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# USE OF CONTINUED ITERATION ON THE REDUCTION OF ITERATIONS OF THE INTERIOR POINT METHOD

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ABSTRACT. Interior point methods have been widely used to determine the solution of large-scale linear programming problems. The predictor-corrector method stands out among all variations of interior point methods due to its efficiency and fast convergence. In each iteration it is necessary to solve two linear systems to determine the predictor-corrector direction. Solving such systems corresponds to the step which requires more processing time, and therefore, it should be done efficiently. The most common approach to solve them is the Cholesky factorization. However, Cholesky factorization demands a high computational effort in each iteration. Thus, searching for effort reduction, the continued iteration is proposed. This technique consists in determining a new direction through projection of the search direction and it was inserted into PCx code. The computational results regarding medium and large-scale problems, have indicated a good performance of the proposed approach in comparison with the predictor-corrector method.

**Keywords**: interior point methods, linear programming, continued iteration.

## 1 INTRODUCTION

Linear programming is an optimization technique widely used due to its robustness, the efficiency of its algorithms and the large number of problems that can be formulated through it. The study of interior point methods for linear programming has been one of the most active areas of research in optimization in recent decades because of great advances described by Gondzio [12]. Among the variations of the interior point methods for the solution of linear programming problems, the predictor-corrector method presented by Mehrotra [15] has great prominence due to its efficiency and fast convergence. This is a primal-dual method that needs to solve two linear systems with the same symmetric positive definite matrix in each iteration. To solve these systems the most used approach is the Cholesky factorization. Thus, interior point methods present a critical step in its computational performance, since this factorization in most cases demands a large computational effort. Vavasis & Ye [19] propose an algorithm that follows the central path, using

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short steps or a layered least squares step, which return an exact optimum after a finite number of steps. Besides Mehrotra's correction direction [15], other technique which determine correction directions have been developed over the last decades to improve interior point methods. Gondzio [5, 11] presented the multiple centrality corrections to interior point methods that consist in computing a direction so that  $x_i z_i$  belongs to the neighborhood of the central path [20], thereby enhancing convergence.

Jarre & Wechs [13] propose to generate corrector directions making use of recursion in a modification of Mehrotra's corrector direction. The idea is to change the residual vector  $r_a$  for another vector r in the linear system which computes the predictor direction. They question what the best choice would be for r to get a good search direction. In general, it is not easy to find a good value for r. So, they propose to find a subspace spanned by k different directions,  $(dx^1, dy^1, dz^1), \ldots, (dx^k, dy^k, dz^k)$ , generated for each  $r^1, r^2, \ldots, r^k$ , where each one of these directions is a predictor-corrector type. They formulate a small linear subproblem to find the best combination of weights in the generated directions to increase the stepsize and the reduction of the complementarity gap.

Mehrotra & Li [16] follow the approach of Jarre & Wechs [13]. They found multiple corrector directions by using information generated by a suitable Krylov subspace. The affine-scaling direction  $(\tilde{d}x, \tilde{d}y, \tilde{d}z)$ , the Mehrotra's corrector direction  $(\bar{d}x, \bar{d}y, \bar{d}z)$  and the first k directions  $(dx^1, dy^1, dz^1), \ldots, (dx^k, dy^k, dz^k)$  generated by Krylov subspace are combined with appropriate weights. Thus a linear programming problem is solved to determine the best set of weights in the combined search direction.

Numerical experiments have shown that direct methods provide sufficiently accurate solutions for interior point methods to achieve fast convergence regardless the ill-conditioning involved [1]. Such results are also supported by theory [20]. However, iterative methods have good accuracy when applied to well-conditioning systems or when preconditioners, as proposed by Oliveira & Sorensen [18], are used for an ill-conditioning system [12]. The direct methods take advantage of the factorization already computed to determine the solution of additional linear systems, but using iterative methods this advantage is lost.

We present in Section 3 an alternative technique to improve the predictor-corrector interior point method as [12, 13, 16], using direct methods. Inspired by the original continued iteration proposal presented on [17] for the dual affine-scaling method, we present the continued iteration for the predictor-corrector interior point method. The technique is incorporated in the predictor-corrector method in order to reduce the total number of iterations required to solve a linear programming problem.

The continued iteration consists in determining a new projection direction. Additionally, to take advantage of the Cholesky factorization already computed, the new direction is found by minimizing the deviation from the original rescaled direction. This technique is used when an iteration of the predictor-corrector method is completed.

This paper is organized as follows: In Section 2, we define the linear programming problem and describe, briefly, the primal dual interior point method. In Sections 3 and 4, the continued iteration is presented and incorporated into the predictor-corrector interior point method for linear programming problems, whether with bounded variables or not. Section 5 shows the results of computational experiments conducted with several problems selected from different collections. Finally, in Section 6, the conclusions are presented.

## 2 INTERIOR POINT METHODS

The linear programming problem in standard form is given by:

$$\begin{array}{ll}
\min & c^T x \\
\text{s.t.} & Ax = b \\
& x \ge 0,
\end{array} \tag{1}$$

in which  $A \in \mathbb{R}^{m \times n}$ , rank(A) = m,  $x \in \mathbb{R}^n$ ,  $c \in \mathbb{R}^n$  and  $b \in \mathbb{R}^m$ .

The problem (1) is called primal problem. The dual problem, associated with it, is given by:

$$\begin{array}{ll}
\max & b^T y \\
\text{s.t.} & A^T y + z = c \\
& z > 0.
\end{array} \tag{2}$$

in which  $y \in \mathbb{R}^m$  represents the vector of free dual variables and  $z \in \mathbb{R}^n$  represents the slack dual variables.

The first order optimality conditions (Karush-Kuhn-Tucker) of problems (1) and (2) are given by [20]:

$$Ax - b = 0$$

$$A^{T}y + z - c = 0$$

$$XZe = 0$$

$$(x, z) \ge 0,$$
(3)

in which X = diag(x), Z = diag(z) and  $e \in \mathbb{R}^n$ , such that  $e = (1.1..., 1)^T$ .

# 2.1 Primal-Dual Affine-Scaling Interior Point Method

The primal-dual affine-scaling method entails applying Newton's method to F(x, y, z) = 0, which is formed by the optimality conditions (3), ignoring  $(x, z) \ge 0$ , but starting from an interior point (x, z) > 0. Thus, the primal and dual problems are solved simultaneously. The affine-scaling direction is obtained by solving the linear system given below:

$$\begin{bmatrix} A & 0 & 0 \\ 0 & A^T & I \\ Z & 0 & X \end{bmatrix} \begin{bmatrix} \tilde{d}x \\ \tilde{d}y \\ \tilde{d}z \end{bmatrix} = \begin{bmatrix} r_p \\ r_d \\ r_a \end{bmatrix}, \tag{4}$$

in which  $r_p = b - Ax$ ,  $r_d = c - A^t y - z$  and  $r_a = -XZe$ .

We use variables substitution to determine the solution of (4). By eliminating the variable  $d\tilde{z} = X^{-1}(r_a - Z\tilde{d}x)$ , we obtain the augmented system:

$$\left[\begin{array}{cc} -D^{-1} & A^t \\ A & 0 \end{array}\right] \left[\begin{array}{c} \tilde{d}x \\ \tilde{d}y \end{array}\right] = \left[\begin{array}{c} r_1 \\ r_p \end{array}\right],$$

in which  $D = XZ^{-1}$  and  $r_1 = r_d - X^{-1}r_a$ . Now eliminating  $\tilde{d}x = D(A^t\tilde{d}y - r_1)$ , the following symmetric and positive definite normal equations system is obtained

$$ADA^{T}\tilde{d}y = r_p + ADr_1. (5)$$

As  $ADA^T$  is symmetric positive definite, the most used approach for solving system (5) is the Cholesky factorization [9].

The primal  $\alpha_P$  and dual  $\alpha_D$  stepsize, to keep the interior point in each iteration are given by:

$$\begin{aligned} \alpha_P &= \min \left\{ 1, \tau \min_t \left\{ -\frac{x_t}{\tilde{d}x_t} | x_t + \tilde{d}x_t \le 0 \right\} \right\}, \\ \alpha_D &= \min \left\{ 1, \tau \min_t \left\{ -\frac{z_t}{\tilde{d}z_t} | z_t + \tilde{d}z_t \le 0 \right\} \right\}, \end{aligned}$$

in which  $\tau \in (0, 1)$ .

**Remark 2.1.** In the primal-dual affine-scaling method, the products  $x_i z_i$  of  $r_a$  can converge to zero at different speeds. Thus, the method may fail or progress slowly. To avoid this, the parameter  $(\mu)$  is added to the optimality conditions so that  $x_i z_i = \mu$ , which is updated every iteration and tends to zero as the method approximates to a solution.

#### 2.2 Predictor-Corrector Interior Point Method

The predictor-corrector method presented by Mehrotra [15] consists in using a direction that contains three components: the affine-scaling direction, the centering direction and the non-linear correction direction. The affine-scaling direction is determined by (4). The centering direction is computed to prevent products  $x_i z_i$  from  $r_a$  converging to zero at different speeds as mentioned in Remark (2.1). Mehrotra [15] presents a proposal for computing  $\mu$ .

When  $\alpha_P = \alpha_D = 1$ , the primal and dual constraints are satisfied, but the complementary products have  $x_i z_i = \tilde{d} x_i \tilde{d} z_i$ , then a non-linear correction direction is computed. Consider,  $\tilde{D} x = diag(\tilde{d}x)$  and  $\tilde{D} z = diag(\tilde{d}z)$ , the corrector direction  $\bar{d}$  is the combination of the centering and the non-linear correction direction, which is obtained by solving:

$$\begin{bmatrix} A & 0 & 0 \\ 0 & A^T & I \\ Z & 0 & X \end{bmatrix} \begin{bmatrix} \bar{d}x \\ \bar{d}y \\ \bar{d}z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ \mu e - \tilde{D}x\tilde{D}ze \end{bmatrix}.$$
 (6)

Thus, the (d) predictor-corrector direction, given by the sum of two directions found, i.e.,  $d = \tilde{d} + \bar{d}$ , can be interpreted as a solution of the linear system:

$$\begin{bmatrix} A & 0 & 0 \\ 0 & A^T & I \\ Z & 0 & X \end{bmatrix} \begin{bmatrix} dx \\ dy \\ dz \end{bmatrix} = \begin{bmatrix} r_p \\ r_d \\ r_s \end{bmatrix}, \tag{7}$$

in which  $r_s = r_a + \mu e - \tilde{D}x\tilde{D}ze$ . Solving the system (7), the predictor-corrector direction is given by:

$$dy = (ADA^{T})^{-1}[r_{p} + AD(r_{d} - X^{-1}r_{s})],$$

$$dx = D(A^{T}dy - r_{d} + X^{-1}r_{s}),$$

$$dz = X^{-1}(r_{s} - Zdx).$$
(8)

Note that, the most expensive step is solving a linear system with the same matrix  $ADA^T$ . The Cholesky factorization is used and it has been already computed to obtain the affine-scaling direction.

Therefore the predictor-corrector method is an iterative method that starts from an interior point  $(x^0, y^0, z^0)$  by computing a new point:

$$x^{k+1} = x^k + \alpha_P dx^k,$$

$$y^{k+1} = y^k + \alpha_D dy^k,$$
  
$$z^{k+1} = z^k + \alpha_D dz^k.$$

in which  $(dx^k, dy^k, dz^k)$  is given in (8) and k varies from 0 to a maximum number of iterations.

# 2.2.1 Stopping criteria

Consider  $\varepsilon_p$ ,  $\varepsilon_d$ ,  $\varepsilon_o$  primal feasibility, dual feasibility and optimality tolerances, respectively, then the stopping criteria is given by:

$$\frac{||r_p^k||_2}{1+||b||_2} \le \varepsilon_p,$$

$$\frac{||r_d^k||_2}{1+||c||_2} \le \varepsilon_d,$$

$$\frac{(x^k)^T z^k}{1 + |c^T x^k|} \le \varepsilon_o.$$

For further details on the predictor-corrector interior point methods see [14, 15, 19].

#### 3 CONTINUED ITERATION

The continued iteration is proposed in order to reduce the total number of predictor-corrector interior point method iterations, and consequently, reduce the total computational time. This iteration determines a new direction, after computing the predictor-corrector step, without being necessary to perform a new Cholesky factorization. The new direction is determined by setting some of its components to zero and thus, the deviation from the predictor-corrector direction is kept to a minimum. Furthermore, the Cholesky factorization of  $ADA^{I}$ , already computed in the predictor-corrector method iteration, is used again for solving the linear systems involved. Therefore, the computing of this new direction is not very expensive in comparison with a new predictor-corrector method iteration. This new direction is called continued predictor-corrector direction.

# 3.1 Computing the continued predictor-corrector direction

The continued predictor-corrector direction is computed in an analogous way to the computing of the predictor-corrector direction. Initially, the continued affine-scaling direction is computed, after that the centering and nonlinear correction direction is computed. More details on these directions will be seen later, because before that we need to define the blocking components.

The components that must be fixed at zero, in the new direction, are those responsible for blocking in the previous direction. The blocking components in the directions (dx, dz) are given by:

$$i = \arg\min_{t} \left\{ -\frac{x_t^k}{dx_t^k} | x_t^k + dx_t^k \le 0 \right\},$$

$$j = \arg\min_{t} \left\{ -\frac{z_t^k}{dz_t^k} | z_t^k + dz_t^k \le 0 \right\}.$$
(9)

As blocking component in any or both directions may not exist, some likely cases can be considered: two, one or none blocking component.

**Remark 3.1.** If there is more than one blocking component i or j, only the first blocking determined component is considered in this study. When there is no blocking component, the continued iteration is not performed.

In the original proposal of continued iteration to the predictor-corrector method only one of the blocking components was fixed at zero [3]. In this work, the two blocking components (i and j) are fixed at zero.

# 3.1.1 Two blocking components

In the continued affine-scaling direction, in which  $\tilde{d}$  is to be computed, the components that perform blocking in the previous direction are fixed at zero, thus, we get:

$$\tilde{d}x_i = 0 \text{ and } \tilde{d}z_i = 0, \tag{10}$$

which are additional conditions to the linear system (4). We compute  $\tilde{d}$  approximately, since linear system (4) admits a unique solution. In addition, we are imposing new conditions (10) to such system.

Similarly to the idea of Dikin [7] by developing the primal affine-scaling method, we find the solution of this system using an auxiliary problem to determine  $\tilde{d}x$ . The auxiliary problem is built using (10) and the first equation of (4). The component  $\tilde{d}x_j$  corresponding to  $\tilde{d}z_j$  is computed using the third equation of (4), in which the value must be  $-x_j$ . We formulate a problem that determines  $\tilde{d}x$  rescaling the new direction and minimizing the deviation in relation to the original rescaled direction, so that the Cholesky factorization is already computed and used. The problem is given by:

min 
$$\frac{1}{2} \|D^{-\frac{1}{2}} \tilde{d}x - D^{-\frac{1}{2}} dx\|^2$$
s.t. 
$$A\tilde{d}x = r_p$$

$$\tilde{d}x_i = \beta_a$$

$$\tilde{d}x_j = \beta_b,$$
(11)

in which  $D = Z^{-1}X$ ,  $\tilde{d}x$ ,  $dx \in \mathbb{R}^n$ ,  $\beta_a = 0$ , and  $\beta_b = -x_i$ .

Consider: 
$$\theta_i = A_i^T (ADA^T)^{-1} A_i$$
,  $\theta_j = A_j^T (ADA^T)^{-1} A_j$  and  $\theta_{ij} = A_i^T (ADA^T)^{-1} A_j$ .

Since the problem (11) is quadratic, we find the solution to this problem using the Lagrangian function, which is given by:

$$\tilde{d}x = dx - DA^T v - \alpha d_{ii} e_i - \gamma d_{jj} e_j,$$

in which

$$v = -\alpha d_{ii} (ADA^{T})^{-1} A_{i} - \gamma d_{jj} (ADA^{T})^{-1} A_{j},$$

$$\alpha = \frac{dx_{i} - \beta_{a} + \gamma d_{ii} d_{jj} \theta_{ij}}{d_{ii} (1 - d_{ii} \theta_{i})},$$

$$\gamma = \frac{dx_{j} - \beta_{b} + \left[\frac{(dx_{i} - \beta_{a})d_{jj} \theta_{ij}}{1 - d_{ii} \theta_{i}}\right]}{d_{jj} \xi},$$

$$\xi = 1 - \left[\frac{d_{ii} d_{jj} \theta_{ij}^{2}}{1 - d_{ii} \theta_{i}}\right] - d_{jj} \theta_{j}.$$

$$(12)$$

From the last two equations of (4), and using least squares in the overdetermined system to compute  $\tilde{d}y$ , we find the remaining directions given by:

$$\tilde{d}z = X^{-1}(r_a - Z\tilde{d}x), 
\tilde{d}y = (ADA^T)^{-1}AD(r_d - \tilde{d}z).$$
(13)

**Remark 3.2.** The continued affine-scaling direction computation implies solving three linear systems with  $ADA^{T}$ . We solve two linear systems: one to obtain v in (12) and another to get  $\tilde{d}y$  in (13).

Given the continued affine-scaling direction, when performing the centering and non-linear correction, we obtain continued predictor-corrector direction, similarly as done in the predictor-corrector method (2.2). Keeping the components that block at zero, in direction  $\hat{d}$  we should have:

$$\hat{d}x_i = 0 \text{ and } \hat{d}z_i = 0. \tag{14}$$

Furthermore, the direction  $\hat{d}$  should be an approximate solution of the linear system (7). We determine  $\hat{d}$  in a similarly way to determine the continued affine-scaling direction described above. However in auxiliary problem (11) there is an change in the value  $\beta_b$  due to the computing of centering and non-linear correction. If  $\hat{d}z_j = 0$ , we find the value of the component  $\hat{d}x_j$  corresponding to the last equation of (7). Then, the auxiliary problem, in this case, is given by:

min 
$$\frac{1}{2} \|D^{-\frac{1}{2}} \hat{d}x - D^{-\frac{1}{2}} dx\|^2$$
  
s.t.  $A \hat{d}x = r_p$  (15)  
 $\hat{d}x_i = \beta_a$   
 $\hat{d}x_j = \beta_b$ ,

in which  $D = Z^{-1}X$ ,  $\hat{d}x$ ,  $dx \in \mathbb{R}^n$ ,  $\beta_a = 0$  and  $\beta_b = -x_j + \frac{\mu}{z_j}$ .

Solving the problem (15), it is obtained:

$$\hat{d}x = dx - DA^{T}v - \alpha d_{ii}e_{i} - \gamma d_{jj}e_{j}.$$

We find the remaining directions in (7) by:

$$\hat{d}z = X^{-1}(r_s - Z\hat{d}x),$$
  
$$\hat{d}y = (ADA^T)^{-1}AD(r_d - \hat{d}z).$$

**Remark 3.3.** To determine the direction  $\hat{d}$  above it is not necessary to solve again the linear systems involving the matrix  $ADA^{t}$  to compute v. In fact, it is necessary to solve only a linear system with matrix  $ADA^{t}$  to determine  $\hat{d}v$ .

**Remark 3.4.** The computing of direction  $\hat{d}$  is analogous whether there is only one or two blocking components. That is, in (10) and (14) only one condition is considered. In the auxiliary problems (11) and (15), the restriction that has no blocking component is disregarded.

**Remark 3.5.** As the direction  $\hat{d}$  is determined in such a way that the change from the direction d is as low as possible, the stepsizes  $\hat{\alpha}_P$  and  $\hat{\alpha}_D$ , adopted are

$$\hat{\alpha}_P = \min\left\{\tau \min_t \left\{ -\frac{x_t}{\hat{d}x_t} | x_t + \hat{d}x_t \le 0 \right\}, 1 - \alpha_P \right\}$$

and

$$\hat{\alpha}_D = \min\left\{\tau \min_{t} \left\{ -\frac{z_t}{\hat{d}z_t} | z_t + \hat{d}z_t \le 0 \right\}, 1 - \alpha_D \right\}.$$

Thus,  $\hat{\alpha}_P + \alpha_P \in (0, 1]$  and  $\hat{\alpha}_D + \alpha_D \in (0, 1]$ . In [3], there is no limitation on the new stepsizes.

# 3.2 Criteria for using continued iteration

Consider  $\hat{r} = (\hat{r}_p, \hat{r}_d, \hat{r}_a)^t$ , formed by new residuals produced by the continued iteration e  $r = (r_p, r_d, r_a)^t$ . Given that the primal infeasibility, the dual infeasibility and/or the complementary products are reduced with continued iteration, then the continued direction only is used if  $||\hat{r}||_2 < \omega_1 ||r||_2$  in which  $\omega_1 \in (0, 1)$ . This is an improvement over the implementation described in [3].

## 4 CONTINUED ITERATION WITH BOUNDED VARIABLES

Consider the primal linear programming problem with bounded variables in its standard form:

min 
$$c^T x$$
  
s.t.  $Ax = b$   
 $x + s = u$   
 $x \ge 0, s \ge 0,$  (16)

in which  $s \in \mathbb{R}^n$  represents the slack of bounded variables, and  $u \in \mathbb{R}^n$  represents the upper bound of x.

The dual problem in its standard form associated with (16) is given by:

max 
$$b^T y - u^T w$$
  
s.t.  $A^T y + z - w = c$  (17)  
 $z \ge 0, \ w \ge 0,$ 

in which  $w \in \mathbb{R}^n$  represents the dual variables associated with the slack variables s.

The first order optimality conditions (Karush-Kuhn-Tucker) of the problems (16) and (17) are as follows:

$$Ax - b = 0$$

$$x + s - u = 0$$

$$A^{T}y + z - w - c = 0$$

$$XZe = 0$$

$$SWe = 0$$

$$(x, s) \ge 0$$

$$(z, w) \ge 0,$$

in which S = diag(s) and W = diag(w).

# 4.1 Computing the continued predictor-corrector direction

In this case, it is conducted the blocking components and they are given by the directions (dx, ds, dz, dw). The blocking components i and j in directions dx and dz are defined as in (9). Consequently, the blocking components in the directions ds, dw are defined by:

$$\begin{split} l_1 &= \arg\min_t \left\{ -\frac{s_t^k}{ds_t^k} | s_t^k + ds_t^k \leq 0 \right\}, \\ l_2 &= \arg\min_t \left\{ -\frac{w_t^k}{dw_t^k} | w_t^k + dw_t^k \leq 0 \right\}. \end{split}$$

The computing for determining the null components in the new direction is performed as follows.

Consider  $h = \min\{-x_i^k/dx_i^k, -s_{l_1}^k/ds_{l_1}^k\}$  and  $g = \min\{-z_j^k/dz_j^k, -w_{l_2}^k/dw_{l_2}^k\}$ . If  $h = -x_i^k/dx_i^k$ , then in the new direction  $\hat{d}x_i = 0$ . Otherwise, we assign  $i \leftarrow l_1$  and  $\hat{d}s_i = 0$ . If  $g = -z_j^k/dz_j^k$ , then in the new direction  $\hat{d}z_i = 0$ ; otherwise,  $j \leftarrow l_2$  and  $\hat{d}w_i = 0$ .

# **4.1.1** Two blocking components

With the given components, we have computed the continued affine-scaling direction  $\tilde{d}$  so that:

$$\tilde{d}x_i = 0 \text{ or } \tilde{d}s_i = 0,$$
  
 $\tilde{d}z_i = 0 \text{ or } \tilde{d}w_i = 0.$  (18)

Additionally, the continued affine-scaling direction should be an approximate solution of the linear system obtained when Newton's method is applied to the optimality conditions of the problem, being the corresponding linear system given by:

$$\begin{bmatrix} A & 0 & 0 & 0 & 0 \\ I & I & 0 & 0 & 0 \\ 0 & 0 & A^{T} & I & -I \\ Z & 0 & 0 & X & 0 \\ 0 & W & 0 & 0 & S \end{bmatrix} \begin{bmatrix} \tilde{d}x \\ \tilde{d}s \\ \tilde{d}y \\ \tilde{d}z \\ \tilde{d}w \end{bmatrix} = \begin{bmatrix} r_{p} \\ r_{u} \\ r_{d} \\ r_{a} \\ r_{b} \end{bmatrix},$$
(19)

in which  $\tilde{d}x$ ,  $\tilde{d}s$ ,  $\tilde{d}z$ ,  $\tilde{d}w \in \mathbb{R}^n$  and  $\tilde{d}y \in \mathbb{R}^m$ .

To determine the direction  $\tilde{d}$ , initially, we compute  $\tilde{dx}$  analogously to (3.1.1), using an auxiliary problem, which in this case is given by:

min 
$$\frac{1}{2} \|D^{-\frac{1}{2}} \tilde{d}x - D^{-\frac{1}{2}} dx\|^2$$
s.t. 
$$A\tilde{d}x = r_p$$

$$\tilde{d}x_i = \beta_a$$

$$\tilde{d}x_i = \beta_b,$$
(20)

in which  $D = (XZ^{-1} + SW^{-1})^{-1}$ ,

$$\beta_a = \begin{cases} 0, & \text{if } \tilde{d}x_i = 0; \\ (r_u)_i, & \text{if } \tilde{d}s_i = 0, \end{cases}$$

and

$$\beta_b = \begin{cases} -x_j, & \text{if } \tilde{d}z_j = 0; \\ (r_u)_j + s_j, & \text{if } \tilde{d}w_j = 0. \end{cases}$$

Problem (20) is similar to the problem (11), in which only the values  $\beta_a$  e  $\beta_b$  may change. Thus,

$$\tilde{d}x = dx - DA^T v - \alpha d_{ii} e_i - \gamma d_{jj} e_j.$$

For the remaining equations (19), we obtain:

$$\begin{split} \tilde{d}s &= r_u - \tilde{d}x, \\ \tilde{d}z &= X^{-1}(r_a - Z\tilde{d}x), \\ \tilde{d}w &= S^{-1}(r_b - W\tilde{d}s), \\ \tilde{d}y &= (ADA^T)^{-1}AD(r_d - \tilde{d}z + \tilde{d}w). \end{split}$$

The procedure performing centering and non-linear correction is similar to the case without bounds, thus obtaining the continued predictor-corrector direction.

**Remark 4.1.** When there is one blocking component, the direction computation is similar to (4.1.1). Furthermore, the equations related to the missing blocking component are disregarded in (18) and (20).

**Remark 4.2.** The criterion for using the continued iteration with bounded variables is similar to that given in (3.2); in this case,  $\hat{r} = (\hat{r}_p, \hat{r}_u, \hat{r}_d, \hat{r}_a, \hat{r}_b)^t$  and  $r = (r_p, r_u, r_d, r_a, r_b)^t$ .

#### 5 COMPUTATIONAL EXPERIMENTS

The computational experiments were performed on an Intel Core i7, 8 GB RAM, 1TB HD and Linux Operating System.

The continued iteration was implemented in language C and incorporated into the PCx code [6] with multiple centrality corrections turned off [11]. To analyze the performance of PCx with the proposed approach, the computational experiments were performed with free access problems belonging to Netlib [10], Kennington [4] and Qaplib [2] collection.

The PCx has a good behavior near a solution, thus the continued iteration was not used in the last iterations. Based on criteria defined in (2.2.1), the continued iteration is to be applied if:

$$\frac{x^t z + s^t w}{(1 + |c^t x|)} > \omega_2,$$

in which  $\omega_2 \in (0, 1)$ .

For the computational experiments  $\omega_1 = 10^{-7}$  in (3.2) and  $\omega_2 = 0.99$ .

Table 1 shows, in the first column, the name of the selected problems and in the second and third columns, are the dimension of the problems (number of rows and columns) after the preprocessing of the PCx. In the fourth column, there is the density of the Cholesky factor provided by PCx, which performs a reordering to obtain this sparse factor. The fifth column relates the number of variables with bounds (VB) for each problem. The last column indicates the collection to which the problem belongs.

Table 2 shows the results by incorporating the continued iteration into PCx code. The first column shows the tests problems. The second column presents the results obtained by PCx standard version without multiple centrality corrections. The third column has the results obtained by PCx with the continued iteration, which will be referred to as PCx-IC. The columns PCx and PCx-IC indicate the total number of iterations (k) performed by the interior point methods and running time in seconds (t). In addition, PCx-IC has the number of performed continued iterations (ic).

**Table 1** – Test problems.

Problem		Table 1 – 1es		st problems	· 		
DFL001         5984         12143         0.09132         13         Netlib           MAROS-R7         2152         7440         0.23023         0         Netlib           PILOT87         1971         6373         0.21863         1578         Netlib           STOCFOR3         15362         22228         0.00144         0         Netlib           CRE-B         5336         36382         0.01728         0         Kennington           KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         <	Problem		Dimension		VB	Collection	
MAROS-R7         2152         7440         0.23023         0         Netlib           PILOT87         1971         6373         0.21863         1578         Netlib           STOCFOR3         15362         22228         0.00144         0         Netlib           CRE-B         5336         36382         0.01728         0         Kennington           KEN1         10085         16740         0.02497         0         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS30         38722         106180         0.01357         <	DEL 001	l I		0.00122	10	NT .19	
PILOT87         1971         6373         0.21863         1578         Netlib           STOCFOR3         15362         22228         0.00144         0         Netlib           CRE-B         5336         36382         0.01728         0         Kennington           CRE-D         4102         28601         0.02497         0         Kennington           KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01357         33150         Kennington           PDS10         15648         48780         0.01377         51389         Kennington           PDS20         38722         106180         0.01363			_				
STOCFOR3         15362         22228         0.00144         0         Netlib           CRE-B         5336         36382         0.01728         0         Kennington           CRE-D         4102         28601         0.02497         0         Kennington           KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS40         64276         214385         0.01363<					_		
CRE-B         5336         36382         0.01728         0         Kennington           CRE-D         4102         28601         0.02497         0         Kennington           KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01							
CRE-D         4102         28601         0.02497         0         Kennington           KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0							
KEN11         10085         16740         0.00192         16740         Kennington           KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS40         64276         214385         0.01293         95668         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS70         111896         386238	CRE-B					Kennington	
KEN13         22534         36561         0.01130         36561         Kennington           KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS70         111896         386238		_	28601		0	_	
KEN18         78862         128434         0.00061         128434         Kennington           OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS90         139752         471538	KEN11	10085	16740	0.00192	16740	Kennington	
OSA-07         1081         25030         0.04747         0         Kennington           OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS100         152300         498530	KEN13	22534	36561	0.01130	36561	Kennington	
OSA-14         2300         54760         0.02255         0         Kennington           OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530	KEN18	78862	128434	0.00061	128434	Kennington	
OSA-30         4313         104337         0.01214         0         Kennington           OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149	OSA-07	1081	25030	0.04747	0	Kennington	
OSA-60         10243         243209         0.00497         0         Kennington           PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417<	OSA-14	2300	54760	0.02255	0	Kennington	
PDS06         9156         28472         0.01395         8448         Kennington           PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587	OSA-30	4313	104337	0.01214	0	Kennington	
PDS10         15648         48780         0.01372         15125         Kennington           PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           KRA30B         18059         85725	OSA-60	10243	243209	0.00497	0	Kennington	
PDS20         38722         106180         0.01357         33150         Kennington           PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725	PDS06	9156	28472	0.01395	8448	Kennington	
PDS30         47968         156042         0.01271         51389         Kennington           PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0	PDS10	15648	48780	0.01372	15125	Kennington	
PDS40         64276         214385         0.01363         72686         Kennington           PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR20         5079         15980         0.51710 <td>PDS20</td> <td>38722</td> <td>106180</td> <td>0.01357</td> <td>33150</td> <td colspan="2">Kennington</td>	PDS20	38722	106180	0.01357	33150	Kennington	
PDS50         80339         272513         0.01293         95668         Kennington           PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         <	PDS30	47968	156042	0.01271	51389	Kennington	
PDS60         96514         332862         0.01247         119785         Kennington           PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0<	PDS40	64276	214385	0.01363	72686	Kennington	
PDS70         111896         386238         0.01257         143325         Kennington           PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib	PDS50	80339	272513	0.01293	95668	Kennington	
PDS80         126120         430800         0.01185         165193         Kennington           PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qap	PDS60	96514	332862	0.01247	119785	Kennington	
PDS90         139752         471538         0.01136         186292         Kennington           PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	PDS70	111896	386238	0.01257	143325	Kennington	
PDS100         152300         498530         0.01036         206383         Kennington           CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	PDS80	126120	430800	0.01185	165193	Kennington	
CHR25A         8149         15325         0.07689         0         Qaplib           CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	PDS90	139752	471538	0.01136	186292	Kennington	
CHR22B         5587         10417         0.08850         0         Qaplib           ELS19         4350         13186         0.40664         0         Qaplib           KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	PDS100	152300	498530	0.01036	206383	_	
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KRA30A         18059         85725         0.51777         0         Qaplib           KRA30B         18059         85725         0.51777         0         Qaplib           ROU20         7359         37640         0.76870         0         Qaplib           SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	CHR22B	5587	10417	0.08850	0		
KRA30B       18059       85725       0.51777       0       Qaplib         ROU20       7359       37640       0.76870       0       Qaplib         SCR15       2234       6210       0.53284       0       Qaplib         SCR20       5079       15980       0.51710       0       Qaplib         STE36A       27683       131076       0.46092       0       Qaplib         STE36B       27683       131076       0.46092       0       Qaplib	ELS19	4350	13186	0.40664	0		
KRA30B     18059     85725     0.51777     0     Qaplib       ROU20     7359     37640     0.76870     0     Qaplib       SCR15     2234     6210     0.53284     0     Qaplib       SCR20     5079     15980     0.51710     0     Qaplib       STE36A     27683     131076     0.46092     0     Qaplib       STE36B     27683     131076     0.46092     0     Qaplib	KRA30A	18059	85725	0.51777	0		
ROU20     7359     37640     0.76870     0     Qaplib       SCR15     2234     6210     0.53284     0     Qaplib       SCR20     5079     15980     0.51710     0     Qaplib       STE36A     27683     131076     0.46092     0     Qaplib       STE36B     27683     131076     0.46092     0     Qaplib	KRA30B	18059	85725	0.51777	0	_	
SCR15         2234         6210         0.53284         0         Qaplib           SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	ROU20	7359	37640	0.76870	0		
SCR20         5079         15980         0.51710         0         Qaplib           STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib	SCR15		6210		0		
STE36A         27683         131076         0.46092         0         Qaplib           STE36B         27683         131076         0.46092         0         Qaplib		5079					
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						_	
31E30C   4/003   1310/0   0.40094   U   Uapiib	STE36C	27683	131076	0.46092	0	Qaplib	

**Table 2** – Comparison between PCx and PCx-IC.

	PCx		PCx-IC			
Problema	k	t	k	t	ic	
DFL001	56	18.34	54	18.17	6	
MAROS-R7	16	0.71	19	0.91	11	
PILOT87	33	1.80	35	1.91	17	
STOCFOR3	30	0.23	29	0.31	5	
CRE-B	41	0.88	45	1.10	6	
CRE-D	41	0.73	47	0.97	8	
KEN11	20	0.13	19	0.16	10	
KEN13	23	0.41	23	0.53	11	
KEN18	29	3.50	31	4.37	11	
OSA-07	22	0.13	22	0.18	8	
OSA-14	25	0.40	18	0.42	6	
OSA-30	24	0.96	18	1.06	10	
OSA-60	33	4.02	18	3.77	9	
PDS06	34	2.62	33	2.60	10	
PDS10	39	13.88	39	14.15	8	
PDS20	55	149.65	52	144.23	10	
PDS30	67	448.41	60	407.16	7	
PDS40	66	1223.58	64	1195.83	4	
PDS50	66	2115.27	71	2275.74	8	
PDS60	69	3695.15	69	3710.79	5	
PDS70	75	6298.36	70	5912.77	9	
PDS80	74	8890.05	71	8580.14	11	
PDS90	76	11275.48	76	11303.87	9	
PDS100	78	12841.34	77	12711.74	9	
CHR25A	28	11.49	26	11.07	1	
CHR22B	27	4.59	28	4.96	1	
ELS19	26	33.48	26	33.92	1	
SCR15	21	5.45	20	5.31	1	
SCR20	20	64.04	20	64.63	1	
ROU20	16	290.70	16	293.19	1	
KRA30A	26	3704.38	25	3585.43	2	
KRA30B	27	3841.13	28	3998.78	2	
STE36A	32	13191.43	31	12857.36	1	
STE36B	31	12801.62	31	12860.21	0	
STE36C	31	12808.24	30	12467.26	1	

In Table 2, we find 18 problems in which the number of iterations is reduced by PCx-IC. The PDS problems present the largest reductions in both of iterations and time by the proposed method. The OSA-60 problem has the highest iteration reduction ratio at 45%. Particularly in terms of time, the largest time reduction ratio stands at 7% in the PDS70 problem among the 14 problems displaying time reduction. As for the

problems that require more processing time whenever PCx-IC reduces the number of iterations the time is also reduced. However, there is no time reduction in the problems solved by PCx in a few seconds and with low reduction. This occurs due to the increased effort exerted by the continued iteration. Thus, excellent performance is obtained by PCx-IC in most large-scale problems regarding iterations reduction as well as for total computational effort.

Figure 1 shows the performance profile [8] by PCx and PCx-IC regarding the total number of iterations. Note that the method PCx-IC offers better performance compared with PCx. It solves 78% of the test problems with a smaller number of iterations.

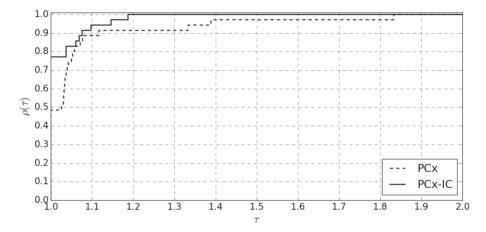
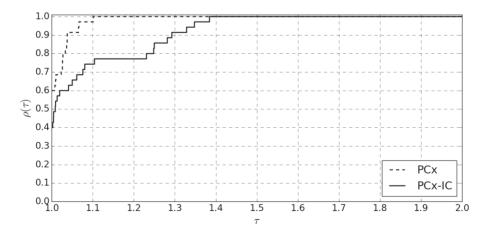


Figure 1 – Total number of iterations.

Figure 2 shows the performance profile of the methods considering the total running time as performance measure. In this case, PCx is the most efficient for approximately 60% of the test problems solved in less time. Moreover, both methods are robust for solving all tested problems.



**Figure 2** – Total time for solving problems.

## 6 CONCLUSIONS

In this study, the continued iteration has been proposed for the predictor-corrector interior point method with and without bounded variables. The main objective is to reduce the total number of predictor-corrector interior point method iterations and consequently, the total computational time. In the continued iteration, a new direction is determined, considering that some of its components are null according to the blocking component in the last computed direction. The continued predictor-corrector direction is determined by setting to zero some of its components and thus the deviation from the predictor-corrector direction is kept to a minimum. The Cholesky factorization, already computed in the predictor-corrector method iteration, is used again for solving the linear systems involved. Thus, it avoids computing a new Cholesky factorization. Then, the new method is applied on two levels. On the outer level, the Cholesky factorization and the traditional predictor-corrector direction are computed. On the inner level, a new direction employing the existing Cholesky factorization on the outer level is used by the continued iteration. The computational effort of each continued iteration is dominated by the solution of up to four linear systems with the same matrix already factored. The computational results show that the continued iteration reduces the number of iterations in most of the test problems. The problems that the PCx needs more time to solve also have their time reduced by PCx-IC. Although the continued iteration with the proposed direction has reduced the number of iterations in most problems, the extra effort per iteration to compute the new direction in smaller problems does not affect the reduction of total computational time. In future work other continued directions will be searched aiming to reduce the extra effort that such directions add in the predictor-corrector method.

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