resistant to the effects of soil management systems compared to other soil physical properties such as MaP, TP and BD.

On the other hand, in no-tillage, 77.01 to 79.44 % of macroaggregates (MaA) were obtained at the assessed layers, values higher than 72.84 to 76.43 % found in conventional tillage (Figure 4), which corroborates that soil aggregation capacity is higher in no-tillage. However, the values obtained in the management systems are lower than those of native vegetation. The higher MaA in no-tillage may be related to the higher amount of organic matter produced under this management system compared to conventional tillage that involves intensive soil disturbance, and hence organic matter oxidation (Castro Filho et al. 1998, Costa Junior et al. 2011). These data indicate that regardless of non-observation of all no-tillage practice requirements, absence of soil disturbance alone contributes to increase soil aggregation.
TABLE II

History of the different soil management systems sampled in the municipalities of the Southwest Piauí State, Brazil.

<table>
<thead>
<tr>
<th>Municipalities</th>
<th>Soil management system</th>
<th>Description</th>
</tr>
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<tbody>
<tr>
<td>Bom Jesus</td>
<td>Conventional Tillage</td>
<td>Converted in 2009, started with cowpea under conventional tillage and lime application for cowpea cultivation from 2010/2011 to 2011/2012 crop season.</td>
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Microaggregation (MiA) showed an inverse behavior to that of macroaggregation in soil under CT, exhibiting higher levels of MiA. However, in both systems these values were lower than those of native vegetation (Figure 4). Bilibio et al. (2010) comparing the CT with NT, verified a reduction of the geometric mean diameter (GMD) of aggregates with subsurface compaction in conservation systems, whereas in conventional systems there was a decrease in the surface layer, due to the constant soil revolving, which breaks the aggregates into smaller units.

Analysis of the relationships between soil physical properties conditioned to the effect of soil texture and organic matter can be seen in Figure 5. Used as additional (canonical) variables, texture and organic matter explained approximately 20 % of the total variability of data. The physical properties that contributed most to principal component 1 were Ksl and ES, contrasted with MaA and MiA, which are inversely proportional and contribute more to principal component 2. Clay, silt and organic matter (OM) showed greater impact on soil physical properties GMD, MiP, RP and TP, while soil coarser fractions (fine and coarse sand) were more related to soil bulk density. These results demonstrate that the higher the clay-silt fraction, the greater GMD, MiP, RP and PT values.
while higher sand content is related to areas with higher soil density.

Principal component analysis (PCA) indicates that native vegetation tends to present higher MaP, ES and Ksl values, represented by the cloud point group associated with these variables. On the other hand, areas under conventional tillage were associated with higher values of bulk density (BD) and MiA, reinforcing the hypothesis that higher BD values in no-tillage system are detected as soon as this system is implemented and remain high afterwards. Pragana et al. (2012) also found that native vegetation tends to relate with MaP and TP, while no-tillage was associated with BD, in the Cerrado of Piauí. Such data corroborates that the current grain production systems in the Cerrado of Piauí result in degradation of soil physical quality compared to the native vegetation of this region. However, although no-tillage farming has higher BD and RP and lower TP, MaP and Ksl, this system apparently tends to favor a better soil physical quality, as it promotes better soil aggregation in the long run. Finally, the implementation of no-tillage system, with observation of all its requirements, may contribute to faster improvement of soil physical quality in the Piauí Cerrado region.

CONCLUSIONS

Soil management in agricultural areas of grain production in the Cerrado of Piauí affects soil...
physical quality compared to the native vegetation. The degree of impact is variable, and silt, clay and organic matter contents are key elements that determine resistance to penetration, total porosity and microporosity. No-tillage compared to conventional soil tillage shows higher bulk density, resistance to penetration and aggregation and lower total porosity, macroporosity and hydraulic conductivity.

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