One of the most important challenges in adapting high-powered tractors, with auxiliary front-wheel drive (FWD) or all-wheel drive, to fieldwork is the power hop phenomenon. According to LINARES et al. (2006), because of the rigid transmission of the tractor and the terrain, the tires or the FWD clutch coupling normally act as fuse elements. However, there are times when the differences are so great that the fuses are not enough, and the tractor starts to suffer from the phenomenon of energy accumulation, with consequent vibration.

Power hop is an example of self-excited vibration, characterized as a type of jump or oscillation, which alternates up and down movements in sequence, in the direction of the movement of tractors equipped with tires, resembling the galloping movement of a horse (WILEY & TURNER, 2008).

When referring to the phenomenon of power hop (wind-up), RACKHAM & BLIGHT (1985) defined it as the interference between two wheels of different diameters, rigidly connected to the same power transmission source, maintaining contact with the surface of the terrain and forced to spin at the same speed. The differences in size occur for several reasons, including the dynamic distribution of the mass on the axles, internal pressures of the tires, wear, and particular characteristics of the wheelsets. When the dynamic spokes in traction working conditions are not the same, the peripheral speeds of the driving wheels are affected, resulting in the occurrence of the power hop phenomenon and causing severe tire wear.
This phenomenon generally occurs when the tractor is pulling implements or agricultural machines connected to the drawbar, on firm soils and in field operations with medium to high effort. This is commonly observed in auxiliary FWD, where the driving front wheels have a smaller diameter than the rear ones, but it can also occur in tractors with isodiametric all-wheel drive (4×4).

From the beginning of the occurrence of power hop, the tractor exhibits an oscillatory movement with gradually increasing amplitude until the driver is forced to intervene to maintain control of the machine. The amplitude of the oscillation increases with each cycle until it reaches a stable value, called the “limit cycle,” determined by geometric restrictions or the power limits being applied. If it is not restricted early on, the movement makes driving impractical, becoming so severe that the operator may lose contact with the seat and controls, in addition to the possibility of component breakage or accidents.

The dynamic mass distribution, i.e., the mass transfer from the front to the rear axle, also influences the occurrence of power hop, with the variation of this mass transfer being a function of an external effort or force. As an example, when a tractor is pulling an implement to prepare the soil, the mass of the tractor is transferred to the rear axle, causing a decrease in mass on the front wheels and, consequently, a greater tendency of these to slip, in addition to the deformation and diameter reduction of the rear wheels.

The greater the load fraction on the rear axle, the greater the deformation of the rear wheels. When this occurs and the kinematic relationship (KR) between the axles is altered, the front wheels acquire greater speed. Provided they have good grip with the ground, they transfer mass and traction to the front axle, causing a small jump and generating the start of the power hop. If there is excess ballast on the tractor, an even greater transfer of mass to the rear axle may occur, which can aggravate the power hop oscillations, if these are already occurring for other reasons.

Another important point regarding power hop is the type of soil and terrain where the work is being carried out because they are directly linked to the traction capacity and slippage index of the tractor. Normally, power hop occurs in dry soils and paved terrain because slippage is less on these types of terrains. Power hop is unlikely to occur in humid soils because the slippage between the wheels tends to increase, which softens the difference between the axes. This factor individually does not cause power hop to occur. The influence of one of the other factors previously mentioned is needed.

As power hop is a phenomenon that depends on several factors for its occurrence and solution, the option selected to solve the problem in a given situation may be ineffective in another because the machine and soil conditions are different. A sequence of activities to be developed, from the easiest to the most complex, to identify and solve the problem is shown in Figure 1.

There are some procedures that can be performed to correct the power hop problem. The first and simplest is the verification of the internal configuration and pressures of the tractor tires, respecting the recommendation of the manufacturer. There is a possibility to change this configuration by decreasing the pressure of the front tires and increasing that of the rear tires, which can be in reverse order, depending on the initial conditions presented and the KR. There are no fixed values of internal pressure that solve the problem in all cases.

If the problem persists, individual weighing of the tractor axles must be carried out to verify the static mass distribution. Tractors with auxiliary FWD should have a ratio close to 60% of the static mass on the rear axle and 40% on the front axle (FERREIRA et al., 2000) or, for modern tractors, approximately 55% on the rear axle and 45% on the front axle (MÁRQUEZ, 2012). Normally, when power hop occurs, there is more mass on the rear axle, which must be corrected with the addition of ballast on the front axle, successively, until the problem is resolved. If it is still not resolved, the mass on the rear axle should be reduced to balance the system.

If these first interventions are insufficient, the user must check the KR value between the front and rear axles of the tractor. Should the obtained value be more than the recommended one (greater than 5%), it is necessary to decrease the internal pressure of the front axle tires and increase the pressure of the rear ones, repeating the KR calculation until the appropriate values are obtained.

It is also recommended that the user measure the slipping index of the tires because it is an indicator of the need for ballasting. As a reference, the values of 10 to 20% of slippage, depending on whether the tire structure type is radial or diagonal, should be sought to determine the amount of ballast because this range has the maximum efficiency in traction.

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DECLARATION OF CONFLICT OF INTERESTS

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AUTHORS’ CONTRIBUTIONS

The authors contributed equally to the manuscript.

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