

METHOD ADJUSTMENT AND EQUATION SET OF MAXIMUM RAINFALL INTENSITY, DURATION AND FREQUENCY IN THE MATO GROSSO DO SUL STATE¹

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ABSTRACT: Due to the lack of information concerning maximum rainfall equations for most locations in Mato Grosso do Sul State, the alternative for carrying out hydraulic work projects has been information from meteorological stations closest to the location in which the project is carried out. Alternative methods, such as 24 hours rain disaggregation method from rainfall data due to greater availability of stations and longer observations can work. Based on this approach, the objective of this study was to estimate maximum rainfall equations for Mato Grosso do Sul State by adjusting the 24 hours rain disaggregation method, depending on data obtained from rain gauge stations from Dourado and Campo Grande. For this purpose, data consisting of 105 rainfall stations were used, which are available in the ANA (Water Resources Management National Agency) database. Based on the results we concluded: the intense rainfall equations obtained by pluviogram analysis showed determination coefficient above 99%; and the performance of 24 hours rain disaggregation method was classified as excellent, based on relative average error WILMOTT concordance index (1982).

KEYWORDS: intense rainfall, rainfall disaggregation, weather stations.

AJUSTE DE METODOLOGIA E DETERMINAÇÃO DAS EQUAÇÕES DE INTENSIDADE, DURAÇÃO E FREQUÊNCIA DA PRECIPITAÇÃO PLUVIAL MÁXIMA PARA O ESTADO DE MATO GROSSO DO SUL

RESUMO: Devido à carência de informações relativas às equações de precipitação máxima para a maioria das localidades do Estado de Mato Grosso do Sul, a alternativa para a realização de projetos de obras hidráulicas tem sido utilizar informações de postos meteorológicos mais próximos da localidade na qual o projeto é realizado ou fazer uso de metodologias alternativas, tal como o método de desagregação de chuvas de 24 horas, a partir de dados pluviométricos em função da maior disponibilidade de estações e maior tempo de observações. Com base nesse enfoque, o objetivo do trabalho foi estimar as equações de precipitação máxima para o Estado de Mato Grosso do Sul por meio do ajuste da metodologia de desagregação de chuvas de 24 horas, em função dos dados obtidos das estações pluviográficas de Dourados e de Campo Grande. Para tanto, foram utilizados dados consistidos em 105 estações pluviométricas, disponíveis no banco de dados da ANA. Com base nos resultados, foi possível concluir: as equações de chuvas intensas obtidas pela análise de pluviogramas apresentaram coeficiente de determinação acima de 99%; e o desempenho do ajuste da metodologia de desagregação de chuvas de 24 horas foi classificado como ótimo, com base no erro médio relativo ao índice de concordância de WILMOTT (1982).

PALAVRAS-CHAVE: chuvas intensas, desagregação de chuvas, estações meteorológicas.

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INTRODUCTION

Knowledge of the quantities characterizing a rainfall that relates the intensity, duration and frequency (IDF), also known as intense rainfalls equation, shows great technical interest in hydraulic structures projects, such as weir dimensioning, watercourse rectification, sewers, drainage systems, among others (PRUSKI et al., 2006; SANTOS et al., 2009).

A research, performed under an agreement between the Sanitation Company of Minas Gerais (COPASA) and the Federal University of Viçosa (UFV), under the Support Foundation of UFV (FUNARBE), set theoretical models of probability distribution to the intense rainfall data for 193 rain gauge stations in Minas Gerais State and at boundaries between Bahia and Espírito Santo States. The adjusted parameters of intensity, duration and frequency equations showed high variability; thus, demonstrating the importance of obtaining intense rain equation for each location (FREITAS et al., 2001).

Due to the lack of information concerning intense rain equations for most Brazilian locations, an alternative to perform hydraulic structure projects has been using information from weather stations nearest the location in which the project is carried out. This procedure, however, can lead to unreliable estimates (PEREIRA et al., 2007; SILVA et al., 2003; SILVA et al., 2002).

Some methods have been developed in Brazil to obtain shorter rains from daily rainfall records, due to existence of a vast rainfall network installed, mainly to serve power generation sector. The methods use multiplicative coefficients, among which the 24 hours rain disaggregation method stands out (CETESB, 1986; OLIVEIRA et al., 2008).

Studies conducted based on annual pluviometric and rain gauge data series, observed simultaneously in São Paulo, showed that average rain heights, of one or two days, can be considered a fairly representative estimate of 24-hour-rainfall of same frequency. They also observed that regardless of return period, there is a constant relationship between 24-hour-rainfalls and one-day-rainfalls, whose value was 1.14 (PINTO et al., 1996).

GENOVEZ & ZUFFO (2000), cited by SANTOS et al. (2009), however, concluded that the methods based on the relationship among intense rainfall of different durations have regional validity. According to the authors, it is convenient to establish new coefficients that are related to local microclimates, for local estimates.

Besides the intense rainfall equation method, it is of fundamental importance to adjust methods that enable equation estimations from daily rainfall data due to greater availability of pluviometric stations and longer observations, so that maximum average rainfall intensity for locations out of rain gauge stations can estimated accurately. However, there are several works with direct application of alternative methods, such as FIETZ et al. (2010); FIETZ & COMUNELLO (2007); GARCIA (2010); OLIVEIRA et al. (2008); and SANTOS et al. (2009).

Based on this approach, the objectives of this work were to obtain the maximum rainfall equations for the cities of Dourado and Campo Grande, located in Mato Grosso do Sul State. In addition, determine intensity, duration and frequency equations by fitting 24-hour rain disaggregation method into data obtained by Dourados and Campo Grande.

MATERIAL AND METHODS

We used the rainfall data from two weather stations available for Dourados-MS, one operated by Embrapa Western Agriculture and another by the Federal University of Grande Dourados (UFGD) in this work. For the region of Campo Grande a weather station belonging to the National Institute of Meteorology (INMET) was used. Table 1 shows the geographical coordinates of the stations and data collection periods.

TABLE 1. Geographical coordinates of the weather stations and collection period of rainfall data used in the estimation of maximum average rainfall for Dourados-MS and Campo Grande-MS, Brazil.

City	Weather station	Latitude	Longitude	Period
Dourados:	Embrapa (CPAO)	22°16'S	54°49'W	1979-1990 1991-2004
	Universidade Federal da Grande Dourados (UFGD)	22°11'S	54°55'W	2004-2010
Campo Grande:	Instituto Nacional de Meteorologia (INMET)	20°27'S	54°38'W	1973-1985 1993-1998 2000-2009

The equation used to relate rainfall intensity, duration and frequency showed the form described by VILLELA & MATTOS (1975).

The phase of the rainfall data acquisition started with the selection of pluviograms containing the most torrential rains by each year. Maximum annual rainfalls were determined for durations of 10, 30, 60, 120, 360 and 1440 min. By dividing the maximum rainfall heights with the corresponding duration, we obtained maximum annual rainfall intensity for each duration.

Annual maximum intensity series for each duration were adjusted to the Gumbel extreme value distribution. The distribution parameters were estimated by maximum likelihood method and data adherence to the theoretical distribution assessed by Kolmogorov-Smirnov test at 20% probability.

Using non-linear adjustment technique based on maximum annual rainfall intensity values, in return periods 2, 5, 10, 20, 50 and 100 years and the different studied durations, we obtained IDF equation parameters.

To compare the 24-hour rainfall disaggregation method with the pluviogram analysis method (standard method); primary the first method was used without changing multiplicative coefficients, as proposed by the Department of Electricity and Water / Basic Sanitation and Technology Center (DAEE / CETESB 1980), in the cities of Dourados and Campo Grande. This method adopts an average factor of 1.14 to convert maximum rainfall into 1 day, that is, from Gumbel distribution method into 24 hour-rainfall; for the remaining rainfall duration times, coefficients are employed according to the aforementioned method, allowing to generate enough points to define IDF equation related to different return periods.

Settings of probability distributions, such as completion of adhesion test, were made similarly to data obtained by pluviogram analysis method, as described by PEREIRA et al. (2007).

Results obtained by intense rainfall equations adjusted by 24-hour rainfall disaggregation method were compared with those obtained by the pluviogram analysis. Method performance was evaluated by relative error and concordance index proposed by WILLMOTT (1981). We also used performance analysis criterion proposed by CAMARGO & SENTELHAS (1997).

For adjusting the 24-hour rainfall disaggregation, and therefore obtaining the relationship between rainfall heights by each duration, rainfall height values in different durations were divided by maximum 24-hour rainfall height. Therefore, coefficients, which allowed conversion of the local 24-hour rainfall height with durations of 10, 30, 60, 120, 360 and 1440 min, were obtained. Multiplicative coefficients representing each duration were obtained by geometric mean of the analyzed period.

Performance of alternative method adjustment was also assessed using relative mean error, concordance index (WILLMOTT, 1982) and performance analysis model (CAMARGO e SENTELHAS, 1997).

After adjusting alternative method, we proceeded to implementation. Then, we selected historical data series of daily rainfall from pluviometric stations located in the State, which were obtained from Hydrological Information System of the National Water Agency (Hidroweb) (ANA, 2013). Subsequently, data were subjected to a consistency analysis and locations whose series had less than 12 years of complete observations were eliminated, resulting in 105 pluviometric stations (Figure 1).

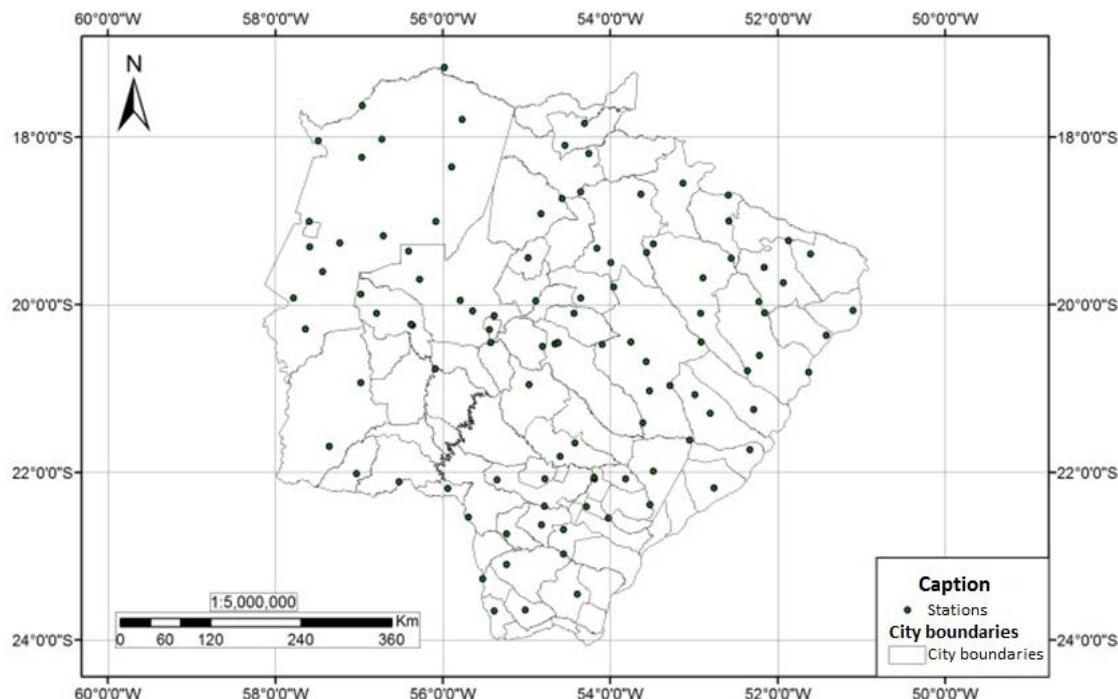


FIGURE 1. Spatial distribution of rainfall stations used in the study, in Mato Grosso do Sul State, Brazil.

For each pluviometric station the historical series of maximum annual values were set by applying multiplicative coefficients adjusted for the 24-hour rainfall disaggregation method and, after the procedure described above, obtaining the IDF equations of rainfall for each pluviometric station.

For spatial distribution of rainfall intensity data expected in Mato Grosso do Sul, we used ArcGIS software with the inverse interpolation of power distance (IPD), considering a 20-year return period, with 30 and 1440 min durations. Although agricultural projects often make hydrological predictions with a 10-year return period (SCHWAB et al., 1966, citado por PRUSKI, 2009; CRUCIANI, 1980), in studies in Southern Minas Gerais, the most advisable return period to implement hydroagricultural projects was 20 years (EUCLYDES, 1987).

RESULTS AND DISCUSSION

Figure 2 shows the frequency distribution of maximum annual rainfall observed and estimated using Gumbel model for Dourados-MS and Campo Grande, respectively. We might see that Gumbel distribution in the studied areas was adequate to estimate maximum rainfall, where there is good adhesion between observed and theoretical distribution.

Once Gumbel model adherence was verified, maximum annual intensities for 10, 30, 60, 120, 360 and 1440 minutes were estimated, considering 2, 5, 10, 20, 50 and 100 year return period. Table 2 presents the IDF equations for Dourados-MS and Campo Grande-MS, which relates duration and return period with maximum rainfall intensity expected, their respective determination coefficients and period analyzed.

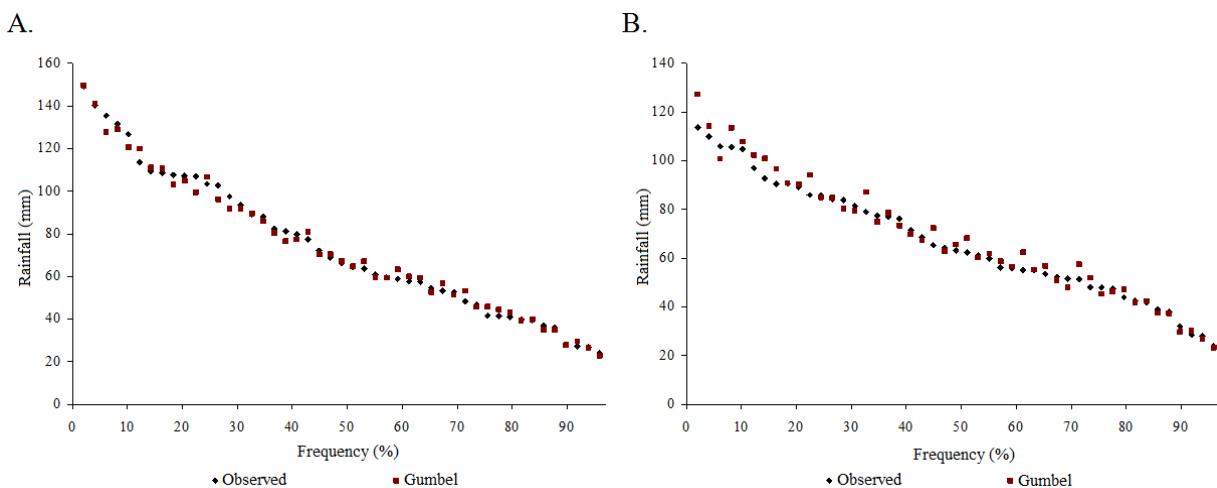


FIGURE 2. Frequency distribution of observed and estimated maximum rainfall by Gumbel model, wherein: a) Dourados-MS, Brazil; and b) Campo Grande-MS, Brazil.

Analyzing determination coefficient (r^2) in Table 2, we observed that generated equations allow calculating maximum rainfall intensity at different durations and return periods, with great accuracy.

TABLE 2. Intensity maximum average rainfall equations (i_m), in mm h^{-1} ; depending on the return period (T), in years; and rainfall duration (t), in minutes; for Dourados-MS and Campo Grande-MS, in Brazil.

Station	Equation	r^2	Analyzed period
Dourados	$i_m = \frac{2455.13 T^{0.18}}{(t + 28.14)^{0.88}}$	0.992	1979 - 1990
			1992 - 2010
Campo Grande	$i_m = \frac{2575.12 T^{0.16}}{(t + 19.87)^{0.93}}$	0.997	1973-1985
			1993-1998 2000-2009

Table 3 presents maximum rainfall intensities for 10, 30, 60, 120, 360 and 1440 minute durations within return periods of 2, 5, 10, 20, 50 and 100 years; which were obtained through pluviogram analysis (standard method), 24-hour rainfall disaggregation as proposed by DAEE/CETESB (1980), and multiplicative coefficients of the 24-hour method adjustment. They were applied to evaluate rainfall disaggregation method performance compared with standard method by means of relative mean error (EMR) and concordance index proposed by WILMOTT (1982).

The standard method achieved excellent performance with respect to Gumbel estimation, with average concordance index of 0.97 for Dourados, and amplitude from 0.94 (duration 1440 min) to 0.99 (durations of 10 and 30 min); and for Campo Grande, average of 0.99, and amplitude from 0.97 (duration 1440 min) to 0.99 (other durations).

The alternative method (proposed by DAEE/CETESB, 1980) compared with multiplicative coefficients adjusted according to standard method; we found better performance for adjusted coefficients in relation to alternative one. They reached an average concordance index of 0.93 for Dourados (amplitudes from 0.80 to 0.99, observed in 1440 and 120 min durations, respectively) and 0.96 for Campo Grande (amplitudes from 0.93 to 0.99, in 60 and 10 min durations, respectively).

TABLE 3. Analysis of rainfall intensities calculated by the ratio between intensity, duration and frequency, obtained by standard method (pluviograms analysis)-(IDF1); 24-hour rainfall disaggregation proposed by DAEE/CETESB (1980)-(IDF2); 24-hour rainfall disaggregation with coefficients - (IDF3); Relative Mean Error (RME) compared with Gumbel method; and concordance index (d), for stations in Dourados-MS and Campo Grande-MS, Brazil.

DOURADOS											
Duration (min)	RP (years)	GUMBEL (mm/h)	IDF1 (mm/h)	RME1 (%)	d	IDF2 (mm/h)	RME2 (%)	d	IDF3 (mm/h)	RME3 (%)	d
10	2	106.48	111.29	4.52		85.47	-23.20		116.81	4.96	
10	5	137.58	131.22	-4.63		105.53	-19.57		142.50	8.60	
10	10	158.18	148.63	-6.04	0.99	123.78	-16.72	0.93	165.62	11.43	0.91
10	20	177.93	168.35	-5.39	Great	145.18	-13.76	Great	192.50	14.34	Great
10	50	203.50	198.49	-2.46		179.26	-9.69		234.83	18.31	
10	100	222.67	224.83	0.97		210.25	-6.48		272.94	21.40	
30	2	70.08	76.67	9.40		51.52	-32.80		77.78	1.45	
30	5	91.37	90.40	-1.06		63.61	-29.63		94.89	4.96	
30	10	105.47	102.39	-2.91	0.99	74.61	-27.13	0.79	110.28	7.71	0.94
30	20	118.99	115.98	-2.53	Great	87.51	-24.54	Very	128.18	10.52	Great
30	50	136.49	136.74	0.19		108.05	-20.98	good	156.37	14.35	
30	100	149.60	154.89	3.54		126.74	-18.18		181.74	17.34	
60	2	45.77	53.08	15.97		34.32	-35.34		51.62	-2.75	
60	5	64.84	62.58	-3.49		42.37	-32.29		62.97	0.63	
60	10	77.47	70.89	-8.50	0.96	49.70	-29.89	0.75	73.19	3.26	0.97
60	20	89.58	80.29	-10.37	Great	58.29	-27.40	Good	85.07	5.95	Great
60	50	105.26	94.67	-10.07		71.98	-23.97		103.78	9.63	
60	100	117.01	107.23	-8.36		84.42	-21.27		120.62	12.49	
120	2	26.65	33.54	25.88		21.92	-34.64		30.70	-8.47	
120	5	38.29	39.55	3.30		27.07	-31.56		37.46	-5.29	
120	10	45.99	44.80	-2.60	0.98	31.75	-29.13	0.76	43.54	-2.82	0.99
120	20	53.39	50.74	-4.95	Great	37.24	-26.61	Very	50.60	-0.28	Great
120	50	62.95	59.83	-4.97		45.98	-23.15	Good	61.73	3.18	
120	100	70.12	67.76	-3.36		53.93	-20.42		71.74	5.87	
360	2	10.56	14.32	35.58		10.30	-28.08		11.56	-19.27	
360	5	15.33	16.88	10.11		12.71	-24.69		14.10	-16.47	
360	10	18.49	19.12	3.42	0.98	14.91	-22.01	0.87	16.39	-14.29	0.94
360	20	21.52	21.66	0.65	Great	17.49	-19.24	Ótimo	19.05	-12.05	Great
360	50	25.44	25.54	0.37		21.60	-15.43		23.24	-9.00	
360	100	28.38	28.92	1.92		25.33	-12.43		27.01	-6.62	
1440	2	2.94	4.42	50.44		3.84	-13.01		3.12	-29.42	
1440	5	4.37	5.21	19.11		4.74	-8.91		3.80	-26.98	
1440	10	5.32	5.90	10.81	0.94	5.57	-5.67	0.99	4.42	-25.07	0.80
1440	20	6.24	6.68	7.15	Great	6.53	-2.32	Ótimo	5.14	-23.11	Very
1440	50	7.42	7.88	6.22		8.06	2.29		6.27	-20.44	good
1440	100	8.30	8.92	7.49		9.45	5.92		7.29	-18.37	
CAMPO GRANDE											
Duration (min)	RP (years)	GUMBEL (mm/h)	IDF1 (mm/h)	RME1 (%)	d	IDF2 (mm/h)	RME2 (%)	d	IDF3 (mm/h)	RME3 (%)	d
10	2	108.54	123.25	13.55		88.07	-28.55		130.05	5.52	
10	5	140.34	142.56	1.58		101.76	-28.62		148.39	4.09	
10	10	161.39	159.15	-1.39	0.99	113.51	-28.68	0.65	163.97	3.03	0.99
10	20	181.59	177.68	-2.15	Great	126.62	-28.74	Medium	181.18	1.97	Great
10	50	207.73	205.51	-1.06		146.30	-28.81		206.73	0.59	
10	100	227.31	229.43	0.93		163.20	-28.87		228.43	-0.44	
30	2	75.20	76.63	1.91		53.08	-30.73		86.31	12.63	
30	5	92.59	88.64	-4.26		61.33	-30.81		98.48	11.11	
30	10	104.10	98.96	-4.94	0.99	68.42	-30.86	0.63	108.82	9.97	0.96
30	20	115.14	110.47	-4.05	Great	76.32	-30.92	Medium	120.24	8.84	Great
30	50	129.43	127.78	-1.28		88.18	-30.99		137.20	7.37	
30	100	140.15	142.65	1.79		98.36	-31.05		151.60	6.27	
60	2	48.14	49.52	2.87		35.35	-28.61		57.03	15.16	
60	5	58.69	57.28	-2.40		40.85	-28.68		65.07	13.61	
60	10	65.67	63.95	-2.63	0.99	45.57	-28.74	0.65	71.90	12.44	0.93
60	20	72.37	71.39	-1.36	Great	50.83	-28.80	Medium	79.45	11.29	Great
60	50	81.05	82.57	1.88		58.73	-28.87		90.66	9.79	
60	100	87.54	92.18	5.30		65.51	-28.93		100.17	8.67	
120	2	28.30	29.46	4.07		22.58	-23.34		33.70	14.40	
120	5	34.97	34.07	-2.56		26.09	-23.42		38.45	12.85	
120	10	39.38	38.04	-3.41	0.99	29.10	-23.49	0.72	42.49	11.70	0.94
120	20	43.61	42.46	-2.63	Great	32.46	-23.55	Good	46.94	10.55	Great
120	50	49.09	49.12	0.06		37.51	-23.63		53.57	9.06	
120	100	53.19	54.83	3.09		41.84	-23.69		59.19	7.94	
360	2	11.22	11.66	3.93		10.60	-9.11		12.51	7.23	
360	5	14.17	13.49	-4.76		12.25	-9.21		14.27	5.78	
360	10	16.12	15.06	-6.54	0.99	13.66	-9.28	0.95	15.77	4.70	0.99
360	20	17.99	16.82	-6.50	Great	15.24	-9.35	Great	17.43	3.62	Great
360	50	20.40	19.45	-4.68		17.61	-9.45		19.88	2.22	
360	100	22.22	21.71	-2.27		19.65	-9.52		21.97	1.18	
1440	2	3.35	3.35	-0.06		3.95	18.12		3.14	-6.25	
1440	5	4.20	3.87	-7.83		4.57	17.99		3.58	-7.52	
1440	10	4.77	4.32	-9.28	0.97	5.10	17.90	0.86	3.96	-8.46	0.94
1440	20	5.31	4.83	-9.04	Great	5.69	17.80	Great	4.37	-9.40	Great
1440	50	6.01	5.58	-7.05		6.57	17.68		4.99	-10.62	
1440	100	6.53	6.23	-4.57		7.33	17.58		5.51	-11.54	

Table 4 lists multiplicative coefficients adjusted for application of the 24-hour rainfall disaggregation method to be practiced in Mato Grosso do Sul. The results obtained showed great performance based on relative mean error (RME), concordance index, and model performance analysis criterion (Table 3).

TABLE 4. Proposition of rainfall disaggregation coefficients of rain data for Mato Grosso do Sul State, Brazil.

Duration	1440min/24h	720min/24h	360min/24h	240min/24h	180min/24h	120min/24h
Coefficient	1.14	0.94	0.88	0.82	0.79	0.74
Duration	60min/24h	50min/24h	40min/24h	30min/24h	20min/24h	10min/24h
Coefficient	0.63	0.60	0.55	0.49	0.39	0.24

The 24-hour rainfall disaggregation method proposed by DAEE/CETESB (1980) resulted, in general, in an underestimation of maximum rainfall intensity for both locations, except for 1440 min duration, which showed a differentiated behavior. This fact provides less security for hydro-agricultural projects but, on the other hand, it decreases cost on project implementation.

The adjusted coefficients were used to estimate equation parameters that relate intensity, duration and frequency for various locations in Mato Grosso do Sul State (Table 5). There was good adjustment of intense rainfalls equations, with r^2 values above 0.98.

We found a significant variation within the fitted equation parameters. **K** parameter presented a variation of 84.5%, ranging from 4905.22, in Ribas do Rio Pardo town (Code: 2153002), to 9048.45 in Cassilândia town (Code: 1951004). **A** values showed a 133% variation, with values from 0.13 (Chapadão do Sul, Code: 1852002) to 0.31 (Cassilândia, Code: 1951004).

Parameters **b** and **c** of the IDF adjusted equation presented the smallest variations, which were 3.6% and 1.7%, with amplitudes from 32.21 (Coxim, Code: 1855000) to 33.37 (Camapuã, Code: 1954006), and from 1.05 (Ribas do Rio Pardo, Code: 2153002) to 1.07 (Camapuã, Code: 1954006), respectively.

Parameters of rainfall intensity equation had great variability what highlights the need for local information attainment to perform studies and hydraulic projects. This fact shows that neighboring station use, for places that do not have the adjusted equation, interferes with the dimensioning safety and cost of projects (PEREIRA et al., 2007; SILVA et al., 2002;).

The results obtained with the spatial distribution of intense rainfall (Figure 3) were made only for the 20-year-return period, with durations of 30 and 1440 min, because according to EUCLYDES (1987), this period is the most recommended for hydro-agricultural project implementation. Thus, the longer the return period, the greater the values of maximum intensities found and, therefore, the greater the safety and cost of the project.

We observed lower values of maximum rainfall intensities in Eastern State analyzing Figure 3, with increasing behavior towards Western direction reaching 290 mm h⁻¹ (20-year-return period and 30-minute duration) and 10.6 mm h⁻¹ (1440-minute). ARAI et al. (2012) identified this same characterization for a basin located in South-Central Mato Grosso do Sul State.

TABLE 5. Maximum rainfall intensity equation coefficients K, a, b and c for 105 rainfall stations located in Mato Grosso do Sul State and respective determination coefficients (r^2).

Code	Latitude	Longitude	Alt.(m)	K	a	b	c	r^2	Years
1754004	17° 49' 51" 54° 18' 47"	268	5690.780.1632.381.050.99	35					
1755001	17° 47' 25" 55° 46' 25"	134	7766.550.2632.541.050.99	35					
1755004	17° 10' 00" 55° 59' 00"	122	7428.200.1932.801.050.99	19					
1756002	18° 01' 15" 56° 43' 55"	110	7352.410.2332.521.050.99	28					
1756003	17° 37' 24" 56° 57' 54"	101	6993.540.2632.621.050.99	37					
1852002	18° 59' 52" 52° 35' 17"	570	6127.410.1332.631.050.99	30					
1852003	18° 41' 30" 52° 35' 38"	721	7140.000.2732.621.050.99	30					
1853002	18° 11' 26" 54° 15' 28"	316	5519.450.1632.921.060.99	31					
1853004	18° 32' 50" 53° 08' 07"	635	5701.190.1732.701.060.99	30					
1853005	18° 40' 47" 53° 38' 16"	392	7169.110.2532.671.060.99	29					
1854001	18° 05' 55" 54° 32' 50"	113	6401.780.1832.801.060.99	36					
1854002	18° 54' 36" 54° 49' 56"	340	6552.890.1632.831.060.99	30					
1854003	18° 38' 57" 54° 21' 26"	250	5770.010.1832.301.050.99	34					
1854006	18° 43' 49" 54° 34' 43"	223	6590.390.1932.631.060.99	28					
1855000	18° 21' 00" 55° 51' 00"	138	6273.490.1532.211.050.99	12					
1857001	18° 02' 25" 57° 29' 27"	111	6292.930.2232.591.050.99	29					
1857002	18° 14' 11" 56° 58' 23"	103	5799.700.1932.511.050.99	27					
1951003	19° 23' 27" 51° 36' 32"	458	5856.280.1832.491.050.99	30					
1951004	19° 13' 45" 51° 51' 52' 30"	734	9048.450.3132.601.050.98	30					
1951005	19° 44' 11" 51° 56' 01"	502	5946.470.2132.781.060.99	30					
1952000	19° 26' 39" 52° 33' 30"	370	5993.000.2232.761.060.99	30					
1952001	19° 40' 41" 52° 53' 47"	471	5936.060.2032.901.060.99	30					
1952002	19° 33' 13" 52° 09' 59"	401	5834.670.1632.631.050.99	30					
1952003	19° 57' 48" 52° 13' 34"	300	6176.710.1832.651.050.99	28					
1953000	19° 22' 37" 53° 34' 11"	447	6013.690.2032.371.050.99	30					
1953001	19° 47' 05" 53° 57' 50"	524	5471.100.1832.671.060.99	30					
1953003	19° 16' 19" 53° 29' 27"	571	5963.150.1732.341.050.99	30					
1954002	19° 57' 09" 54° 53' 34"	259	5418.410.1632.361.050.99	33					
1954003	19° 26' 23" 54° 59' 00"	233	6018.500.2132.811.060.99	33					
1954004	19° 29' 48" 53° 59' 48"	404	6234.040.1832.291.050.99	35					
1954005	19° 55' 04" 54° 21' 31"	456	6327.620.1832.631.050.99	32					
1954006	19° 19' 20" 54° 09' 40"	357	7003.090.1933.371.070.99	30					
1955000	19° 56' 41" 55° 47' 40"	130	7152.430.2132.281.050.99	31					
1956001	19° 10' 24" 56° 42' 44"	96	5984.280.2332.401.050.99	34					
1956003	19° 41' 48" 56° 16' 58"	103	6852.030.1632.961.060.99	32					
1956004	19° 00' 12" 56° 05' 20"	123	6252.520.1832.451.050.99	34					
1956005	19° 52' 15" 56° 59' 01"	133	6481.440.2232.461.050.99	34					
1956008	19° 21' 33" 56° 24' 33"	105	6665.920.2132.841.060.99	31					
1957002	19° 00' 21" 57° 36' 07"	126	6002.670.2332.921.060.99	18					
1957003	19° 15' 30" 57° 14' 07"	86	6783.760.1832.561.050.99	30					
1957004	19° 55' 07" 57° 47' 22"	83	5944.540.1932.571.050.99	33					
1957005	19° 18' 19" 57° 35' 36"	97	7430.450.2432.791.060.99	30					
1957006	19° 36' 03" 57° 26' 17"	83	5994.500.2232.411.050.99	34					
205103720	19° 48' 00" 51° 38' 00"	260	6132.640.2032.931.060.99	34					
2051045	20° 21' 49" 51° 25' 26"	348	5618.300.1432.701.060.99	30					
2051046	20° 04' 06" 51° 06' 13"	375	5294.070.1733.071.060.99	30					
2052002	20° 26' 43" 52° 55' 08"	292	5921.580.1932.481.050.99	37					
2052003	20° 06' 07" 52° 55' 33"	376	6324.520.1932.851.060.99	30					
2052004	20° 36' 10" 52° 13' 06"	391	5496.570.1932.611.050.99	30					
2153003	21° 58' 56" 53° 26' 20"	374	5325.190.1732.751.060.99	29					
2153004	21° 01' 22" 53° 32' 13"	383	5347.920.1732.921.060.99	29					
2154000	21° 38' 50" 54° 25' 31"	287	5670.430.2132.721.060.99	41					
2154001	21° 48' 22" 54° 36' 11"	321	6120.840.2232.551.060.99	41					
2157005	21° 41' 20" 57° 21' 35"	213	7146.460.2032.861.060.99	32					
2252000	22° 11" 52° 42" 48"	284	6568.710.1732.721.060.99	41					
2253000	22° 22' 59" 53° 31' 51"	341	5593.330.1532.821.060.99	25					
2253015	22° 32' 42" 54° 01' 40"	275	5761.190.1832.391.050.99	28					
2254000	22° 37' 28" 54° 49' 29"	454	6137.530.1932.831.060.99	36					
2254001	22° 23' 53" 54° 47' 30"	293	6149.910.1732.671.060.99	41					
2254003	22° 24' 21" 54° 14' 07"	422	6546.290.1732.521.050.99	29					
2254004	22° 04' 31" 54° 11' 21"	303	6386.580.2032.731.060.99	29					
2254005	22° 04' 29" 54° 47' 02"	342	6127.710.1832.591.050.99	29					
2255001	22° 32' 00" 55° 42" 00"	658	5852.480.2432.741.050.99	12					
2255002	22° 11" 55° 56" 37"	691	7631.350.1732.571.050.99	29					
2255003	22° 43' 55" 55° 14' 32"	357	6546.290.1732.521.050.99	29					
2255004	22° 05' 10" 55" 21' 10"	493	6168.350.1833.001.060.99	29					
2256001	22° 06' 36" 56" 31' 39"	185	7250.710.1732.661.050.99	32					
2257000	22° 00' 51" 57" 01' 56"	232	7178.650.2032.611.050.99	33					
2353048	22° 04' 22" 53" 49' 14"	303	6395.670.1732.611.050.99	29					
2354000	22° 03' 28" 54" 11' 38"	366	6502.950.1832.431.050.99	41					
2354001	22° 40' 55" 54" 33' 42"	333	5813.080.1932.431.050.99	40					
2354002	22° 58' 13" 54" 33' 48"	307	5959.360.1832.321.050.99	40					

The decrease in the values of annual maximum intensities with increase in rainfall duration is also evident in Figure 3, which is typical for rains, since rainfall intensity tends to decrease with increased durations.

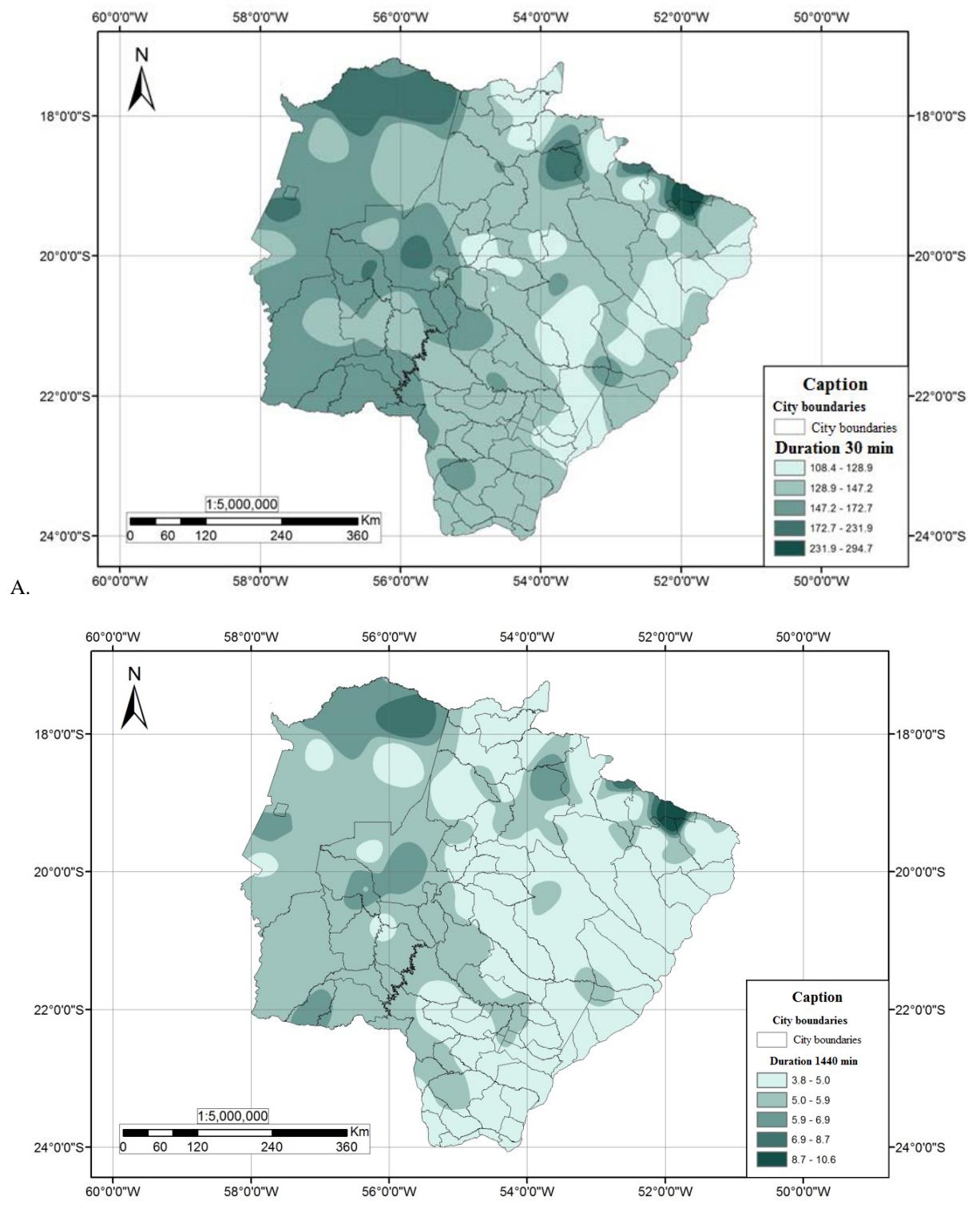


FIGURE 3. Spatial distribution of maximum rainfall (mm h^{-1}) for Mato Grosso do Sul State, with a 20-year return period, wherein: a) 30-min duration; and b) 1440-min duration.

CONCLUSIONS

Intense rainfall equations obtained through pluviogram analysis present great adjustments with determination coefficients above 99%;

The 24-hour rainfall disaggregation method with adjusted coefficients presented excellent performance when compared to pluviogram analysis;

The 24-hour rainfall disaggregation method with original coefficients tends to underestimate maximum rainfall intensities in Mato Grosso do Sul State, Brazil; and

The highest rainfall intensities foreseen for Mato Grosso do Sul occur in Western State and the lowest ones in Eastern area.

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