# Evaluation of shear strength of lingual brackets bonded to ceramic surfaces

Michele Balestrin Imakami\*, Karyna Martins Valle-Corotti\*\*, Paulo Eduardo Guedes Carvalho\*\*, Ana Carla Raphaelli Nahás Scocate\*\*

#### **Abstract**

Objectives: The aim of this study was to evaluate the shear strength of lingual metal brackets (American Orthodontics) bonded to ceramic veneers. Methods: A total of 40 specimens were divided into four groups of 10, according to bonding material and ceramics preparation: Group I - Sondhi Rapid-Set resin and hydrofluoric acid, Group II - Sondhi Rapid-Set resin and aluminum oxide, Group III - Transbond XT resin and hydrofluoric acid, and Group IV - Transbond XT resin and aluminum oxide. Prior to bonding, the brackets were prepared with heavy-duty resin base (Z-250) and the ceramic veneers were treated with silane. The shear test was conducted with a Kratos testing machine at a speed of 0.5 mm/min. **Results:** The results were statistically analyzed by the Tukey test (p<0.05) and showed a statistically significant difference between groups I (2.77 MPa) and IV (6.00 MPa), and between groups III (3.33 MPa) and IV. Conclusions: In conclusion, the bonding of lingual brackets to ceramic surfaces exhibited greater shear strength when aluminum oxide was used in association with the two resins utilized in this study, although Transbond XT showed greater shear strength than Sondhi Rapid-Set.

**Keywords:** Bonding. Ceramic surface. Orthodontics. Lingual brackets.

#### INTRODUCTION

A few years ago orthodontic treatment was regarded as exclusively geared toward children and adolescents. As of the 1970's, the orthodontic industry sought to improve the aesthetic appearance of orthodontic appliances by introducing transparent brackets that could be bonded to the labial surface of the teeth in order to meet the aesthetic needs of adult patients.9 In Europe, in the 1980's, studies began to be conducted on

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<sup>\*</sup> Master in Orthodontics, University of the City of São Paulo (UNICID),

<sup>\*\*</sup> Master and Doctor in Orthodontics, Faculty of Dentistry of Bauru. Associate Professor of the course of Master in Orthodontics, University of the City of São Paulo (UNICID).

lingual orthodontics, which was indicated for those patients who value aesthetics and sometimes refuse traditional orthodontic treatment.9

Besides the concern with aesthetics, another important factor to be considered in adult patients is the presence of prosthetic ceramic crowns. This fact raises the need for studies on the bonding of orthodontic brackets to lingual ceramic surfaces. 15 Although the literature contains research on the bonding of brackets to ceramic surfaces, their results were based on techniques for bonding directly to the labial surface. 4,8,15

It is noteworthy that lingual bonding differs from labial bonding in many respects. The first difference is the laboratory phase, which consists in positioning the brackets in a plaster model with the teeth properly positioned in a setup model of the patient's initial malocclusion. Each bracket receives a portion of filler resin on their base to regularize lingual surface anatomy and the buccolingual width of the teeth, thereby preventing the archwire from having inset/offset bends placed during orthodontic treatment. Thus, bracket bonding (in the patient) occurs by adhesion between the resin on the bracket base and the enamel or ceramic surface.2

Another difference is that the lingual surfaces of teeth exhibit different characteristics when compared to labial surfaces. The lingual surface of posterior teeth is narrower mesiodistally in the occlusocervical direction, showing a steep curvature relative to the labial surface. The upper incisors display concave surfaces with compromised visibility while the lower incisors are affected by tongue position, which requires a skilled professional.<sup>3</sup>

Thus, the lingual technique requires scientific studies to assess and reduce the rate of bracket debonding. It further requires the use of the best possible materials and bonding techniques for preparation of ceramic surfaces mainly due to the fact that ceramic surfaces exhibit lower adhesion than dental enamel.

### **OBJECTIVE**

Based on the reviewed literature, this study intended to evaluate the shear strength of lingual brackets bonded to ceramic surfaces using two resins, i.e., Sondhi Rapid-Set A and B self-curing resin (3M-Unitek) and Transbond XT light-curing resin (3M-Unitek), in addition to two ceramic surface preparation materials, namely, hydrofluoric acid and aluminum oxide.

### **MATERIAL AND METHODS**

For this experiment 40 lingual premolar metal brackets of the Stealth brand (American Orthodontics, Lot No.: 395-0023B) were prepared and had their shear strength tested as follows:

# Bracket base resin preparation

For this research a maxillary arch model in ideal occlusion was selected. The model was duplicated with dental plaster and the lingual brackets were bonded using resin Z-250 (3M, Lot No.: 5BX) to the maxillary right first molars and premolars.

To determine the exact position of the forty brackets on the second premolars a rectangular 0.017x0.025-in stainless steel archwire (American Orthodontics) was adapted to the bonded brackets bypassing the distal side of the second molars, resting on the occlusal surface of the molars and stabilized with self-curing acrylic resin (Ortho Cril yellow, Dental Vip). The mesiodistal position of the brackets was standardized with a red mark on the wire which coincided with the mesial bracket tie wing (Fig 1). The surface of the second premolars received an insulation layer (Cel-lac) to prevent the brackets from adhering to the plaster.

Single Bond 2 (3M) was applied to the second premolar bracket bases prior to Z-250 resin

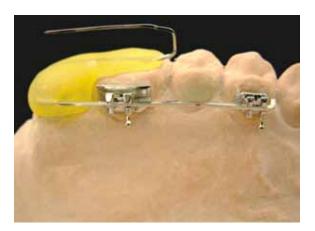


FIGURE 1 - Model with brackets bonded and 0.017x 0.025-in stainless steel adapted with acrylic resin.

application. After placing the brackets in the model all excesses was removed and the resin was cured for 20 seconds (Fig 2).

The resin bases of the 40 brackets received a jet of aluminum oxide (Bio-art, Lot No.: 156,957) for 5 to 10 seconds at a distance of 10 mm until they turned white and opaque. Subsequently, the resin was cleaned with a brush and a solution of ether at 50% (Removex), followed by acetone solution (5, Lutex AP at 58%, Lot No. 11256208), for removal of any oily resin layer from the bracket bases.

#### Fabrication of ceramic specimens

The second premolars in the model received a coat of waxing wax in order to compensate for any shrinkage in the ceramics caused by oven heat (Fig 3). An impression of the model was then made with heavy condensation silicone (Zetalabor). On top of this new impression the ceramic body was applied to the lingual half of the crown impression and subsequently dried with an electric dryer to remove moisture from the ceramic.

The ceramic body was placed in a vacuum oven at a temperature of 925°C for 1 minute. Finishing was accomplished with fine-grained diamond stone and polishing was completed

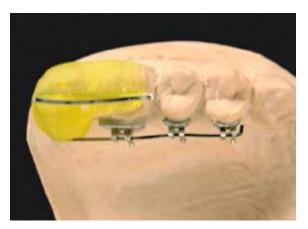


FIGURE 2 - Occlusal view of model with bracket positioned on second premolar and stabilized with occlusal support during resin base Z-250 preparation.

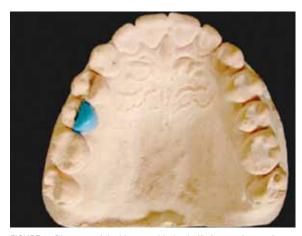


FIGURE 3 - Plaster model with wax added to half of second premolar.

with a special rubber made especially for this procedure. The piece was glazed and surface imperfections corrected. The ceramic body was placed in a non-vacuum oven at a temperature of 880°C for 1 minute.

# **Acrylic cylinder preparation**

A cylinder of Jet acrylic resin was fabricated using a silicone impression tray with 11.0 mm diameter and 8.0 mm thickness to match the



FIGURE 4 - Acrylic cylinder with ceramic specimen adapted with acrylic resin.

size of the metal support on the KRATOS testing machine. The ceramic specimen — in the shape of the second premolar — was attached to the cylinder in such a manner as to allow the metal base of the bracket to be positioned parallel to the acrylic surface after bonding (Fig 4).

## Ceramics preparation and bracket bonding

Twenty ceramic pieces, which had already been inserted in the acrylic cylinder, were prepared with a jet of aluminum oxide (Bio-art, Lot No. 156,057) for 5 seconds at a distance of 5 to 10 mm, rinsed thoroughly and dried with air. The other part of the sample was prepared with 10% hydrofluoric acid (Dentsply, Lot No. 579861) for 4 minutes, rinsed and dried for 15 seconds as described by the manufacturer.

All ceramic veneers received an application of silane (Dentsply, Lot No. 209,071) in a 1:1 ratio, mixed for 10 seconds, with a 5-minute rest.

On twenty specimens (10 prepared with aluminum oxide and 10 with hydrofluoric acid) brackets were bonded with Sondhi Rapid-Set A (3M-Unitek, Lot: 051219), applied to the ceramic surface; and Sondhi Rapid-Set B (3M-Unitek, Lot: 0511114), applied to the resin base of the bracket.

On the other twenty specimens (10 prepared with aluminum oxide and 10 with hydrofluoric



FIGURE 5 - Specimen bonded to ceramic veneer attached to acrylic resin cylinder with bracket base parallel to cylinder surface (lateral distal view of bracket).

acid) brackets were bonded using Transbond XT adhesive (3M-Unitek, Lot: 6 CP) (Fig 5).

Thus, taking into account ceramics preparation and bonding system, the samples were divided into four groups with 10 brackets each, as follows:

- » Group I Sondhi and hydrofluoric acid.
- » Group II Sondhi and aluminum oxide.
- » Group III Transbond XT and hydrofluoric acid.
- » Group IV Transbond XT and aluminum oxide.

## Specimen storage for shear strength test

The specimens were stored for seven days prior to shear test in plastic containers with lids and water at room temperature. The containers were kept in a thermal bag to maintain the temperature.

### Shear strength test

Tensile shear strength tests were performed with a KRATOS Universal Testing Machine at the Department of Prosthodontics, Bauru School of Dentistry, University of São Paulo (Fig 6), by applying 50 Kgf of force at 0.5 mm/min. The values initially obtained in kgf were converted into MPa, a measure used for pressure evaluation.



FIGURE 6 - KRATOS Universal Testing Machine, Department of Prosthodontics, Bauru School of Dentistry, University of São Paulo.

moscedasticity had been applied, one-criterion variance analysis was used to compare groups, disclosing a statistically significant difference between groups (Table 2).

Tukey's test for multiple comparisons only showed statistically significant differences between Group I and Group IV, and between Group III and Group IV (Table 3).

# **Statistical Analysis**

The test results were analyzed statistically. In order to check whether or not the data had normal distribution, the Kolmogorov-Smirnov test was used, and to test for homogeneity of variance among groups, the Bartlett test was used.<sup>21</sup> To compare differences between groups, one-criterion variance analysis (ANO-VA) was performed. When ANOVA showed a significant difference, the Tukey test for multiple comparisons was applied. In all tests, a significance level of 5% was adopted.<sup>21</sup> The tests were performed using the program Statistics for Windows v. 5.1 (StatSoft Inc., USA).

## **RESULTS**

Based on the methodology used in this study comparative results were obtained for the four groups. Table 1 shows the results of means and standard deviations for the four groups.

In checking the normal distribution of data, the Kolmogorov-Smirnov test showed no statistically significant difference (p>0.05). The Bartlett test, which was used to check homoscedasticity (homogeneity of variance) between groups showed no statistically significant difference between variances (p = 0.127). After the criteria of normality and ho-

TABLE 1 - Shear strength means and standard deviations for the four groups, in Mpa.

Group	Strength		
атопр	mean	SD	
1	2.77	0.93	
II	4.30	1.74	
III	3.33	1.35	
IV	6.00	2.17	

TABLE 2 - One-criterion variance analysis (ANOVA) for comparing the four groups.

	GL	QM	GL	QM	F	p
ı	effect	effect	error	error		
	3	19.444	35	2.663	7.302	0.001*

<sup>\*</sup>Statistically significant difference (p < 0.05).

TABLE 3 - Tukey's test for multiple comparisons among the four groups.

Comparison	р
l x II	0.212ns
l x III	0.886 ns
I x IV	0.001*
II x III	0.552 ns
II x IV	0.110 ns
III x IV	0.004*

<sup>\*</sup> Statistically significant difference (p < 0.05). ns = no statistically significant difference.

#### **DISCUSSION**

The bonding of lingual brackets to a ceramic surface was evaluated in this study by comparing two kinds of ceramics preparation and two bonding resins.

The decision to use silane in this study was based on data from the literature that prove its effectiveness in the bonding of labial brackets.11,15,16,22 When applied to ceramic surfaces, silane increased the shear strength, regardless of how the ceramics was prepared. 15,16 Although the use of silane is considered optional by some authors<sup>1,20</sup> — due to difficulties inherent in lingual bonding combined with the inadequate bond strength shown by ceramic surfaces — the silane used on all ceramic surfaces in this research was considered an important element.

Although no research has hitherto been conducted on the bonding of lingual brackets to ceramic surfaces, Wiechmann, 18 in a recent investigation recommended the use of aluminum oxide and hydrofluoric acid prior to bonding ceramic brackets.

The bonding of lingual brackets, which consists of two stages (clinical and laboratory), often with indirect bonding, prompted the need to evaluate the difference in strength between a chemically activated (self-curing) bonding resin (Sondhi Rapid-set A and B) and a light-cured resin (Transbond XT).

The self-curing resin brand commonly found in the literature is Concise which, when combined with hydrofluoric acid showed, respectively, mean values of 17.38 MPa, 15 9.52 MPa, 8 and 4.17 MPa.11 In this study, when preparation was carried out using hydrofluoric acid and bonding performed with the self-curing resin (Sondhi) the mean value found was 2.77 MPa.

Cochran et al<sup>1</sup> obtained a mean value of 39.10 MPa when evaluating the shear bond strength of Concise on a ceramic surface previously prepared with aluminum oxide and silane, while Gillis and Redlich<sup>5</sup> found a mean value of 17.90 MPa. Sant'Anna et al<sup>15</sup> used a primer (Scotchprime - 3M) after the aluminum oxide and found a mean value of 18.64 MPa. Literature values were found to be higher than those reported in this paper. Group II (Sondhi resin and aluminum oxide) showed shear strength of 4.30 MPa. However, the self-curing resin used was different from those reported in the literature.

The lower values of Groups I and II compared to those observed in the literature may have occurred due to differences between labial and lingual bonding techniques. In the lingual technique, adhesion between brackets and ceramic surfaces occurs between the resin on the base (Z-250) and the bonding material, but in the labial technique adhesion takes place between the metal bracket base and the bonding material.

Transbond XT is the most widely used selfcuring resin in the literature and was also selected for this research. Nebbe and Stein<sup>12</sup> also used this resin but prepared the ceramic surface with 37% phosphoric acid and silane, obtaining a mean value of 6.03 MPa. This result was higher than the one found in this study, which vielded a mean value of 3.33 MPa in Group III. However, the acid used in this study was 10% hydrofluoric acid. The choice of acid also differs from the one used by Moreira et al, 11 who applied 35% phosphoric acid with silane to the ceramic surface and found a mean value of 4.27 MPa, also higher than the results of this study.

Based on the methodology, the results showed that the values of Groups I, II and III were lower than would be clinically acceptable, i.e., between 6 and 8 MPa. 19 Group IV showed the best result, with values near those indicated for clinical use.

Group IV (Transbond XT + aluminum oxide) yielded a mean value of 6.00 MPa. This group showed the best overall results, demonstrating superior shear bond strength. Nebbe and Stein<sup>12</sup> concluded that bonding with Transbond XT combined with silane achieves a bonding strength comparable to bonding to enamel. Although the literature reports the effectiveness of Transbond XT and aluminum oxide, no association was found with ceramics bonding.

When the groups were subjected to analysis of variance a statistically significant difference was found between groups (Table 2). Tukey's test showed that this difference was found between Groups I and IV, and III and IV.

The difference between Groups I and IV involved all the factors studied in this research. The resin and preparation used in Group IV (Transbond XT aluminum oxide) showed greater shear strength than in Group I (hydrofluoric acid + Sondhi) (Table 3). Based on the methodology used in this work, light-curing resin proved superior to chemically activated resin. This result differs from other studies in the literature, which did not use Sondhi resin.4,10

Groups III and IV, which were also statistically different, showed that aluminum oxide is superior to hydrofluoric acid when bonding to ceramic surfaces (Table 3). This result is in agreement with Cochran et al, who noted that when ceramics is treated with silane, aluminum oxide affords greater strength than hydrofluoric acid. Some authors contradict the results reported above. Gillis and Redlich<sup>5</sup> conducted an electron microscopy analysis and revealed that erosion caused by a diamond bur or jet of aluminum oxide produced superficial wear while hydrofluoric acid produced deep wear. In a literature review,

Vieira et al<sup>16</sup> concluded that hydrofluoric acid appears more effective than aluminum oxide for roughening the ceramic surface.

Wiechmann<sup>18</sup> described the influence of a jet of aluminum oxide prior to etching with phosphoric acid. The author concluded that the adhesive strength between enamel and bonding material can be significantly increased with a jet of aluminum oxide prior to etching. He recommended the same procedure when bonding to ceramic surfaces.

Due to difficulties involved in bonding lingual brackets, an effective method has been sought to ensure a low debonding rate. The combination of hydrofluoric acid and aluminum oxide applied to the ceramic surface can increase shear strength. In this study, the best result was obtained with Transbond XT lightcuring resin. Some professionals, however, still prefer self-curing resins. It is therefore suggested that other chemically activated resins also be evaluated to meet this market demand.

## **CONCLUSIONS**

Based on the methodology used and results achieved in this study, it can be concluded that:

The bonding of lingual brackets to ceramic surfaces exhibited greater shear strength when aluminum oxide was used in association with either of the two resins utilized in this study, although Transbond XT showed greater shear strength than Sondhi Rapid-Set.

#### REFERENCES

- 1. Cochran D, O'Keefe KL, Turner DT, Powers JM. Bond strength of orthodontic composite cement to treated porcelain. Am J Orthod Dentofacial Orthop. 1997;111(1):297-300.
- Chumak L, Galil KA, Way DC, Johnson LN, Hunter WS. An in vitro investigation of lingual bonding. Am J Orthod Dentofacial Orthop. 1989;95(1):20-8.
- Echarri P. Procedimiento para el posicionamiento de brackets em Ortodoncia lingual. Parte I. Ortod Clin. 1998;1(2 Pt 1):69-77.
- Eustaquio R, Garner LD, Moore BK. Comparative tensile strengths of brackets bonded to porcelan with orthodontic adhesive and porcelain repair systems. Am J Orthod Dentofacial Orthop. 1988;94(5):421-5.
- 5. Gillis I, Redlich M. The effect of different porcelain conditioning techniques on shear bond strength of stainless steel brackets. Am J Orthod Dentofacial Orthop. 1998;114(4):387-92.
- Huang TH, Kao CT. The shear bond strength of composite brackets on porcelain teeth. Eur J Orthod. 2001;23(4):433-9.
- Jost-Brinkmann PG, Can S, Drost C. In-vitro study of the adhesive strengths of brackets on metals, ceramic and composite. Part 2: bonding to porcelain and composite resin. J Orofacial Orthop. 1996;57(3 Pt 2):132-41.
- Kao EC, Johnston WM. Fracture incidence on debonding of orthodontic brackets from porcelain veneer laminates. J Prosthet Dent. 1991;66(5):631-7.
- Kurz C, Romano R. Lingual Orthodontics: historical perspective. In: Romano R. Lingual Orthodontics. Amilton: BC Decker; 1998.
- 10. Major PW, Koehler JR, Manning KE. 24-hour shear bond strength of metal orthodontic brackets bonded to porcelain using various adhesion promoters. Am J Orthod Dentofacial Orthop. 1995;108(3):322-9.
- 11. Moreira NR, Sinhoreti MAC, Oshima HMS, Casagrande RJ, Consani RLX. Avaliação in vitro da resistência à tração de braquetes ortodônticos metálicos colados ao esmalte ou à cerâmica, com compósitos químicos ou fotoativados. Biosci J. 2001;17(2):171-82.

- 12. Nebbe B, Stein E. Orthodontic brackets bonded to glazed and deglazed porcelain surfaces. Am J Orthod Dentofacial Orthop. 1996;109(4):431-6.
- 13. Newman SM, Dressler KB, Grenadier MR. Direct bonding of orthodontic brackets to esthetic restorative materials using a silane. Am J Orthod. 1984;86(6):503-6.
- 14. Pannes DD, Bailey DK, Thompson JY, Pietz DM. Orthodontic bonding to porcelain: a comparison of bonding systems. J Prosthet Dent. 2003;89(1):66-9.
- 15. Sant'Anna EF, Monnerat ME, Chevitarese O, Stuani MBS. Bonding brackets to porcelain - In vitro study. Braz Dent J. 2002;13(3):191-6.
- 16. Vieira S, Saga A, Wieler W, Maruo H. Adesão em Ortodontia – Parte 2. Colagem em superfícies de amálgama, ouro e cerâmica. J Bras Ortodon Ortop Facial. 2002;7(41 Pt 2):415-24.
- 17. Wang WN, Tarng TH, Chen YY. Comparison of bond strength between lingual and buccal surfaces on young premolars. Am J Orthod Dentofacial Orthop. 1993;104:251-3.
- 18. Wiechmann D. Lingual orthodontics (Part 3): intraoral sandblasting and indirect bonding. J Orofac Orthop. 2000; 61(4 Pt 3): 280-91.
- 19. Winchester L. Direct orthodontic bonding to porcelain: an in vitro study. Br J Orthod. 1991;18(4):299-30.
- 20. Zachrisson BU. Orthodontic bonding to artificial tooth surfaces: clinical versus laboratory findings. Am J Orthod Dentofacial Orthop. 2000;117(5):592-4.
- 21. Zar JH. Biostatistical analysis. 3rd ed. New Jersey: Prentice-Hall; 1996.
- 22. Zelos L, Bevis RR, Keenan KM. Evaluation of the ceramic/ ceramic interface. Am J Orthod Dentofacial Orthop. 1994;106(1):10-21.

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# Contact address

Michele Balestrin Imakami Avenida Vila Rica, 6 - Centro CEP: 87.250-000 - Peabiru / PR, Brazil E-mail: michele\_bales@oi.com.br