Long-term stability decay of standard and regenerated Bragg gratings tailored for high temperature operation

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Abstract— Thermal stability of both standard and regenerated Bragg gratings written in normal and photosensitive optical fibers was accessed. An apparent spectral wavelength stabilization of common gratings with no thermal hysteresis was reached after thermal treatments. However, after a time interval of 5 months, gratings exhibited a shift in the resonance Bragg wavelength at room temperature, as well as important changes in the thermal sensitivity above 200 °C. Regenerated gratings proved to be stable only at temperatures below the critical regeneration temperature, with significant loss of reflectivity above that critical value.

Index Terms- Bragg sensors, High temperature, Decay stability.

I. INTRODUCTION

Fiber Bragg gratings – FBG and recently regenerated-fiber Bragg gratings - RFBG have a great potential for applications as sensors. FBGs have been employed for sensing temperature, mechanical strain, pressure and refractive index [1], [2], [3]. Any external parameter that affects the effective refractive index of the fiber core and/or the grating period may result in a change of the reflected wavelength and might be sensed. Despite their ubiquity, the long term thermal stability of FBG sensors is an important issue to allow their efficient use. Spectral stability is related to the defects responsible by the refractive index modulation that constitutes the FBG. These defects can be thermally activated resulting in changes in the refractive index modulation and consequently affecting spectral characteristics of the FBG based sensor. Due to this drawback, FBG temperature sensors are usually employed in applications with typical operation temperatures below 200°C [4]. Along the past few years, many process as thermal treatments and fiber co-doping were proposed to enhance the FBG stability and lifetime [5]-[8]. Besides, a new class of grating produced by thermal regeneration of fiber Bragg gratings, emerged as a solution for the sensors stability problems [9]-[11]. Mechanism responsible by the FBG regeneration and densification [10], [13]. Regenerated fiber Bragg gratings –

RFBG, operate at high-temperatures and have been employed for measurements up to 1300 °C [14]. However, regeneration is performed by heating the FBG at high temperatures making the fiber brittle. A packaged RFBG sensor was recently proposed to provide mechanical stability and the sensor performance and response time were analyzed [15]. Despite the packaging does not interfere with the RFBG short term sensitivity and repeatability, the measured recovering time of 22 seconds is a direct consequence of the packaging.

In this work, efficiency of thermal treatments on the spectral stabilization of both standard and Bragg and regenerated gratings written in normal and photosensitive optical fibers was accessed. FBGs were submitted to thermal cycles at temperatures up to 425 °C while RFBGs were heated up to 900 °C. Gratings long-term performance regarding sensitivity, hysteresis and spectral stability were analyzed. Performance of a packaged RFBG was also evaluated.

II. METHODS

FBGs were produced in single mode (GF-1 from Nufern) photosensitive and standard (G-652 from Draktel and Furukawa) single mode optical fibers whether hydrogenated or not for photosensitivity enhancement. Inscription was carried out by direct phase mask (PM) laser illumination with KrF (Coherent Xantos XS 500 or Coherent BraggStar Industrial-LN) at 248 nm, as well as with a phase mask interferometer (PMI) under Nd:YAG laser illumination (New Wave Tempest-20) at 266 nm. Fibers were hydrogenated at room temperature along 10 days in a 110 kgf/cm² pressure chamber. Table I summarizes main writing characteristics of produced FBG.

FBG	Fiber	Writing method	Laser frequency (Hz)	Writing time (s)	Energy per Pulse (mJ)	Grating Length (mm)
1	Nufern	PM	100	500	5.00	3.0
2	Nufern	PM	100	500	5.00	3.0
3	Furukawa (H)	PM	100	80	5.00	3.0
4	Furukawa (H)	PM	100	80	5.00	3.0
5	Draktel	PM	50	300	5.00	3.0
6	Draktel (H)	PMI	20	1800	0.11	1.5
7	Nufern	PM	20	5682	0.11	10.0
8	Furukawa (H)	PM	20	3757	0.11	10.0
9	Nufern	PM	20	3009	0.11	10.0
10	Draktel (H)	PM	500	300	5.00	4.0

TABLE I. WRITING PARAMETERS OF FBGS EMPLOYED IN THE EXPERIMENTS (H- HIDROGENATED; PM- PHASE MASK; PMI- PHASE MASK INTERFEROMETER)

Thermal treatments (TT) were carried out in a furnace with a 1200 °C maximum temperature operation. FBGs 1, 2, 3 e 4 were submitted to 3 warm-up/cooling-down cycles. For warm-up temperature ranged from (25.0 ± 0.5) °C to (425.0 ± 0.5) °C in 45 minutes-long steps of 50 °C each. FBG1 and FBG3 were slowly cooled-down (*annealing*) by keeping them inside the furnace after power was switched-off. FBG2 and FBG4 were removed from the furnace immediately after the last

30 minutes-long step at (425.0 \pm 0.5) °C for a fast cooling-down (*quenching*). An optical spectrum analyzer - OSA (Agilent 8614), with 0.06 nm resolution and \pm 2 pm wavelength stability was employed for acquisition of FBGs spectra.

FBGs 5, 6, 7 and 8 were submitted to 4 TT cycles: firstly, the gratings were heated up to (180.0 ± 0.5) °C and kept at this temperature for 2 hours. Then, they were kept at (200.0 ± 0.5) °C for 30 minutes and after at (400.0 ± 0.5) °C for 2 hours. This last procedure was repeated 3 times. After each cycle gratings were submitted to quenching.

After the TT, FBG5 and FBG6 thermal responses were evaluated by heating the gratings up to (350.0 ± 0.5) °C and measuring gratings spectra within temperature steps of 50 °C. Five months later, this procedure was repeated. Values of wavelength and reflectivity were obtained by averaging three measurements obtained under repeatability conditions. Statistical dispersion associated with the measurements was estimated for a confidence level of 68.3 % by means of the combined uncertainty considering the standard deviation of the mean, as well as uncertainties associated with OSA stability and temperature fluctuations.

A similar TT up to (400.0 ± 0.5) °C was applied to FBG7 and FBG8. After, they were kept at (500.0 ± 0.5) °C along 6 hours and 30 minutes and at (600.0 ± 0.5) °C for 6 hours and 40 minutes. A subsequent TT at (700.0 ± 0.5) °C was applied in four stages with the FBGs kept into the oven for: 9 hours and 30 minutes, 7 hours and 30 minutes, 8 hours and finally 7 hours. After each stage the gratings were quenched. Subsequently 3 TT were carried out at (800.0 ± 0.5) °C along 7 hours, 5 hours and 30 hours. A new warm-up/cooling-down cycle was carried out in order to evaluate the thermal sensitivity of gratings. Additionally, FBG7 and FBG8 experienced two TT at (900.0 ± 0.5) °C, each one during time stages of 8 hours.

FBG9 was heated from the room temperature up to (900 ± 0.5) °C in a first time interval of 10 minutes up to (300.0 ± 0.5) °C and then in steps of 50 °C along 35 minutes in each stage.

FBG10 was encapsulated prior the regeneration. For encapsulation, the grating was accommodated inside a ceramic tube (4 mm internal / 6 mm external diameters, 530 mm long, one extremity closed) constituted by Al_2O_3 , heat-resistant up to 1950 °C. Protective acrylate was removed from the optical fiber along 500 mm from the sensing tip with the grating, positioned close to the closed extremity of the tube. The opposite open extremity was sealed with Pattex – NURAL 30 from Henkel Ibérica S.A. (heat-resistant up to 1000 °C) in order to keep the fiber immobile.

Regeneration (RFBG10) was reached by rising the temperature from (23.0 ± 0.5) °C up to (850.0 ± 0.5) °C within a warm-up stage of 78 minutes and kept at this regeneration temperature for 550 minutes. After regeneration the grating experienced a quenching down to room temperature along a 6 hours stage. Spectra were measured with an optical interrogator (Micron Optics SM125, ±5 pm wavelength stability) in the spectral range from 1510 to 1590 nm.

Thermal sensitivity of this probe was determined by submitting the set to warming-up steps 5 minutes long and temperature increment of (100.0 ± 0.5) °C. Between such stages the probe was kept

at constant temperature for 15 minutes. Spectra were measured 5 times at each constant temperature under repeatability conditions and the temperature inside the furnace was monitored with a K-type thermocouple positioned close to the grating. Thermal stability of the probe with RFBG10 was carried out at (800.0 \pm 0.5) °C throughout 490 minutes (55 minutes rise time from 23 °C to 800 °C plus 435 minutes at the final temperature).

III. RESULTS

FBGs 1, 2, 3 and 4 thermal responses during three cycles of TT up to (425.0 ± 0.5) °C are shown in Fig. 1.



Fig. 1. (a) FBG 1, (b) FBG2, (c) FBG3 e (d) FBG4 along the TT for 3 warm-up/cool-donwn cycles from (25.0 ± 0.5) °C to (425.0 ± 0.5) °C.

After each cycle, spectra were measured at room temperature. Linear equations were fitted to the experimental data of each cycle in two temperature ranges, from (25.0 ± 0.5) °C to (225.0 ± 0.5) °C (range I), and from (225.0 ± 0.5) °C to (425.0 ± 0.5) °C (range II). During the whole TT, FBG1 and FBG2 showed constant reflectivity and wavelength stability was observed after the third cycle for both FBGs in spite of grating cooling was fast or slow. As expected, FBG3 and FBG4 thermal response is strongly influenced by the first heating, showing wavelength and reflectivity changes after the first cycle of TT. However, at the end of the TT, these FBGs presented an apparent stability for

both wavelength and reflectivity. Molecular hydrogen diffusion out of the fiber activated by the temperature is mainly responsible by the behavior observed at the first cycle. Thermal responses at the two temperature ranges and the wavelength shift measured at room temperature after each cycle are shown in Table II.

FBG	TT (Heating)	Range I (pm/°C)	Range II (pm/°C)	Δ λ (nm)
1	1°	11.78 ± 0.10	14.49 ± 0.15	- 0.24 ± 0.02
	2°	11.62 ± 0.10	14.39 ± 0.21	- 0.01 ± 0.01
	3°	12.13 ± 0.10	13.98 ± 0.21	- 0.01 ± 0.01
2	1°	11.85 ± 0.09	13.51 ± 0.12	- 0.35 ± 0.02
	2°	12.13 ± 0.10	13.98 ± 0.21	- 0.07 ± 0.01
	3°			0.00 ± 0.01
	1°			- 1.18 ± 0.02
3	2°	11.91 ± 0.10	14.94 ± 0.20	0.01 ± 0.02
	3°			- 0.01 ± 0.01
	1°			-1.35 ± 0.02
4	2°	12.61 ± 0.10	14.24 ± 0.21	0.02 ± 0.02
	3°			0.00 ± 0.01

TABLE II. FBGS SENSITIVITY EVOLUTION ALONG 3 TT AND WAVELENGTH SHIFT AT ROOM TEMPERATURE AFTER EACH CYCLE

Fig. 2 shows the FBG5 (a) and FBG6 (b) time evolution of resonance at (400.0 ± 0.5) °C and at (20.0 ± 0.5) °C during the TT. Data of Fig. 2(c) and 2(d) were fitted by an empirical exponential curve. Due the presence of molecular hydrogen, FBG6 and FBG8 (not depicted here) presented larger wavelength shifts and reflectivity loss than FBG5 and FBG7 (also not depicted here), mainly after the end of first cycle.



Fig. 2. Time evolution of resonance at (400.0 ± 0.5) °C along TT of FBG 5 (a) and FBG6 (b). Resonance wavelength at (20.0 ± 0.5) °C of FBG 5 (c) and FBG6 (d) after each TT. Vertical dotted lines indicate the separation between TT.

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received 21 Oct 2012; for review 7 Dec 2012; accepted 31 July 2013 © 2013 SBMO/SBMag ISSN 2179-1074 After the third and fourth cycles of TT the Bragg wavelength tends to stabilize at room temperature. However, at higher temperatures (200 °C and 400 °C) this behavior is no longer observed for FBG6 and FBG8. As can be seen from Fig. 2(d), important wavelength shifts are observed during all the TT for FBG6, which means that the process was not efficient to stabilize the grating.

Five months later, thermal responses of FBG5 and FBG6, Fig. 3(a) and 3(b), were measured again by heating the gratings up to (350.0 ± 0.5) °C at steps of 50 °C.



Fig. 3. Thermal response of FBG5 e FBG6 along warm-up and cooling-down cycles, measured just after the TT and 5 months later.

Thermal sensitivities were obtained by fitting a linear equation to the experimental data for ranges I (from 20 °C to 200.0 °C) and range II (from 200.0 °C to 350.0 °C). The results are shown in Table III.

	FBG5 (pm/°C)		FBG6 (pm/°C)		
	range I	range II	range I	range II	
1st heating	12.2 ± 0.1	17.6 ± 0.5	12.6 ± 0.2	17.9 ± 0.6	
1st cooling	12.2 ± 0.1	16.3 ± 0.3	12.5 ± 0.1	16.7 ± 0.4	
2nd heating	12.7 ± 0.1	14.9 ± 0.2	12.5 ± 0.1	14.3 ± 0.1	
2nd cooling	13.5 ± 0.1	14.9 ± 0.2	12.8 ± 0.1	14.9 ± 0.2	

TABLE III. THERMAL SENSITIVITY OF FBG5 AND FBG6 JUST AFTER THE TT AND 5 MONTHS LATER.

A comparison between both thermal cycles indicates the TT was not effective to promote the gratings stabilization. For each warm-up to (350.0 ± 0.5) °C and subsequent cooling-down it was not observed any important hysteresis in the Bragg wavelength. However, by repeating the same cycle 5 months later, a blue wavelength shift is observed. Although the thermal sensitivity is not modified up to 200 °C, gratings experience an important change in its sensitivities from 200.0 to 350.0 °C. The presence of hydrogen can be associated with a lower stability of defects responsible for the grating formation, reflected by a higher change in the slope for FBG6, Fig. 3(b).

FBG7 and FBG8 were kept for long time intervals at higher temperatures, (500.0 ± 0.5) °C and (600.0 ± 0.5) °C, but significant wavelength or reflectivity changes were not observed. However, when heated up to (700.0 ± 0.5) °C (1°TT:9 hours and 30 minutes; 2°TT: 7 hours and 30 minutes, 3°TT: 8 hours and 4°TT: 7 hours), both gratings showed important spectral changes. Results are presented in Fig. 4(a) and 4(b). At the first stage of TT, FBG7 were completely erased after 3 hours at (700.0 ± 0.5) °C and a regenerated grating (RFBG) appeared at an approximately 0.3 nm longer wavelength, reaching 60% of the initial reflectivity. In the next stages of TT (at 700.0 °C) after regeneration, reflectivity and wavelength remained approximately unchanged. FBG8 presented loss of reflectivity during the whole TT without noticeable wavelength change. With a further increase of temperature up to (800.0 ± 0.5) °C, RFBG7 experienced a 25% loss of reflectivity (not shown in Fig. 4), and FBG8 regenerated according to Fig. 4(c).



Fig. 4. TT at (700.0 \pm 0.5) °C for (a) FBG7 and (b) FBG8; (c) TT at (800.0 \pm 0.5) °C for FBG8. Vertical dotted lines indicate the separation between TT.

This RFBG8 presented a 2 nm wavelength blue shift after a 2 hours TT (800 °C), recovering about 60 % of its reflectivity. Along the next 30 hours at this temperature, RFBG7 showed an additional 12% loss of reflectivity without tendency for stabilization, in spite of its resonance wavelength remained unchanged.

RFBG7 e RFBG8 regenerated at 700.0 e 800.0 °C, respectively, were submitted to a new 700 °C (bellow the critical temperature for regeneration) warm-up and cooling-down cycle, Fig. 5, without further noticeable spectral changes.

Table IV summarizes the thermal sensitivities of both gratings. For a new 48 hours-long TT at (900.0 ± 0.5) °C, both gratings were erased after 46 hours (RFBG7) and 9 hours (RFBG8), without wavelength shifts along the process.



Fig.5. Thermal response of RFBG7 and RFBG8 bellow the critical temperature for regeneration.

TABLE IV. THERMAL SENSITIVITIES OF RFBG7 E RFBG8.

	RFBG7 (pm/°C)		RFBG8 (pm/°C)		
	range I	range II	range I	range II	
heating	12.0 ± 0.2	15.5 ± 0.1	13.0 ± 0.1	15.8 ± 0.2	
cooling	11.8 ± 0.1	15.7 ± 0.1	13.1 ± 0.1	15.4 ± 0.1	

FBG9 was submitted to a short-term TT in 35 minutes-long steps from room temperature up to 900 °C. Wavelength shift thermal behavior can be described by a single linear function with a (13.8 ± 0.1) pm/°C slope. As expected, grating reflectivity decreased as the temperature was raised, erasing completely at (850.0 ± 0.5) °C but without revealing regeneration within the employed temperature range. Such results show the regeneration is strongly dependent on the fiber constituents, as well as the fiber must be kept at the critical temperature for an adequate long time interval. For the regenerated grating, blue or red wavelength shifts for the resonance may occur also dependent on the fiber constituents.

Fig. 6 shows the time-evolution of FBG10 (encapsulated) reflected signal kept at (850.0 ± 0.5) °C. Amplitudes in dB correspond to the difference between the measured amplitude at resonance wavelength and the average noise out of resonance. As the temperature was raised from the room temperature to the set-point, the reflected amplitude showed a constant value about 50.5 dB, starting to decrease at (850.0 ± 0.5) °C. After 80 minutes the amplitude dropped to a minimum value of 11.9 dB (a decrease of about 38.6 dB). In the next 90 minutes, the grating regenerated reaching maximum amplitude of 39 dB.



Fig. 6. Time-evolution of FBG10 reflected signal, regenerated at (850.0 ± 0.5) °C.

After regeneration, thermal stability of encapsulated RFBG10 was probed at 800 °C along 490 minutes. It was observed increases in both the resonance wavelength at 2.79×10^{-4} nm/minute rate and the reflectivity at 2.74×10^{-4} dB/minute rate. Along 435 minutes, shifts in the wavelength of 0.12 nm and 0.12 dB in the reflectivity were measured; an indicative of the regeneration process was not complete after the initial TT.

Long-term stability was checked for RFBG10. Fig. 7(a) shows the thermal response the encapsulated grating just after the regeneration and 15 months later, where each experimental point is comprised of measurements taken under repeatability conditions. The thermal cycle from room temperature up to (800.0 ± 0.5) °C and back to 23 °C are superimposed, indicating the stability of the device and the absence of thermal hysteresis. Statistical dispersion [16] associated with the measurements was estimated for a confidence level of 68.3 % by means of the combined uncertainty considering the standard deviation of the mean, as well as uncertainties associated with wavelength stability of SM125 interrogator and temperature fluctuations [17]. In Fig. 7(a), the resulting error bars are smaller than the symbols size. A second order polynomial calibration curves were fitted to the experimental points and its derivatives represent the thermal sensitivities in Fig. 7(b). Resolution is also depicted in Fig. 7(b) and was calculated by considering the thermal sensitivities curves and the SM125 wavelength stability.

The non-linear behavior does not present any thermal hysteresis in the thermal cycle for the same experiment. However, after 15 months, besides a positive 0.14 nm hysteresis (estimated at 0° C) there are also changes in sensitivity and resolution. Fig. 7(b) shows the sensitivity increases to the whole dynamic range as the temperature increases, with a consequent better resolution for the measurement. A 0.56 °C resolution at 800 °C is obtained, but for a good performance the sensor requires a periodic calibration. If the initial calibration curve is employed after 15 months, a 721.4 °C value is obtained for a 700 °C temperature, even after the correction of a 0.14 nm hysteresis.



Fig. 7. RFBG10 after regeneration (black) and 15 months later (red): (a) thermal response, (b) thermal sensitivity and resolution.

IV. CONCLUSION

In this work, thermal treatments of FBGs at 400 °C developed an apparent thermal stabilization, independently whether the time evolution of warm-up and cooling-down cycles, type of fiber, writing process or hydrogenation. For all studied gratings, such apparent stabilization was reached after 3 cycles of thermal treatment, the lack of thermal hysteresis misleading to consider the transductor as completely stabilized.

However, long-term assessment showed the thermal stabilization was not reached after the thermal treatment, this effect being more pronounced with hydrogenated Draktel fiber: after 5 months gratings were still instable even operating below the temperature of thermal treatment. Spectral changes occurred at room temperature, and additionally important changes in the thermal sensitivity were found above 200 °C. Such changes were more noticeable for hydrogenated fiber, what suggests the instability can be associated with defect-hydrogen in silica.

By keeping similar gratings (FBG7 and FBG9) under dissimilar thermal treatments it was established the grating regeneration is facilitated by employing long-term (~hours) instead of short (~half-hour) processes. Furthermore, the critical temperature for regeneration is strongly dependent on the fiber constituents.

Regenerated gratings were not stable when heated above the critical temperature for regeneration, and revealed to be just apparently stable under this temperature: although thermal hysteresis was not verified in short-term operation, prolonged storage impaired the metrological characteristics of the sensor, mainly its calibration curve. The need for regular recalibration must be considered to confer reliability to the sensor: along the 15-month storage time of RFBG10, the encapsulated sensor head was just employed on an occasional basis and always bellow the critical temperature for regeneration.

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REFERENCES

- [1] K. O. Hill, G Meltz, "Fiber Bragg grating technology fundamentals and overview," *Journal of Lightwave and Technology*, vol. 15, issue 8, pp. 1263-1276, 1997.
- [2] A. D. Kersey, M. A. Davis, H. J. Patrick, M. LeBlanc, K. P. Koo, C. G. Askin, M. A. Putnam, E. J. Friebele, "Fiber grating sensors," *Journal of Lightwave Technology*, vol. 15, no. 8, pp. 1478-1463, 1997.
- [3] E. Lindner, C. Chojetztki, S. Brueckner, M. Becker, M. Rothhardt, J. Vlekken, H. Bartelt, "Arrays of Regenerated Fiber Bragg Gratings in Non-Hydrogen-Loaded Photosensitive Fibers for High-Temperature Sensor Networks," *Sensors* vol. 9, no. 10, pp 8377-8381, 2009.
- [4] S. R. Baker, H. N. Rourke, V. Baker, D. Goodchild, "Thermal decay of fiber Bragg gratings written in boron and germanium codoped silica fiber," *Journal of Lightwave Technology*, vol. 15, pp. 1470-1477, 1997.
- [5] H. Patrick, S. L. Gilbert, A. Lidgard, M. D. Gallagher, "Annealing of Bragg gratings in hydrogen-loaded optical fiber," *Journal Applied Physics*, vol. 78, pp. 2940-2945, 1995.
- [6] G. Brambilla, L. Reekie, C. Contardi, D. Milanese, M. Ferraris, "Bragg gratings in ternary SiO₂: SnO₂: SnO₂: Na₂O optical glass fibers," *Optics Letters*, vol.25, no. 16, pp. 1153-1155, 2000.
- [7] E. M. Dianov, K. M. Golant, R. R. Khrapko, A. S. Kurkov, B. Leconte, M. Douay, P. Bernage, P. Niay, "Grating formation in a germanium free silicon oxinitride fibre," *Electronics Letters*, vol. 33, no. 3, pp. 236-238, 1997.
- [8] Q. Wang, A. Hidayat, P. Niay, M. Douay, "Influence of Blanket Postexposure on the Thermal Stability of the Spectral Characteristics of Gratings Written in a Telecommunication Fiber Using Light at 193 nm," *Journal of Lightwave Technology*, vol. 18, no. 8, pp. 1078-1083, 2000.
- [9] S. Bandyopadhyay, J. Canning, M. Stevenson, K. Cook, "Ultra-high temperature regenerated gratings in boron codoped germanosilicate optical fibre using 193 nm," *Opt. Lett.*, vol. 33, pp. 1917–1919, 2008.
- [10] J. Canning, M. Stevenson, S. Bandyopadhyay, K. Cook, "Extreme silica optical fibre gratings," Sensors, vol. 8, pp. 6448–6452, 2008.
- [11] J. Canning, S. Bandyopadhyay, M. Stevenson, P. Biswas, J. Fenton, M. Åslund, "Regenerated Gratings," *Journal of European optical Society-Rapidy Publications*, 4, no. 09052, 2009.
- [12] M. Fokine, "Formation of thermally stable chemical composition gratings in optical fibers," *Journal Optical Society of America B*, vol. 19, issue 8, pp. 1759-1765, 2002.
- [13] E. Lindner, C. Chojetztki, S. Brueckner, M. Becker, M. Rothhardt, H. Bartelt, "Thermal regeneration of fiber Bragg gratings in photosensitive fibers," Opt. Expr, vol. 17, pp. 12523–12531, 2009.
- [14] M. L. Åslund, J. Canning, F. Hongyan, H. Tam, "Rapid disappearance of regenerated Fibre Bragg Gratings at Temperatures approaching 1500 °C in Boron-codoped Germanosilicate Optical Fibre," 4th European Workshop on Optical Fibre Sensors-EWOFS'2010, Porto, Portugal, 2010.
- [15] D. Barrera, V. Finazzi, J. Villatoro, S. Sales, V. Pruneri, "Packaged Optical Sensors Based on Regenerated Fiber Bragg Gratings for High Temperature Applications," *IEEE Sensors Journal*, vol. 12, no. 1, pp. 107-111, 2012.
- [16] Evaluation of measurement data Guide to the expression of uncertainty in measurement, JGCM 100:2008, published by BIPM in the name of BIPM, IEC, IFCC, ILAC, ISO, IUPAC, IUPAP and OIML, 2008.
- [17] G. R. C. Possetti, R. C. Kamikawachi, M. Muller, J. L. Fabris, "Metrological Evaluation of Optical Fiber Grating-Based Sensors: An Approach Towards the Standardization," *Journal of Lightwave Technology (Print)*, vol. 30, pp. 1042-1052, 2012.