Evaluation of Castor Bark Powder as a Corrosion Inhibitor for Carbon Steel in Acidic Media

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The inhibition effect of castor bark powder obtained from Ricinus communis on AISI 1020 carbon steel in acidic media (HCl 0.5 mol.L⁻¹) has been studied by electrochemical impedance spectroscopy (EIS), polarization curves, scanning vibrating electrode technique (SVET) and weight loss measurements. Fourier transform infrared spectroscopy (FTIR) and scanning electron microscopy (SEM) were employed as characterization techniques. The EIS and gravimetric results showed that the inhibitory efficiency increases with inhibitor concentration achieving 83%. Polarization curves indicated that the castor bark powder acts as mixed inhibitor. The adsorption of the powder components on the metal surface follows the Langmuir isotherm. The FTIR analyses indicate the presence of C, N and O heteroatoms, incorporated in functional groups mainly related to the presence of carboxylic acids as ricinoleic acid, which could be responsible for the inhibitory properties of the powder. SEM analyses showed that the corrosion process was retarded in the presence of inhibitor in the electrolyte, which was confirmed by SVET measurements. Therefore, the results indicate that castor bark powder has potential to be a corrosion inhibitor for carbon steel in acidic media.

Keywords: Carbon Steel, EIS, Ricinus communis, SVET, Green inhibitors

1. Introduction

Metals and alloys are widely used in industrial applications such as automobiles, petroleum refining, architecture and others. Among them, carbon steel has an important place due to its low cost, good mechanical properties and workability, thermal conductivity, etc. However, this material has low corrosion resistance in acidic media, which can lead to economic losses. Industrial processes as acid cleaning, acid pickling and oil acidification typically use aggressive species, such as hydrochloric acid, which severely attacks carbon steel, being necessary the use of corrosion inhibitors to protect it ¹, ².

Corrosion inhibitors are substances which when added in small quantities to solutions can significantly decrease the metal corrosion rate. One of the proposed inhibitory mechanisms consists in the adsorption of the molecules to the metal surface, creating a barrier between the metal and the electrolyte, blocking active sites and reducing the metal dissolution and/or reduction reactions ³. Many of these inhibitors are organic molecules containing nitrogen, oxygen, sulphur, and phosphorous heteroatoms in their structures, which can adsorb into active sites of the metal surface through conjugated bonds ⁴.

Several conditions must be considered in the choice of an inhibitor, such as, its cost, availability and toxicological effects to humans and to the environment ⁵. Many synthetic inhibitors are known for their toxic properties and high costs. Because of this, researchers have been focused in investigating the inhibitory properties of easily available and low cost natural products that, in addition, are not harmful to health and to the environment, which are generally denominated green inhibitors ⁶. In the literature, several studies are available on the efficiency of leaves or peel extracts as corrosion inhibitors for carbon steel in acidic solutions (generally electrolyte prepared using 37% m/v HCl), like aqueous extracts of mango and orange peel ⁷, and alcoholic extracts of Astemisia Mesatlantica oil ⁸, Roselle ⁹, Eruca sativa ¹⁰, Saccocalyx satureioides ¹¹, Argemone mexicana ¹², Chrysophyllum albidum ¹³, Agavoidae ¹⁴, Tiliacora acuminata ¹⁵, Pimenta dioica ¹⁶, Ilex paraguariensis ¹⁷, Aniba rosa eodora ¹⁸, Ruta chalepenis ¹⁹.

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Castor (*Ricinus communis*) is a fruit used to produce castor oil. The seeds, after being separated from the bark, are submitted to a production process, which involves their pressing to obtain the castor oil. The oil has a wide range of applications, especially in food industry, lubricant, cosmetic ingredient and as source for renewable fuel. The northeast of Brazil is a tropical area that has good conditions for castor cultivation, boosting its production in this region. The state of Bahia is the largest castor producer in Brazil being the castor oil industry an important source of jobs and incomes for the state. However, the oil production generates a large amount of by-products, which recycling is a major challenge for the castor oil industry. Several investigations have already demonstrated that derivatives of the castor oil productive cycle can effectively act as corrosion inhibitor for steel in acidic media. For instance, extract of *Ricinus communis* leaves was investigated as corrosion inhibitor for mild steel and achieved 84% efficiency, three isolated compounds of *Ricinus communis* were tested as corrosion inhibitors and a maximum efficiency of 87% was achieved for ricinine. Efficiency of 87% against corrosion of mild steel in hydrochloric acid media can be achieved using castor oil.

One of the by-products generated during castor oil production is the bark, and the aim of the present work is to investigate the potentiality of castor bark (*Ricinus communis*) powder as corrosion inhibitor for AISI 1020 carbon steel in acidic media (HCl 0.5 mol L\(^{-1}\)) using electrochemical techniques and weight loss measurements.

### 2. Experimental

The AISI 1020 carbon steel (CS) samples were cut into (20 x 20 x 8) mm dimensions, which, previously to testing, were progressively ground using different emery paper (80, 120, 320, 400, 600 and 1200 grit) and then washed with distilled water, ethanol and acetone and dried under a hot air stream.

The castor was granted by farmers of the Camacan city (Bahia, BR). Initially, the bark was extracted from the seeds employing a knife at the Materials and Environment Laboratory (LAMMA) of UESC (State University of Santa Cruz - BA), where some of the experiments were performed. Then, it was washed in distilled water to remove unwanted impurities and dried in an oven at 70 °C for 24 h. To reduce the particles size to a powder, the dried material was milled progressively ground using different emery paper (80, 120, 320, 400, 600 and 1200 grit) and then washed with distilled water, ethanol and acetone and dried under a hot air stream.

The electrochemical experiments were carried out in triplicate with a potentiosiat/galvanostat Metrohm Autolab, model PGSTAT302N, with impedance module. A conventional three-electrode cylindrical glass cell was used with the AISI 1020 carbon steel sample as working electrode (1 cm\(^2\) of exposed surface area), Ag/AgCl/KCl sat as reference electrode and a titanium wire coated with rhodium as auxiliary electrode. The electrolyte was a 0.5 mol L\(^{-1}\) HCl (Anidrol) solution without or with different amounts of the castor bark powder. The experiments were controlled by the software NOVA 1.11 and the data were treated with software Micorcal® Origin® 8.0.

Electrochemical impedance spectroscopy (EIS) diagrams were acquired at the open circuit potential (OCP) after 90 min of stabilization, from 10 kHz to 10 mHz, with 10 points per frequency decade using a potential perturbation amplitude of 10 mV. For quantitative analyses, the EIS data were fitted with ZView2 software.

Potentiodynamic polarization curves were obtained subsequently to the EIS measurements. Anodic sweeps were performed from -30 mV vs OCP to + 250 mV vs OCP, whereas cathodic curves from + 30 mV vs OCP to - 250 mV vs OCP at a scan rate of 0.5 mV s\(^{-1}\). To check reproducibility of results, different samples of working electrode were employed to acquire each branch.

Weight loss measurements were carried out in triplicate according to AISI-G1 standard using rectangular samples (20 x 20 x 8) mm. The immersion time was 120 min, in the 0.5 mol L\(^{-1}\) HCl acid pickling solution without and with different amounts of castor bark powder. With the aim of removing corrosion products from samples surface, they were gently scrubbed with toothbrush and then washed with distilled water, alcohol, acetone and dried under a hot air stream after the immersion test. From the results, corrosion rates and inhibiting efficiencies were determined.

The scanning vibrating electrode technique (SVET) was performed using the Applicable Electronics equipment controlled by ASET-Sciencewares software. The data treatment was carried out using the software QuickGrid in version 5.4. A microelectrode of platinum/iridium from MicroProbes with a platinum deposit of about 10 μm at its tip was used as vibrating electrode and two auxiliary platinum electrodes were used. The distance between the sample and the vibrating probe was 150 μm. The electrolyte used was HCl 1.10\(^{-3}\) mol L\(^{-1}\), which is less aggressive than the other used in this work, because SVET is a localized electrochemical technique and the appearance of bubbles during the experiment affects the measurements, so a less aggressive medium is always used to permit sensing the very beginning of the corrosion process.
The morphologies of the samples surfaces after 120 min immersion in the test electrolyte in the absence and in the presence of the castor bark powder were acquired by scanning electron microscopy (SEM). SEM analyses were obtained by Quanta 250F.

3. Results and Discussion

3.1 Chemical characterization

3.1.1 Fourier transform infrared spectroscopy (FTIR)

Figure 1 shows the FTIR spectrum of the castor bark powder. The large peak centered at 3421 cm⁻¹ can be attributed to OH or/and NH from water or amines. Absorption peak at 2923 cm⁻¹ can be assigned to C-H and its low intensity indicates that only short chain compounds are detected. The band at 1653 cm⁻¹ can be assigned to carbonyl group CN or C=O from carboxylates, as unsaturated carboxylic acids (ricinoleic acid) are present in the castor oil composition. The band at 1457 cm⁻¹ corresponds to CH₃ and its low intensity indicates that the inhibitor may block active sites at the metal surface by adsorption, decreasing the exposed area and reducing the corrosion rate of the material.

The results displayed in Table 1 show that the inhibition efficiency determined for castor bark powder against AISI 1020 carbon steel corrosion increases up to 83% when 1.77 g.L⁻¹ was added to the solution. Several scientists in their studies reported similar results for green inhibitors. The maximum values achieved are also compatible with those found for other castor oil compounds. In addition, from 0.77 g.L⁻¹, the efficiency is higher than 70%, which is indicated in classic literature as an acceptable value for an efficient inhibitor.

The inhibition efficiency (ηᵪ) was calculated from Equation 2, where Cᵪ and Cᵫ are the corrosion rates of carbon steel specimens in the absence and presence of inhibitor, respectively.

\[ \eta_{WL} = \left(1 - \frac{C_{\text{Ri}}}{C_{\text{Ro}}}\right) \times 100 \]  

(2)

Table 1 shows that Cᵪ and iᵩᵪ decrease with increasing inhibitor concentration. This indicates that the addition of castor bark powder to the solution, even in small amounts, hinders the electron transfer between the metal and the electrolyte. It is proposed that the inhibitor may block active sites at the metal surface by adsorption, decreasing the exposed area and reducing the corrosion rate of the material.

The results displayed in Table 1 show that the inhibition efficiency of castor bark powder against AISI 1020 carbon steel corrosion increases up to 83% when 1.77 g.L⁻¹ was added to the solution. Several scientists in their studies reported similar results for green inhibitors. The maximum values achieved are also compatible with those found for other castor oil compounds. In addition, from 0.77 g.L⁻¹, the efficiency is higher than 70%, which is indicated in classic literature as an acceptable value for an efficient inhibitor.

4. Gravimetric test

The inhibition efficiency and corrosion rate (Cᵪ) calculated for AISI 1020 carbon steel from the whole set of weight loss experiments are presented in Table 1. The values of Cᵪ were calculated from Equation 1, where ΔW is the average weight loss in grams, A is the total exposed area (average 8.3 cm²), and t is the immersion time in hours.

\[ C_R = \frac{\Delta W}{A \cdot t} \]  

(1)

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4.1 Adsorption Isotherm

Fitting the surface coverage for different inhibitor concentrations with adsorption isotherms can be used to provide information about the interaction between inhibitor-metal interfaces. In aqueous solutions, the metal surface is covered by adsorbed water dipoles, which may be displaced and replaced by the inhibitors molecules. The simplest of the isotherms, the Langmuir one, is given in Equation 4 and assumes that the adsorbed inhibitor molecules occupy only one site at the metal surface and that there are no interactions between neighboring adsorbed species. In Eq.4, C is the inhibitor concentration, K stands for the adsorption.
Table 1. Corrosion rate, corrosion current density, coverage degree and inhibitory efficiency calculated from gravimetric experiments for AISI 1020 carbon steel, after immersion during 120 min in 0.5 mol.L\(^{-1}\) HCl solution, in the absence and in the presence of different amounts of castor bark powder.

<table>
<thead>
<tr>
<th>Concentration (g.L(^{-1}))</th>
<th>(C_{\text{R}}) (g.h(^{-1}.\text{cm}^{-2}))</th>
<th>(i_{\text{corr}}) (A.cm(^{-2}))</th>
<th>(\eta_{\text{WL}}) (%)</th>
<th>(\theta)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Blank</td>
<td>1.96x10(^{-4})</td>
<td>0.68</td>
<td></td>
<td></td>
</tr>
<tr>
<td>0.44</td>
<td>0.69x10(^{-4})</td>
<td>0.24</td>
<td>65%</td>
<td>0.65</td>
</tr>
<tr>
<td>0.77</td>
<td>0.59x10(^{-4})</td>
<td>0.20</td>
<td>70%</td>
<td>0.70</td>
</tr>
<tr>
<td>1.11</td>
<td>0.51x10(^{-4})</td>
<td>0.18</td>
<td>74%</td>
<td>0.74</td>
</tr>
<tr>
<td>1.44</td>
<td>0.39x10(^{-4})</td>
<td>0.13</td>
<td>80%</td>
<td>0.80</td>
</tr>
<tr>
<td>1.77</td>
<td>0.33x10(^{-4})</td>
<td>0.12</td>
<td>83%</td>
<td>0.83</td>
</tr>
</tbody>
</table>

The equilibrium constant and \(\theta\) is the fractional coverage degree \([\eta_{\text{WL}} (%)/100]\):

\[
\frac{C}{\theta} = \left( \frac{1}{K} \right) + C
\]  

(4)

Figure 2 presents the plot of \((C/\theta)\) against \(C\), according to the data presented in Table 1. A linear plot was obtained, with a correlation coefficient \((R^2)\) higher than 0.99, suggesting that the inhibitor adsorption follows the Langmuir isotherm. The angular coefficient close to 1.0 further confirms the obedience to this isotherm model. This adsorption behaviour is in accordance with other previously reported for green inhibitors on carbon steel surface in different acidic media\(^{2,8,37}\).

4.2 Effect of immersion time on the corrosion inhibition efficiency

The influence of immersion time on the corrosion inhibition efficiency was investigated by the gravimetric method. Table 2 presents the results of the corrosion rates and corrosion current densities, calculated according to Eq. 1 and 3, respectively, for AISI 1020 carbon steel in 0.5 mol.L\(^{-1}\) HCl solution in the presence of 1.77 g.L\(^{-1}\) of castor bark powder after different immersion times. The results show that \(C_{\text{R}}\) and \(i_{\text{corr}}\) increase with immersion time, suggesting deterioration of the inhibitory properties and indicating that electrons exchange between the metal and H\(^+\) becomes easier, enhancing the corrosion process. The comparison of \(i_{\text{corr}}\) values between Table 1 and 2 confirms this analysis, where it can be noted that after 24h of exposure, the \(i_{\text{corr}}\) value for solution with 1.77 g.L\(^{-1}\) of castor bark powder is higher than \(i_{\text{corr}}\) value for the blank sample after 2h of exposure, which confirms that the inhibitor lost its corrosion protection due to immersion time. These results are in accordance with the \(\Delta G_{\text{ads}}^0\) values previously determined and confirm weak interactions between the inhibiting molecules and the metal surface, indicating that the castor bark powder may be used only for applications where long immersion periods are not required, like in pickling processes. Similar behaviour was reported for aqueous extract of \(Argemone\) \(mexicana\) roots\(^6\) and for aqueous coffee ground extracts\(^39\) for carbon steel in 1 mol.L\(^{-1}\) HCl.

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Table 2. Corrosion rates and corrosion current densities calculated from gravimetric experiments for AISI 1020 carbon steel immersed for different times in 0.5 mol.L⁻¹ HCl solution with 1.77 g.L⁻¹ of castor bark powder.

<table>
<thead>
<tr>
<th>Immersion time (h)</th>
<th>CR (g.h⁻¹.cm⁻²)</th>
<th>icorr (A.cm²)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2 h</td>
<td>0.33x10⁻⁴</td>
<td>0.12</td>
</tr>
<tr>
<td>6 h</td>
<td>1.05x10⁻⁴</td>
<td>0.36</td>
</tr>
<tr>
<td>12 h</td>
<td>1.46x10⁻⁴</td>
<td>0.50</td>
</tr>
<tr>
<td>24 h</td>
<td>2.52x10⁻⁴</td>
<td>0.87</td>
</tr>
</tbody>
</table>

5. Electrochemical Techniques

5.1 Electrochemical impedance spectroscopy (EIS)

The EIS diagrams obtained at the OCP after 90 min immersion of the AISI 1020 carbon steel in the test electrolyte in the presence of different amounts of castor bark powder are presented in Figure 3. Initially, the results show that the addition of the powder to the test solution does not change the shape either of the Nyquist (Fig. 3(a)) or of the phase angle x log f (Fig. 3(b)) diagrams indicating that there is no modification of the corrosion mechanism 16,32. In addition, for all experiments, Nyquist plots (Fig. 3(a)) are composed by a single depressed capacitive loop, which diameter and capacitive behavior (Fig. 3(b)) increases with increasing amount of powder added to the electrolyte, evidencing enhanced corrosion resistance. This confirms that castor bark powder inhibits the corrosion of the substrate, which must be a consequence of increased adsorption of molecules with inhibitory properties to the metallic surface hindering the electrochemical process. This hypothesis is in accordance with the adsorption isotherm previously determined, and, is a behaviour already verified for other green inhibitors 40,41.

For a quantitative evaluation of the effects of castor bark powder addition in the corrosion resistance of the CS AISI 1020, impedance diagrams were fitted using the electrical equivalent circuit (EEC) presented in Figure 4. The model is composed by a single time constant and has been commonly used to fit impedance diagrams of CS in acidic solutions, without or with inhibitor addition 17,32,42-44.

In the circuit, $R_s$ is the solution resistance, $R_{ct}$ the charge transfer resistance and $CPE_{dl}$ is a constant phase element (CPE) accounting for the double layer capacity. In EEC fitting of EIS diagrams, capacitances are frequently replaced by CPE to take into account frequency dispersion in the diagrams (depressed loops). The impedance of a CPE can be calculated by means of Equation 6, at which $Q$ is the CPE constant and $\alpha$ is the dispersion factor, other variables having their usual meaning. For $\alpha = 1$, $Q$ is a pure capacitor and the electrode behaves ideally, $\alpha = 0.5$ is obtained when a diffusion-controlled process occurs 46,47 or when the electrode is porous 48,49, whereas for $0.5 < n < 1.0$ the deviation from the ideal capacitive behaviour is attributed to heterogeneities in the electrode surface or to non-homogeneous current distribution on the electrode surface 50,51. Table 3 shows the results of the EEC fitting procedure.

$$Z_{CPE} = \frac{1}{Q(j\omega)^\alpha} \tag{6}$$

Figure 3. EIS diagrams obtained for AISI 1020 carbon steel after 120 min of immersion in 0.5 mol.L⁻¹ HCl in absence and presence of different amounts of castor bark powder: (a) Nyquist and (b) phase angle x log f plots.
For a one time constant process, $R_{CT}$ is directly proportional to the corrosion resistance. Data in Table 3 clearly show that $R_{CT}$ increases when increased amounts of castor bark powder are added to the test solution, confirming the results of the weight loss experiments. The inhibitory efficiency against corrosion (IE%) was calculated using Equation 7, where $R_{CT(0)}$ and $R_{CT(w)}$ are the charge transfer resistance in the absence and in the presence of the inhibitive compound, respectively. The values depicted in Table 3 show the same trend as those calculated from the weight loss measurements (Table 2) but with slightly higher values. This discrepancy can be likely ascribed to the longer immersion time for the weight loss experiments (120 min) when compared to the EIS ones (90 min). As shown in the investigation of the effect of immersion time on the corrosion inhibition efficiency, this parameter decreases with increasing immersion time. Therefore, the longer immersion period taken for the weight loss determination would explain this difference. Interestingly, the discrepancies between the two methodologies diminishes as the powder is added to the electrolyte, remaining almost unchanged whatever the castor bark powder amount. As the inhibitor concentration was reached. The data of Table 3 also points that upon increasing the amount of the inhibitor above the critical concentration the inhibiting efficiency is not decreased, as sometimes found for other inhibitors.

The values reported in Table 3 for the dispersion coefficient ($\alpha$) show that it lies between 0.8 and 0.9, approaching a capacitive behaviour, and it slightly decreases when the powder is added to the electrolyte, remaining almost unchanged whatever the castor bark powder amount. As largely discussed in the literature, interpretation about CPE and their exponents are controversial and methodologies have been developed to determine an effective capacity value ($C_{eff}$) which can be used to disclose the double layer capacity according to Brug formula. However, considering that there are not many differences between the $\alpha$ values of the experiments, a qualitative comparison can be performed for the CPE variation with the castor bark powder amount, allowing associating it with the properties of the interface. According to Helmholtz equation, the double layer capacity can be calculated with Equation 8, where $d$ is the thickness of the double layer, $\varepsilon$ is the dielectric constant of the medium and $\varepsilon_0$ is the vacuum permittivity, which is a constant. Therefore, modifications of the parameters $\varepsilon$ and $d$ can produce changes in $C_{eff}$ which in Table 3 is proportional to $CPE_{dl}$. Water molecules and/or chloride ions can be displaced from the electrode surface by the inhibitors molecules, thus diminishing the dielectric constant of the double layer. In addition, the bigger size of the organic molecules with

$$IE\% = \frac{R_{CT(0)} - R_{CT(w)}}{R_{CT(0)}} \times 100 \quad (7)$$

As already stated, the classic literature reports that the inhibitory efficiency against corrosion must be higher than 70% for an inhibitor to be classified as efficient. Table 3 shows that the inhibitor efficiency calculated from the EIS data fitting achieves more than 70%, which ever the amount of bark powder added to the test solution. These values are the same order of magnitude to those found in the literature for other natural inhibitors, like as Aniba rosaeodora extract (95%)

Molecules with inhibitory properties have been developed to determine an effective capacity value ($C_{eff}$) which can be used to disclose the double layer capacity according to Brug formula.

Table 3. Parameters from the fitting of EIS diagrams with the equivalent circuit of Figure 4 for corrosion of AISI 1020 carbon steel in 0.5 mol.L$^{-1}$ HCl in the absence and presence of different amounts of castor bark powder.

<table>
<thead>
<tr>
<th>Concentration (g.L$^{-1}$)</th>
<th>Rs (Ω.cm$^2$)</th>
<th>Rct (Ω.cm$^2$)</th>
<th>CPE$_{dl}$ μFcm$^{-2}$s$^{\alpha-1}$</th>
<th>$\alpha$</th>
<th>Inhibition Efficiency (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Blank</td>
<td>6.25</td>
<td>272</td>
<td>15.6 E-05</td>
<td>0.88</td>
<td>77%</td>
</tr>
<tr>
<td>0.44</td>
<td>6.15</td>
<td>1195</td>
<td>9.2E-05</td>
<td>0.81</td>
<td>79%</td>
</tr>
<tr>
<td>0.77</td>
<td>6.15</td>
<td>1286</td>
<td>8.0E-05</td>
<td>0.81</td>
<td>79%</td>
</tr>
<tr>
<td>1.11</td>
<td>6.16</td>
<td>1415</td>
<td>8.1E-05</td>
<td>0.82</td>
<td>81%</td>
</tr>
<tr>
<td>1.44</td>
<td>6.14</td>
<td>1561</td>
<td>7.3E-05</td>
<td>0.82</td>
<td>83%</td>
</tr>
<tr>
<td>1.77</td>
<td>6.19</td>
<td>1599</td>
<td>6.3E-05</td>
<td>0.83</td>
<td>83%</td>
</tr>
</tbody>
</table>
inhibitory activity increases the thickness of the double layer\textsuperscript{42,56}. These two features contribute to diminish $C_{dl}$, which is in accordance both with the decreasing of $CPE_{dl}$ values for increasing amounts of castor bark powder (Table 3) and with the adsorption of inhibiting molecules to the electrode surface, previously indicated by the adsorption isotherm.

\[
C_{dl} = \frac{E}{E_{0}}
\]

\[\text{(8)}\]

5.2 Potentiodynamic polarization curves

Potentiodynamic polarization curves for AISI 1020 CS in the absence and presence of different amounts of castor bark powder in 0.5 mol.L\textsuperscript{-1} HCl solution are show in Figure 5. They were obtained after 120 min of immersion, after OCP monitoring and EIS measurements. Figure 5 reveals that both anodic and cathodic polarization curves are shifted towards lower current densities whenever castor bark powder was added to the electrolyte. The current densities were reduced by almost two orders of magnitude for all concentrations, confirming the presence of substances with inhibitory properties in the powder composition. It can be noted that the polarization curves are shifted towards more positive potentials, revealing that castor bark powder acts as mixed inhibitor with slight anodic predominance. Similar behaviours were found in the literature for CS in acidic solutions in the presence of green inhibitors\textsuperscript{2,9,16,57}.

The anodic curves (Fig. 5(a)) indicate that metal oxidation is controlled by activation, since they feature a long linear stretch (Tafel behaviour), whereas the cathodic process is clearly H\textsuperscript{+} reduction. In addition, the shapes of both branches do not change with the addition of castor bark powder, further indicating that the corrosion mechanism does not change and that the inhibiting molecules act by blocking the reaction sites\textsuperscript{28}, which is in agreement with the EIS results.

5.3 Scanning vibrating electrode technique (SVET)

The SVET measurements were carried out by adding 1.77 g.L\textsuperscript{-1} of the bark powder to HCl 1.10\textsuperscript{-3} mol.L\textsuperscript{-1} solution, which is less aggressive than the other solution used in the present work, in order to avoid the evolution of hydrogen bubbles during the experiment. For this technique is mandatory to know the electrolyte resistivity value and in this study it was verified that the presence of corrosion inhibitor increases the bulk electrolyte resistivity value (3370 $\Omega$.cm) due to the presence of organic compounds, when compared with the blank condition (2207 $\Omega$.cm). Thus, localized ionic currents determined by local ratio of potential difference in the perpendicular direction to the surface and electrolyte resistivity became lower in the presence of the inhibitor (less Fe\textsuperscript{2+} ions are released from carbon steel surface) indicating the protective role of the castor bark powder.

The SVET ionic currents maps are show in Figure 6. The sample in the blank solution presents anodic and cathodic areas that represent the electrochemical activity and attack to the metal by the aggressive medium. After 90 min and 240 min of immersion, the current values were intensified due to the evolution of anodic and cathodic reactions, resulting in uniform corrosion of the surface.

The powder was added to the aggressive medium 15 minutes before the immersion of the metal in the solution and the beginning of ionic current measurements. The sample immersed in the electrolyte containing the castor bark powder, after only 2 min of immersion, shows that both anodic and cathodic currents were drastically reduced in comparison to the blank solution.

![Figure 5](image_url)

**Figure 5.** Potentiodynamic polarization curves for AISI 1020 carbon steel in 0.5 mol.L\textsuperscript{-1} HCL solution in the absence and presence of different amounts of castor bark powder: anodic (a) and cathodic (b) branches.
Figure 6. SVET ionic current maps for different immersion times for AISI 1020 carbon steel in absence and in the presence of castor bark powder in $1 \times 10^{-3}$ mol.L$^{-1}$ HCl and the visual aspect of the samples after a) 2 min, b) 90 min and c) 240 min of immersion.

with the blank solution. After 90 and 240 min of test, it can be observed that the behaviour is maintained, the ionic current densities were lower than in the blank solution, proving the inhibitory action of the natural inhibitor leached from the castor bark powder. However, the cathodic current values were concentrated in one region of the sample, indicating that the adsorption process is not completely uniform.
The visual aspect of the samples after 240 min of immersion (Figure 6) shows that there is no formation of corrosion products on the substrate surface in the presence of the powder, whereas a corroded surface was observed for the sample immersed in the blank solution, confirming, once more, the efficiency of the castor bark powder as corrosion inhibitor.

6. Mechanism of Inhibition

The analysis of EIS, SVET and gravimetric results showed a higher corrosion resistance for AISI 1020 carbon steel when the castor bark powder was added to the aggressive electrolyte. According to thermodynamic calculations, the corrosion inhibition mechanism can be ascribed to the adsorption on the metal surface of molecules leached from the castor bark powder, forming a protective barrier, thus reducing CS oxidation and the H⁺ reduction reaction, as demonstrated by the polarization curves. The inhibitive action of castor bark could be explained by the presence of O, N, heteroatoms in the leached molecules that are usually found on corrosion inhibitors that act as adsorption centers and which functionalities were identified in the FTIR spectrum.

The literature suggests that the presence of chloride ions in acidic medium enables the existence of organic constituents of inhibitor in the protonated form as well as neutral molecules, and the adsorption of inhibitor molecules due to excess of negative charge on the metal surface, enhancing the electrostatic interactions between protonated inhibitor molecules and the negatively charged metal surface. On the other hand, neutral molecules reduce the metal dissolution by its adsorption through lone pair of electrons over heteroatoms.

The inhibiting molecules adsorbed at the metal surface block the active sites probably due to the displacement of water molecules through hydrogen bonding with hydroxyl groups of the inhibitor (Reaction 1). This results in the formation of a protective barrier that contributes to retard the ionic flow on the metal surface thus reducing the corrosion rate.

\[
\text{Org}_{(sol)} + x\text{H}_2\text{O}_{(ads)} \rightarrow \text{Org}_{(sub)} + x\text{H}_2\text{O}_{(sol)} \quad \text{Reaction 1}
\]

where \(x\) is the number of water molecules and \(\text{Org}\) is an organic inhibitor.

7. SEM Characterization

SEM images of the AISI 1020 carbon steel surface were acquired before and after 2 h of immersion in HCl 0.5 mol.L\(^{-1}\) in the absence and in the presence of 1.77 g L\(^{-1}\) of castor bark powder. Figure 7 depicts the image of a sample before immersion into aggressive medium. This Figure shows a surface free from corrosion products, but scratches due to the grinding procedure can be detected.

The substrate surface after 2 h immersion in the absence of inhibitor (Figure 8) revealed high degree of attack with the precipitation of corrosion products. On the other hand, when the castor bark powder was added to the solution (Figure 9) corrosion products were not clearly detected and scratch lines are still visible in the surface confirming that the metal is effectively protected from the corrosion process.

Figure 10 shows the substrate surface after 12 h of immersion in HCl 0.5 mol.L\(^{-1}\).

Figure 10 shows the substrate surface after 12 h of immersion in the absence of inhibitor. It can be seen a higher degree of attack in comparison with Figure 8 (2 hours of immersion). However, in the presence of castor bark powder (Figure 11), even with the high time of exposure, the substrate surface was less attacked than in absence of inhibitor, presenting few corrosion products, indicating the inhibitory property of the castor bark powder.
8. Conclusions

The results of the corrosion and, of the electrochemical tests showed that castor bark powder is a potential inhibitor against corrosion of 1020 carbon steel in 0.5 mol L\(^{-1}\) HCl with the inhibiting efficiency increasing when higher amounts of the powder was added to the aggressive solution.

The results of the electrochemical tests (EIS and polarization curves) indicated that the corrosion mechanism was not changed when the powder was added to the solution, whereas the polarization curves showed a mixed inhibitor behaviour with slight anodic predominance. SVET measurements show that in the presence of inhibitors both anodic and cathodic ionic currents became significantly lower showing that the technique can be used to prove the inhibition of molecules on metal surface.

Thermodynamic considerations showed that the inhibiting molecules are weakly adsorbed to the metal surface (physorption) according a Langmuir type adsorption isotherm, which probably takes place by interaction of heteroatoms with the metal surface, as indicated by the FTIR analysis.

Finally, an inhibitory efficiency of 83\% was determined for the highest amount of castor bark powder added (1.77 g.L\(^{-1}\)) to the HCl 0.5 mol L\(^{-1}\), which is compatible with results available for others green inhibitors\(^{20-22}\) as well as determined for other castor oil compounds\(^{10,29,31}\). However, in accordance with the adsorption isotherm calculations, the results showed a decrease of the inhibition efficiency with immersion time, indicating that the castor bark powder can be used only in applications where long immersion periods are not required.

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10. References


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Erratum


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