Influence of Sintering Time on the PTCR Effect of \( \text{Nb}_2\text{O}_5 \)-doped \( \text{BaTiO}_3 \) Ceramics

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The effects of the sintering time on the electrical properties and the positive temperature coefficient of resistance (PTCR) effect of \( \text{Ba}_{1.000}(\text{Ti}_{1-x}\text{Nb}_x)\text{O}_3 \) (BTN) ceramics were investigated, which were sintered at 1190 °C for 0.5–6 hours in a reducing atmosphere and then re-oxidized at 800 °C for 1 hour. The results indicated that the sintering time affected the electrical properties and the PTCR effect of the multilayer BTN samples, whose room-temperature resistance decreased with an increase of the sintering time at same sintering temperature of 1190 °C. However, the resistance jump first increased and then reduced as a function of the sintering time. Furthermore, The BTN ceramics exhibited a pronounced PTCR effect, with a resistance jump greater by 3.6 orders of magnitude, along with a low RT resistance of 0.14 Ω at a reoxidated temperature of 800 °C after sintering at 1190 °C for 2 h in a reducing atmosphere. In addition, the activation energy of samples obtained at different sintering times had also been investigated.

**Keywords:** \( \text{BaTiO}_3 \), PTC effect, \( \text{Nb}_2\text{O}_5 \)-dopant, Reoxidation.

1. Introduction

It is well-known that barium titanate can undergo phase transition from tetragonal to cubic structures \(^1\). Replacing of A or B sites in \( \text{BaTiO}_3 \) (ABO\(_3\)) with trivalent donors or pentavalent impurities, respectively increases the positive temperature coefficient of resistance (PTCR) effect of this material \(^2,3\), as reported by Heywang \(^4,5\) and Jonker \(^6\). According to a proposed model, the PTCR effect of positive temperature coefficient (PTC) ceramics can be considered a grain-boundary effect.

PTCR thermistors are usually used in low-voltage integrated circuits as overcurrent-protection elements. At present, elements with ever-decreasing room-temperature (RT) resistance are required. However, the RT resistance of ceramics can be hardly reduced with traditional preparation methods. In this sense, the RT resistance of ceramics has been reduced by sintering these materials with a reduction/re-oxidation method, which led to a laminated chip-type structure \(^7,8\).

Recently, Lin et al. \(^9\) reported that the electrical properties of two categories of samples were affected by the soaking time. Lu et al. \(^10\) found that the RT resistivities of ceramic samples increased with the soaking time, mostly as a result of the increase in the grain-boundaries resistivities. In addition, according to Al-Allak et al. \(^11\), the PTCR effect is affected by the interfacial segregation of cation vacancies. Ho et al. \(^12\) found that the acceptor-state density depends on the annealing time. Langhammer et al. \(^13\) suggested that the potential barrier height can be enhanced during the cooling process.

However, the influence of the sintering time on the PTCR and electrical properties of \( \text{Ba}_{1.000}(\text{Ti}_{1-x}\text{Nb}_x)\text{O}_3 \) (BTN) ceramics sintered in reducing atmospheres has been scarcely described in the literature. Therefore, the electrical and PTCR properties of BTN samples prepared by the reduction/re-oxidation method were investigated in this paper.

2. Material and Methods

The starting materials were high-purity \( \text{BaCO}_3 \) (> 99.8%), \( \text{TiO}_2 \) (> 99.8%), \( \text{Nb}_2\text{O}_5 \) (> 99.9%), and \( \text{SiO}_2 \) (> 99.9%). The amounts of the different materials were calculated for a formula \( \text{Ba}_{1.000}(\text{Ti}_{1-x}\text{Nb}_x)\text{O}_3 + 0.05 \text{ mol}% \text{SiO}_2 \) (BTN), where \( x \) is 0.35 mol%. These materials were mixed by high-energy ball milling for 90 min (2400 rpm) in deionized water using zirconia balls and subsequently calcined at 1150 °C for 2 h in air. After drying and sieving steps, the calcined powder was ground again using wet ball milling for 5 h in a polyurethane jar. Next, the dried powder was blended with dispersant, solvent, binder, and defoamer agents via ball milling for 18 h in a nylon pot. The mixture was subsequently cast into 55-μm thick green sheets using the doctor-blade method. These sheets were printed with Ni internal electrodes, stacked at 15 MPa and 50 °C to form a ceramic block, and cut into rectangular blocks (3.8 mm × 1.6 mm). Subsequently, the binder was removed by heating at 330 °C in air. The samples were sintered in an aluminum tube at 1190 °C for 0.5, 1, 2, 4 and 6 h (S1, S2, S3, S4, and S5, respectively) in a reducing atmosphere (3% \( \text{H}_2\text{N}_2 \)) at a 200 °C/h heating/cooling rate.

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The bulk densities of the sintered specimens were measured using the Archimedes method. The surface microstructure of the as-sintered ceramics was observed by scanning electron microscopy (SEM; TESCAN MIRA3 EasyProbe, Czech). The mean grain size of the ceramic materials was estimated with the line-intersection method. The sintered BTN ceramics were re-oxidized at 800 °C for 1 h in air, and the surfaces were rubbed with an In–Ga alloy (60:40) to form the electrode. The resistance was measured using a digital multimeter, while the temperature dependent-resistance was measured in a temperature-programmable furnace (ZWX-B, Huazhong University of Science and Technology, China) at a 1.6 °C/min heating rate ranging between 25 and 250 °C.

3. Results and Discussion

3.1 Microstructure of the Ceramics

Figure 1 shows the microstructure of the BTN ceramics sintered at 1190 °C for 0.5−6 h in a reducing atmosphere. The microstructure of the specimens, specially the grain size, was affected by the sintering time. As shown in Figures 1 (a–e), the mean grain size of the S1, S2, S3, S4, and S5 ceramics were 0.86, 0.99, 1.21, 1.49, and 1.54 µm, respectively. The different grain sizes obtained may be explained by differences in the grain growth rates. The grain size increased with the sintering time.

![Figure 1](image-url)

Figure 1. The SEM micrograph on the surfaces of the as-sintered specimens sintered at 1190 °C with different sintering time; (a) 0.5 h, (b) 1 h, (c) 2 h, (d) 4 h, (e) 6 h.
3.2 Influence of the Sintering Time on the Electrical Properties

The resistance jump ratio \( \left[ \log_{10}(R_{\text{max}}/R_{\text{min}}) \right] \) and the RT resistance of the BTN ceramics are shown in Figure 2 as a function of the firing time. The RT resistance of the specimens re-oxidized (air, 800 °C, 1 h) after being reductively sintered (1190 °C, 2 h) decreased with the sintering time increasing from 0.5 to 6 h. The corresponding jumping ratio increased initially and decreased thereafter with the sintering time (0.5–6 h). The optimal resistance jump ratio was obtained for a sintering time of 2 h. This optimal resistance jump ratio increased 3.60 times, and the RT resistance was 0.14 Ω.

3.3 Influence of the Sintering Time on the PTCR Effect

The influence of the sintering time on the PTCR characteristics of BTN ceramics is shown in Figure 2 and 4. The PTCR effect increased first and decreased thereafter with the sintering time. Moreover, the samples re-oxidized at 800 °C for 1 h after being fired at 1190 °C for 2 h exhibited a remarkable PTCR effect. The porous structure (Figure 1) and relative densities (ca. 84.9%) of the ceramics fired at 1190 °C can account for the observed results. The oxygen atoms are easily absorbed at the grain boundaries. Thus, the grain boundaries will be oxidized during the annealing treatment, increasing the resistance and the barrier height in these regions. According to the Heywang–Jonker model, the PTCR effect can be considered a grain-boundary effect. Herein, the PTCR effect was enhanced because of the development of a grain-boundary barrier.

Alternatively, according to the Arrhenius equation, the resistivity is given by the following formula:

\[
\rho = \rho_0 \exp\left(\frac{E_a}{kT}\right)
\]  

where \( \rho_0 \) is a constant, \( \rho \) is the resistivity, \( E_a \) is the activation energy, \( T \) is the absolute temperature, and \( k \) is the Boltzmann constant. Therefore, the slope (\( \lambda \)) of the Arrhenius plot (\( \ln \rho \) versus \( 1/T \)) was introduced, and the slope could be estimated from Eq. 1 with the following formula:

\[
\lambda = \frac{E_a}{k}
\]  

Figure 5 shows the Arrhenius plots (\( \ln \rho \) versus 1000/T) for the BTN samples shown in Figure 4. As shown in Table 1, the activation energies calculated from Eq. 2 for the BTN ceramics fired ranged from 0.29 to 0.97 eV with the sintering time (0.5–6 h). Shorter sintering times resulted in lower activation energies, leading to lower diffusion coefficients of the atoms through the matrix. However, long sintering times favored atomic diffusion because of the high activation energy. In addition, as in the case of the PCTR effect, the activation energy reached a maximum with the sintering time. Meanwhile, the potential-barrier height (\( \phi_0 \)) was estimated from the \( E_a \), when the Fermi level (\( E_F \)) of the grain boundary reached the interface of an accepter level. According to the Heywang–Jonker model, the potential-barrier height should follow the formula:

\[
e\phi_0 = E_a - E_F
\]  

The PTCR effect of the ceramics re-oxidized at 800 °C for 1 h after being fired at 1190 °C for 2 h was enhanced. According to Eq. (3), the potential-barrier height was maximized for these samples, and this can explain these results.

**Figure 2.** The room-temperature resistance and the jumping ratio are as a function of the sintering time.

**Figure 3.** The relative densities of the ceramics are as a function of the sintering time.
4. Conclusions

In present work, the influence of the sintering time on the electrical and the PTCR properties of BTN ceramics fired using the reduction/re-oxidation method was investigated. The relative densities of the samples increased with the sintering time. Moreover, the RT resistance of the BTN ceramics decreased fast with the sintering time and increased slowly thereafter. The resistance jump ratio increased first and decreased thereafter with the sintering time. The BTN ceramics re-oxidized at 800 °C for 1 h after being reductively sintered at 1900 °C for 2 h showed superior PTCR characteristics. Thus, these samples showed increased (by 3.6 times) resistance jumps and a low RT resistance of 0.14 Ω. In addition, the experimental results indicated that the activation energy varied from 0.29 to 0.97 eV with the sintering time.

5. Acknowledgements

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6. References


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**Table 1. Activation energy of the BTN samples, sintered at 1190 °C for different times and reoxidized at 800°C for 1 h.**

<table>
<thead>
<tr>
<th>Samples</th>
<th>Sintering time (h)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>0.5</td>
</tr>
<tr>
<td>$</td>
<td>\lambda</td>
</tr>
<tr>
<td>$E_a$ (eV)</td>
<td>0.29</td>
</tr>
</tbody>
</table>

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**Figure 4.** The temperature dependence of resistance for different sintering time.

**Figure 5.** Arrhenius plots of lnR against $10^3/T$ for BTN samples were reoxidized at 800°C for 1 h after sintering at 1190 °C for different time.


