BIOMECHANICAL ACCESS METHOD FOR ANALYZING ISOMETRICITY IN RECONSTRUCTING THE MEDIAL PATELLOFEMORAL LIGAMENT

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ABSTRACT

Objective: To present a biomechanical device for evaluating medial patellofemoral ligament (MPFL) reconstruction and its isometricity. Methods: An accessible biomechanical method that allowed application of physiological and non-physiological forces to the knee using a mechanical arm and application of weights and counterweights was developed, so as to enable many different evaluations and have a very accurate measurement system for distances between different structures, for analysis on experiments. This article describes the assembly of this system, and suggests some practical applications. Six cadaver knees were studied. The knees were prepared in a testing machine developed at the Biomechanics Laboratory of IOT-HCFMUSP, which allowed dynamic evaluation of patellar behavior, with quantification of patellar lateralization be-

tween 0° and 120°. The differences between the distances found with and without load applied to the patella were grouped according to the graft fixation angle (0°, 30°, 60° or 90°) and knee position (intact, damaged or reconstructed). Results: There was a tendency for smaller lateral displacement to occur at fixation angles greater than 30 degrees of flexion, especially between the angles of 45° and 60° degrees of flexion, after the reconstruction. For the other angles, there was no statistical significance. Conclusion: The method developed is a useful tool for studies on the patellofemoral joint and the MPFL, and has a very accurate measurement system for distances between different structures. It can be used in institutions with fewer resources available

Keywords - Knee/surgery; Joint Instability; Biomechanics; Patellar Ligament

INTRODUCTION

The medial patellofemoral ligament (MPFL) has been documented as the greatest restrictor of lateral translation of the patella⁽¹⁻³⁾. In most patients, the MPFL is ruptured during acute dislocation of the patella^(4,5). For this reason, a large number of surgical techniques for treating patellar instability have been described⁽⁶⁾.

Starting in the 1990s, a growing number of studies dealing specifically with reconstruction of the MPFL appeared in the literature⁽⁷⁻¹⁶⁾. Reconstruction of this ligament has been shown to be an excellent alterna-

tive for restoring both the anatomy and the function of the medial patellofemoral joint. The grafts used for reconstructing this ligament have ranged from synthetic grafts to grafts from the semitendinosus, gracilis and quadriceps tendons and the patellar ligament^(2,9,13,16-23).

Since the start of the 21st century, biomechanical studies on cadavers have been developed using simulators constructed for analysis on the patellofemoral joint^(7,17,21,24-33). These studies can be divided into anatomical and biomechanical. Anatomical studies have

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been better accepted in the literature, given that they directly assess the reality of structures that make up the human body. On the other hand, biomechanical studies have been much criticized and need to be examined with care, given that they present controlled situations with very limited reproducibility, relating to a mechanical demand that might occur in real life. The most evident example of this is the lack of dynamic muscle action for stabilization of a joint.

Several models in biomechanical studies have attempted to address this failing, through simulating muscle loading by means of fixed weights or weights transferred to muscle structures^(27,34). The problem is that many of these models are complex and poorly reproducible, either because of their cost or because of the need for very specialized instrumentation.

In this paper, we present a device developed by the Biomechanics Laboratory of the Institute of Orthopedics and Traumatology, Hospital das Clínicas, School of Medicine of the University of São Paulo (IOT-HC-FMUSP), which makes it possible to simulate biomechanical situations close to reality on the knees of cadavers, through using weights and counterweights with accuracy calculations based on previously published values, and which also enables measurement of the distances between anatomical structures through a precise method based on analysis of photographs (photogrammetry) (35). We believe that this method is very useful in biomechanical analyses, since it is reproducible and not does have high costs.

MATERIALS AND METHODS

Obtaining and preparing the anatomical specimens

The study was conducted using six anatomical knee specimens taken from recent cadavers. The cadaver specimens came from the Death Verification Service of the city of São Paulo, after obtaining approval from the Scientific Committee of the Institute of Orthopedics and Traumatology (IOT), University of São Paulo, and from the Ethics Committee for Analysis of Research Projects (CAPPesq) of Hospital das Clínicas, School of Medicine of the University of São Paulo (FMUSP).

Group formation

The MPFL was reconstructed by means of resec-

tion of the middle third of the patellar ligament, in accordance with the surgical technique described by Camanho *et al*⁽¹⁶⁾ and it was fixed at angles of 0, 30, 60 and 90 degrees. All the trials were sequenced, in such a way that the same knee was subjected firstly to trials with its tendon and ligament structures intact, and then with the MPFL injured and lastly with the ligament reconstructed and fixed with the knee positioned at the angles of 0, 30, 60 and 90 degrees of flexion.

Reconstruction using the patellar ligament

The surgical procedure was performed using the patellar ligament as an autogenous graft, starting with an incision proximally to the upper margin of the patella, centered between the medial margin of the patella and medial epicondyle, and going towards the medial margin of the anterior tuberosity of the tibia (Figure 1).

Test method

All the specimens that had previously been selected for the study were evaluated mechanically in three distinct situations: with the MPFL intact, injured and reconstructed. In each situation, the knee was subjected to mechanical tests, divided into two test sequences. In the first sequence, the tests were repeated three times with the knee subjected to flexion-extension movement, from 120 to 0°, without any load applied laterally to the patella. In the second sequence, another three tests were repeated with the

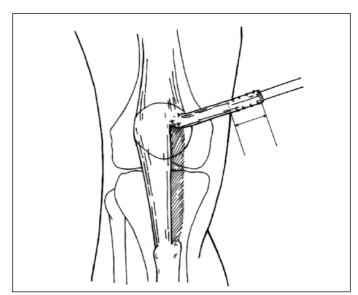


Figure 1 – Resection of the middle third of the patellar ligament going towards the medial edge of the patella, between the middle and proximal thirds (reproduced with permission from Camanho et al)⁽¹⁶⁾.

knee subjected to the same flexion-extension movement, but with the patella lateralized by means of a static load of 33.3 N (3.39 kg).

A mechanical device with the function of carrying out the abovementioned tests was developed at the Biomechanics Laboratory of IOT-HC-FMUSP. This device was coupled to a Kratos® K5002 universal mechanical test machine, equipped with a 5 tf load cell (Figure 2). All the information coming from the tests was controlled by a data acquisition system (Lynx Technology, model ADS-2000). Figure 3 illustrates a right knee positioned in the mechanical device developed.

With the objective of standardizing the force applied laterally to the patella, with the purpose of provoking subluxation of the patella, a force of 1 kgf was exerted on the graft during its fixation at the four different knee flexion angles. A load cell of 20 kgf that had been developed at the Biomechanics Laboratory (Figure 4) was coupled laterally in the femoral tunnel that had been created for the graft to pass through, with the aim of measuring the force used at the time of its fixation, and this standardized force was maintained for all the tests.



Figure 3 – Right knee fixed to the mechanical device, showing the weight coupled to the pulley (right) and the weight used to lateralize the patella (left).

In detail, the Ethibond® wires were tied to the upper beam of the load cell.

With the aim of monitoring the displacement of the patella in relation to a reference point on the femur, a three-dimensional photogrammetry system was developed at the Biomechanics Laboratory, based on

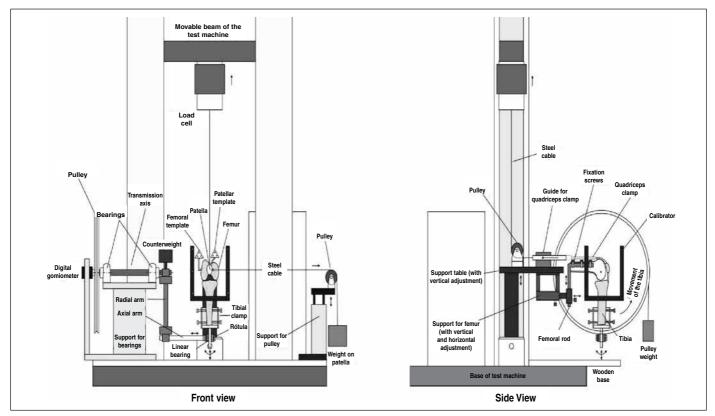


Figure 2 – Schematic representation of the left knee positioned in the mechanical device coupled to the universal mechanical test device. Front and side views of the components of the device.

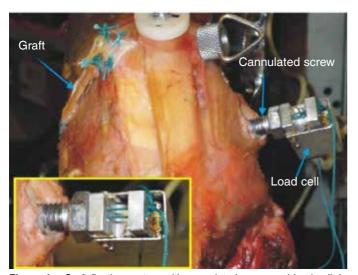


Figure 4 – Graft fixation system with cannulated screw and load cell. In detail, the Ethibond® wires tied to the upper beam of the load cell.

the model developed by Abdel-Aziz and Karara⁽³⁵⁾, which measured the positioning of the patella during the tests, with the knee positioned at flexion-extension of 120°, 105°, 90°, 75°, 60°, 45°, 30°, 15° and 0°.

This system comprised the following: another computer program in the Delphi[®] language, two digital photographic cameras, a three-dimensional calibrator and two templates fixed to the femur and patella.

The measurements on the three-dimensional coordinates of the 12 markers of the calibrator were made in the Dimensional Metrology Laboratory of the Institute of Industrial Studies and Research (IPEI), University Center of the School of Industrial Engineering (FEI), using a three-dimensional coordinate measurement machine (Mitutoyo®, model QM-353/189-314 BR) with a measurement uncertainty of 0.012 mm.

The template was composed of a small triangular plate containing three points similar to the markers of the calibrator, distributed at the vertices of an equilateral triangle, equidistant at around 21.3 mm from each other. Two templates were used: their measurements were made by the same laboratory that made the measurements on the calibrator. One template was fixed using two screws in the medial region of the patella and the other was placed in the posterior region of the femur (close to the capsule) by means of two cortical screws and an osteosynthesis plate molded for correct positioning of the template (Figure 5).

A computer program was developed in the Delphi[®] language with the functions of controlling (via ADS 2000) the up and down movements of the movable beam of the test machine and the action of the remote

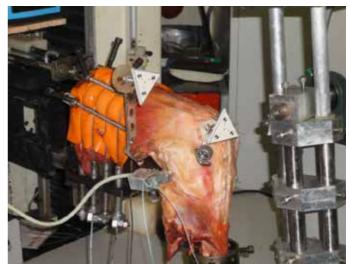


Figure 5 – Triangular templates used in the three-dimensional measurement process.

control, and recording the angle of knee flexionextension by means of digital goniometry and the force coming from the load cell.

The program correlated the two-dimensional coordinates of the markers present in the two templates, which were located on the pair of photographs obtained during the measurement process, with the two-dimensional coordinates of the 12 markers located on the two photographs that were obtained during the calibration process (Figure 5), by means of direct linear transformation (DLT), as described by Abdel-Aziz and Karara⁽³⁵⁾. The center of each marker was located automatically by the program, which generated a report with the special coordinates of the six markers distributed on the two templates.

Following this, measurements of the lateromedial deviation of the patella marker under the conditions of load application and without lateral loads were calculated.

The distances with and without load applied to the patella were grouped according to the angle of graft fixation (0° , 30° , 60° and 90°) and situation of the knee (intact, injured or reconstructed). The results were tabulated from the means of the three repetitions.

RESULTS

Table 1 shows the descriptive statistics on the differences between the distances with and without load applied to the patella, according to the angle of knee flexion (0°, 15°, 30°, 45°, 60°, 75°, 90°, 105° and 120°) and the situation of the knee (intact, injured or

reconstructed). These results were obtained from the means of the three measurements made on each knee for each situation and are presented in Figures 6 and 7.

Statistically significant differences were found in relation to lateralization of the patella, both between the angles of graft reconstruction (p < 0.001)

Table 1 – Description of the lateralization of the patella according to the graft reconstruction angle and the knee flexion angle.

Flexion- extension	MPFL conditions	n	mean	SD	median	Minimum	Maximum
0°	Intact	6	1.75	0.23	1.70	1.50	2.10
	Reconstructed 0°	6	8.13	0.10	8.10	8.00	8.30
	Reconstructed 45°	6	7.40	0.17	7.35	7.20	7.60
	Reconstructed 60°	6	5.67	0.15	5.60	5.50	5.90
	Reconstructed 90°	6	6.65	0.14	6.65	6.50	6.80
	Injured	6	9.50	0.13	9.50	9.20	9.60
15°	Intact	6	1.58	0.19	1.55	1.40	1.90
	Reconstructed 0°	6	7.97	0.10	8.00	7.80	8.10
	Reconstructed 45°	6	7.18	0.15	7.15	7.00	7.40
	Reconstructed 60°	6	5.53	0.16	5.55	5.30	5.70
	Reconstructed 90°	6	6.37	0.14	6.35	6.20	6.60
	Injured	6	9.32	0.13	9.40	9.10	9.40
30°	Intact	6	1.47	0.16	1.45	1.30	1.70
	Reconstructed 0°	6	7.87	0.10	7.90	7.70	8.00
	Reconstructed 45°	6	7.08	0.15	7.05	6.90	7.30
	Reconstructed 60°	6	5.41	0.17	5.40	5.20	5.60
	Reconstructed 90°	6	6.20	0.09	6.20	6.10	6.30
	Injured	6		0.12	9.25	9.00	9.30
45°	Intact	6	1.30	0.14	1.30	1.10	1.50
	Reconstructed 0°	6	7.77	0.10	7.80	7.60	7.90
	Reconstructed 45°	6		0.15	6.95	6.80	7.20
	Reconstructed 60°	6		0.12	5.30	5.20	5.50
	Reconstructed 90°	6	6.10	0.09	6.10	6.00	6.20
	Injured	6		0.12	9.15	8.90	9.20
60°	Intact	6	_	0.14	1.20	1.00	1.40
	Reconstructed 0°	6	7.67	0.10	7.70	7.50	7.80
	Reconstructed 45°	6		0.15	6.85	6.70	7.10
	Reconstructed 60°	6	5.22	0.12	5.20	5.10	5.40
	Reconstructed 90°	6	_	0.09	6.00	5.90	6.10
	Injured	6	9.02		9.05	8.80	9.10
	Intact	6	1.10	0.14	1.10	0.90	1.30
	Reconstructed 0°	6	7.57	0.10	7.60	7.40	7.70
75°	Reconstructed 45°	6		0.15	6.75	6.60	7.00
	Reconstructed 60°	6	5.12	0.12	5.10	5.00	5.30
	Reconstructed 90°	6	5.90	0.09	5.90	5.80	6.00
	Injured	6	_	0.12	8.95	8.70	9.00
	Intact Reconstructed 0°	6	1.00 7.47	0.14 0.10	1.00	0.80 7.30	1.20
	Reconstructed 45°	6		0.15	7.50 6.65	6.50	7.60 6.90
90°	Reconstructed 60°	6	5.02	0.13	5.00	4.90	5.20
	Reconstructed 90°	6		0.12	5.80	5.70	5.90
	Injured	6	8.82	0.03	8.85	8.60	8.90
	Intact	6	0.90		0.90	0.70	1.10
105°	Reconstructed 0°	6	7.36		7.40	7.20	7.50
	Reconstructed 45°	6	6.62		6.65	6.40	6.80
	Reconstructed 60°	_		0.12	4.90	4.80	5.10
	Reconstructed 90°			0.09	5.70	5.60	5.80
	Injured	6	8.72	0.12	8.75	8.50	8.80
120°	Intact	6	0.80	0.14	0.80	0.60	1.00
	Reconstructed 0°	6	7.27	0.10	7.30	7.10	7.40
	Reconstructed 45°	6	6.55	0.16	6.60	6.30	6.70
	Reconstructed 60°	6	4.82	0.12	4.80	4.70	5.00
	Reconstructed 90°	6	5.60	0.09	5.60	5.50	5.70
	Injured	6	8.62	0.12	8.65	8.40	8.70

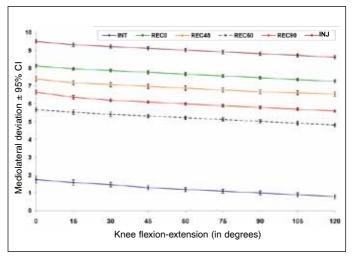


Figure 6 – Mediolateral deviation of the patella ± standard error, according to the graft reconstruction angle and the knee flexion angle.

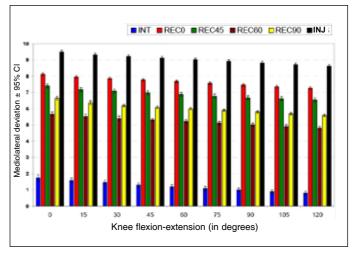


Figure 7 – Mediolateral deviation of the patella \pm standard error, according to the graft reconstruction angle and the knee flexion angle.

and between the angles of knee flexion-extension (p < 0.001). However, no alterations in behavior were observed with regard to the mean deviation of lateralization of the patella between the MPFL conditions across the flexion-extension parameters used (interaction of reconstruction * flexion-extension; p = 0.997) (Figures 6 and 7).

With the aim of investigating the reconstruction graft angles for which there were statistically significant differences, Tukey multiple comparisons were conducted⁽³⁶⁾ (Table 2).

For all the flexion-extension angles, greater lateralization was observed in the reconstruction of the injured knee, in comparison with the other situations; and the least lateralization was observed at the reconstruction of 60°, independent of the flexion-extension angle.

Table 2 – Multiple comparisons of the standard deviations for lateralization of the patella with the graft reconstruction angles.

Comp	arison	Estimated mean difference	Standard error	p value
Intact	ntact Lesado		0.022	<0.001
Intact	Reconstructed 0°	-6.441	0.022	<0.001
Intact	Reconstructed 45°	-5.674	0.022	<0.001
Intact	Reconstructed 60°	-3.991	0.022	<0.001
Intact	Reconstructed 90°	-4.802	0.022	<0.001
Injured	Reconstructed 0°	1.346	0.022	<0.001
Injured	Reconstructed 45°	2.113	0.022	<0.001
Injured	Reconstructed 60°	3.796	0.022	<0.001
Injured	Reconstructed 90°	2.985	0.022	<0.001
Reconstructed 0°	Reconstructed 45°	0.767	0.022	<0.001
Reconstructed 0°	Reconstructed 60°	2.450	0.022	<0.001
Reconstructed 0°	Reconstructed 90°	1.639	0.022	<0.001
Reconstructed 45°	Reconstructed 60°	1.683	0.022	<0.001
Reconstructed 45°	Reconstructed 90°	0.872	0.022	<0.001
Reconstructed 60°	Reconstructed 90°	-0.811	0.022	<0.001

DISCUSSION

The methodology used in the present study was based on the study of Ostermeier *et al*⁽³⁴⁾. Similarly, their study used a device that would allow knee extension movement through traction of the quadriceps with resistance to the movement, with lateral loading applied to the patella and measurement of the translation of the patella. However, the mechanical conception of the device and the method of measuring the displacement of the patella were different and adapted such that the studies could be conducted with the resources available.

Patellofemoral instability may result from anatomical factors that contribute towards greater lateralization of the patella. However, studies like those of Ahmad et $al^{(37)}$, Steiner et $al^{(22)}$ and Watanabe et $al^{(38)}$ demonstrate that reconstruction of the MPFL alone is effective even in cases with associated predisposing factors. Moreover, the same situation was reached in all the tests, and the force that caused the dislocation of the patella could be standardized in all the test sequences. The choice of force applied laterally to the patella was in accordance with the known data on forces resulting in patellar displacement, from previous studies^(1,24,27). Thus, the factors predisposing towards instability (patellar dysplasia, trochlear dysplasia and increased anterior tuberosity-trochlear groove distance), which may be associated in anatomical specimens, can be leveled in comparative tests like the present one, given that all the specimens were tested under the same test conditions⁽³⁹⁾.

It has been suggested that this laterally directed force might be less than the force that causes complete rupture of the MPFL $(200 \text{ N})^{(18,26)}$, but would result in significant lateral displacement of the patella without irreversible effects on the medial soft tissue contributing towards its restriction⁽²⁷⁾. The force applied laterally in the present study was fixed to the lateral margin of the patella in order to minimize the influence of patellar tilt, in accordance with the study by Sandmeier *et al*⁽²⁴⁾.

In all the tests, we applied a load of 1 kg, based on the biomechanical study of Beck *et al*⁽³⁰⁾, thereby demonstrating that a maximum traction of between 2 N and 10 N would be sufficient and adequate for stabilizing the reconstruction of the MPFL, and would not cause any increase in medial contact pressure of the patellofemoral joint.

Ostermeier *et al*⁽³⁴⁾ used an extension moment of 31 N.m that represented the physiological extension moment measured in healthy individuals undergoing isokinetic knee extension tests. However, if this is extrapolated to individuals undergoing reconstruction of the MPFL, application of this torque value during the initial recovery phase may be harmful. For this reason, a torque value corresponding to one third of the value of 31 N.m was applied for the flexion moment, as discussed by Beck *et al*⁽³⁰⁾. With the aim of maintaining the same proportions between the flexion torque and the load applied to the patella, the value of one third of 100 N recommended by Ostermeier *et al*⁽⁴⁰⁾ was used to promote lateralization of the patella.

In the present study, we evaluated the reconstruction of the MPFL with regard to the best knee flexion angle for graft fixation, along with the mediolateral path of the patella during knee flexion-extension. Through this, it could be affirmed that greater lateralization of the patella occurred at the first angles of knee flexion. This could, under conditions of injury to this ligament, promote dislocation of the patella in relation to the femoral trochlea. From the graphs and values presented in the statistical analysis, it could be seen that reconstruction of the MPFL fixed at angles less than 30 degrees of knee flexion promoted greater lateralization of the patella, thus coming close to the condition of an injured ligament. During knee flexion-

-extension, it could be seen, like in previous biomechanical studies⁽²⁹⁾, that the patella tended to dislocate at the first angles of flexion. This can be explained by the absence of bone structures acting as stabilizers at these angles, such that the MPFL was performing the function of primary restrictor against dislocation of the patella⁽⁴¹⁾. Thus, centralization of the patella in relation to the femur can be maintained at angles of 45 to 60 degrees, which favors correct fixation of the graft. At angles less than 30 degrees, the MPFL is under tension and without adequate bone protection against lateral displacement of the patella⁽²⁹⁾. Consequently, when the graft of the MPFL is fixed at these angles, excessive tensioning of the graft may occur, due to the absence of adequate medial parameters for determining its position, thus promoting increased pressure from the medial facet of the patella⁽³⁹⁾. At angles greater than 70 degrees, the MPFL is found to be slack, and tensioning of the graft above this angle is capable of inducing excessive medialization of the patella.

The force exerted by the hamstrings during knee extension promotes additional stabilization of the patellofemoral joint, thereby controlling tibial rotation⁽⁴²⁾. In our study, we standardized the force by fixing the tibia and making use of a counterweight to the extensor force of the quadriceps. Absence of weight-bearing,

which has a stabilizing effect during the movement of the patella, may lead to systematic bias⁽³⁴⁾.

The present study serves as a further aid towards decision-making during surgery for correction of patellofemoral instability, with regard to reconstruction of the MPFL. The cost of constructing the test apparatus is low in comparison with the methods found in the literature⁽²⁷⁾: a total of 11,000 dollars for the system. It can be used in less developed countries that lack the resources to purchase high-cost apparatus.

Examples of uses for this system include biomechanical studies that involve measurements of patella subluxation, with analysis on reconstruction of the MPFL using different grafts; studies on the isometry of different anatomical studies; studies on translation between the tibia and femur following different techniques for ligament reconstruction; and thus likewise comparing the different types of graft available. Through small adjustments to the device, these experiments are fully feasible.

CONCLUSION

This method developed in the biomechanics laboratory will be a useful tool for evaluating isometricity of the MPFL and of the patella and thus reconstruction of the MPFL.

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