J. Braz. Chem. Soc., Vol. 25, No. 11, 1984-1992, 2014. Printed in Brazil - ©2014 Sociedade Brasileira de Química 0103 - 5053 \$6.00+0.00

Kinetic and Thermodynamic Parameters of Biodiesel Oxidation with Synthetic Antioxidants: Simplex Centroid Mixture Design

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A influência da temperatura sobre a oxidação de biodiesel foi avaliada pelos parâmetros cinéticos e termodinâmicos do biocombustível de óleo de soja e gordura suína com antioxidantes sintéticos: 3-terc-butil-4-hidroxianisol (BHA), 3,5-di-terc-butil-hidroxitolueno (BHT), 2-terc-butil-hidroquinona (TBHQ) e galato de propila (PG), de acordo com delineamento de mistura simplex-centróide. Os parâmetros cinéticos foram determinados considerando-se reação de primeira ordem e aplicando a equação de Arrhenius. A adição de antioxidantes promoveu o aumento da energia de ativação (E_a), sendo TBHQ e PG os mais eficientes, apresentando efeito sinérgico. BHT e BHA foram os menos eficientes, assim como suas misturas. Os parâmetros termodinâmicos de ativação, avaliados pela equação de Eyring, não indicaram processos espontâneos ($\Delta G^{\sharp} > 0$) com valores de ΔH^{\ddagger} positivos, e ΔS^{\ddagger} positivos e negativos. O delineamento simplex-centróide indicou valor otimizado de 174,46 kJ mol⁻¹ para a mistura contendo 33,33 e 66,67% de TBHQ e PG, respectivamente.

Temperature's influence on biodiesel oxidation was evaluated by kinetic and thermodynamic data in biofuel from soybean oil and lard with synthetic antioxidants: butylatedhydroxyanisol (BHA), butylatedhydroxytoluene (BHT), *tert*-butylhydroquinone (TBHQ), and propylgallate (PG) by simplex centroid mixture design. The kinetic parameters ware obtained by Arrhenius equation and showed that addition of antioxidants in all tests increased activation energy (E_a) and that TBHQ and PG were more efficient and presented synergistic effect. BHT and BHA were the least efficient, as well as their mixtures. The thermodynamic activation parameters of the reactions, evaluated by the Eyring equation and based on the theory of the activated complex (ACT), indicated no spontaneous processes ($\Delta G^{\ddagger} > 0$) with positive ΔH^{\ddagger} values and positive and negative ΔS^{\ddagger} values. The application of simplex centroid mixture design, using E_a as response, showed the optimised value of 174.46 kJ mol⁻¹ for a mixture containing 33.33 and 66.67% of TBHQ and PG, respectively.

Keywords: activated complex, synthetic antioxidants, oxidation stability, mixture design

Introduction

The storage stability of a fuel is related to changes in physical and chemical characteristics caused by its interactions with the environment, and these changes can vary according to the nature of the raw material used in the production of biodiesel, specially due the presence/ absence of natural antioxidant in the final product.^{1,2} The autooxidation of fatty acid methyl esters (FAMEs) is associated with the oxygen reaction with allylic hydrogens on their unsaturated chains, resulting in the formation of free radicals and by-products that can cause problems in the engine and injection equipment.^{3,4} To inhibit or delay the oxidation reaction, antioxidants are used; phenolic compounds, classified as primary antioxidants, promote the removal or inactivation of free radicals by donating active hydrogen atoms.^{5,6}

Determination of the oxidative stability emerged in an attempt to predict the shelf life of oils and fats, however, the monitoring of oxidation products in storage conditions is slow and can consume a large amount of reagents.⁷ A way of determining the oxidative stability of FAMEs is by accelerated methods, such as Rancimat,

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which features rapid results, thus, reducing labour time and reagent consumption.⁸ Monitoring the oxidative stability obtained by Rancimat allows the determination of kinetic and thermodynamic parameters involved in the mechanism of biodiesel oxidation. Data such as energy (E_a) , enthalpy (ΔH^{\ddagger}), entropy (ΔS^{\ddagger}) and Gibbs free energy (ΔG^{\ddagger}) of activation allow the assessment of the efficiency of antioxidants added in biofuel and also to estimate the storage time, ensuring product quality in the periods of storage, distribution and use.⁴

The great diversity of raw materials and production techniques results in variations in the physicochemical properties of biodiesel, making it difficult to choose a specific antioxidant. Therefore, mixing is the most effective and economical way to maintain quality of the biofuel.^{2,9,10} The development of any product that involves more than one component implies some particular experiments with mixtures. Many studies employing mixture designs follow the models proposed by Scheffe, which allow the exploration of the entire experimental region.^{9,11,12}

Taking into consideration the importance of knowledge about kinetic and thermodynamic parameters and the fact that there are few reports in the literature on this subject, this work aimed to apply mathematical models that describe the oxidation reaction at several temperatures, throughout Rancimat method, with different synthetic antioxidants, alone or in mixtures.

Experimental

Biodiesel

B100 biodiesel was acquired from BioPar - Bioenergia do Paraná Ltda. (Rolândia, Paraná, Brazil), free of antioxidants, obtained by transesterification with a mixture of soybean oil (90%) and lard (10%), in methylic route using sodium methoxide as catalyst.

Some specification tests were carried out to determine the flash point (ASTM D93),¹³ the acid number (ASTM D664)¹⁴ and the specific mass (ASTM D4052)¹⁵ of the biodiesel.

Antioxidants

The antioxidants used were butylatedhydroxyanisol (BHA) Synth, 98.50%, butylatedhydroxytoluene (BHT) Synth, 99%, *tert*-butylhydroquinone (TBHQ) Acros, 97% and propyl gallate (PG) Acros, 98%. All of these analytical grade reagents were added directly to the biodiesel prior to the evaluation of oxidation stability; the proportions were stipulated by mixture design.

The total concentration of antioxidants did not exceed 6.0×10^{-3} mol L⁻¹, that corresponds to approximately 0.1% m/m, except PG, which was used at a concentration of 3.0×10^{-3} mol L⁻¹ (approximately 0.05% m/m). The choice of antioxidants and their concentrations was made according to preliminary tests.¹¹

Experimental design

A simplex centroid mixture design was applied for four components (TBHQ, BHT, BHA and PG), with two repetitions at the central point with combinations of mixtures 2^{q} -1, where q is the number of components equal to the sum 1 or 100%.¹⁶ The control sample was also performed in triplicate.

Mathematical model

The function used was equation 1:

$$Y(x) = \sum_{1 \le i \le q}^{q} \beta_{i} x_{i} + \sum_{1 \le i < j \le q}^{q} \beta_{ij} x_{i} x_{j} + \sum_{1 \le i < j < l \le q}^{q} \beta_{ijl} x_{i} x_{j} x_{l}$$
(1)

where *Y* is the response function of the experimental data E_a (kJ mol⁻¹), x_1 , x_2 , x_3 and x_4 are independent variables which correspond to the ratios of TBHQ, BHT, BHA and PG in the mixture, respectively, and β represents the estimated parameters.¹²

Statistical analysis

The optimisation of the conditions, the regression coefficients and analysis of variance (ANOVA) were determined by Statistica Software version 9.0.¹⁷

Oxidation stability test and induction period (IP) determination

Tests were carried out using the oxidative stability accelerated method through Rancimat equipment model 873 (Metrohm[®], Herisau, Switzerland) according to official EN 14112.¹⁸ Assays were performed at temperatures of 110, 115, 120 and 125 °C.

The induction period (IP) is determined by automated Rancimat software: a graph of conductivity (μ S cm⁻¹) *vs.* time (s) is generated, and the second derivative of the experimental data corresponds to IP, which is the maximum point of acceleration in chain reactions. The increase in conductivity is due to volatiles (products of degradation from biodiesel oxidation) dissolved in distilled water, monitored by a conductimetric sensor along the analysis.

Determination of kinetic and thermodynamic parameters of the biodiesel oxidation reaction

Data of the electrical conductivity (A) vs. time (t), obtained by Rancimat, for all assays of the mixture design and each temperature, were adjusted considering first-order reactions, so the rate constants (k) could be determined. The parameter activation energy (E_a) and pre-exponential factor (A) were calculated using the Arrhenius equation, while the enthalpy (ΔH^{\ddagger}) and entropy (ΔS^{\ddagger}) of activation were obtained by the Eyring equation or activated complex theory (ACT). The Gibbs free energy of activation (ΔG^{\ddagger}) was obtained from the fundamental equation of thermodynamics for all temperatures.⁴

Chromatographic analysis

Methyl esters, methanol, free and total glycerin, mono-, di- and triglyceride content were determined using a gas chromatograph with a flame ionization detector (GC-FID) system (Shimadzu GC 17A) and a DB1 column (100% polydimethylsiloxane with 30 m length \times 0.25 mm internal diameter \times 0.25 µm film thickness, J&W Scientific) was employed. The temperatures of split injector and detector were maintained at 340 °C. The oven was maintened initially at 50 °C for 2 min, and then heated at a rate of 10 °C min⁻¹ until 180 °C, maintained at this temperature for 2 min and, finally, heated at a rate of 15 °C min⁻¹ until it reached 340 °C, where it was maintained for 10 min. The carrier gas flow, N₂, was 1.5 mL min⁻¹ and the injection volume was 2.0 µL. Data were acquired and treated by the software Shimadzu CLASS-CR10.

The ester content was determined according to EN 14103,¹⁹ where a sample of 0.1 mL of biodiesel was solved in *n*-heptane (Sigma Aldrich, HPLC-grade) in a proportion of 1:10, using methyl heptadecanoate (Fluka, analytical grade) as internal standard. The alcohol content was verified according to EN 14110²⁰ using methanol (Fluka, analytical grade) as standard. For analysis of free and total glycerin, mono-, di- and triglyceride content, according to ASTM D6584,²¹ analytical standards of glycerin (Restek, 500 µg mL⁻¹ in pyridine), monoolein (Supelco, 500 µg mL⁻¹ in pyridine), triolein (Restek, 500 µg mL⁻¹ in pyridine), were used.

Results and Discussion

Biodiesel properties and composition

The EN 14214²² standard determines that the acceptable percentage of methyl esters in biodiesel must be equal to

or greater than 96.50% m/m. Chromatographic analysis of biodiesel showed that the content of methyl esters was 98.98% m/m, thus complying with current legislation; 84.82% m/m of this amount was composed of unsaturated esters $C_{18:1}$, $C_{18:2}$ and $C_{18:3}$, at a percentage of 26.98, 50.06 and 7.78%, respectively. High content of unsaturated esters in the composition of biodiesel is assigned to the high content of soybean oil (90%), which was used as raw material. The biodiesel produced had density equal to 879 kg m⁻³, 167.0 °C of flash point and 0.45 mg_{KOH} g⁻¹ of acid number, all values that meet the product specifications.²³

According to Knothe²⁴ biodiesel obtained from vegetable oils are rich in unsaturated fatty acids, making it susceptible to oxidation reaction resulting in low values of induction period (IP).^{24,25} The average IP value for control was 1.42 h, which is higher than the values of 0.16 h²⁶ and 1.36 h²⁷ of biodiesel obtained from 100% of soybean oil, showing that use of the pig fat may influence the increase of the oxidative stability. However, the addition of antioxidants is still needed in order for biodiesel to meet specifications,²³ of which the minimum value of IP is 6 h.⁹

Oxidation stability at different temperatures

According to Table 1, IP values decreased with increasing temperature and increased with the addition of antioxidants in all treatments, when comparing to the control sample.

 Table 1. IP values at different temperatures for each test from simplex centroid mixture design

	Mixture ^a -	IP / h				
Treatment		110 °C	115 °C	120 °C	125 °C	
1	(1,0,0,0)	6.23	3.22	2.19	1.87	
2	(0,1,0,0)	3.64	2.23	1.24	0.69	
3	(0,0,1,0)	5.62	3.1	2.19	1.62	
4	(0,0,0,1)	25.63	12.45	8.04	5.4	
5	(1/2,1/2,0,0)	5.56	3.44	2.27	1.34	
6	(1/2,0,1/2,0)	7.52	2.68	1.95	1.58	
7	(1/2,0,0,1/2)	31.54	14.76	7.54	5.52	
8	(0,1/2,1/2,0)	4.18	2.67	1.89	1.66	
9	$(0, \frac{1}{2}, 0, \frac{1}{2})$	21.09	9.88	6.43	4.49	
10	$(0,0,\frac{1}{2},\frac{1}{2})$	23.23	11.96	7.53	5.62	
11	(1/3,1/3,1/3,0)	5.77	2.65	1.99	1.28	
12	(1/3,1/3,0,1/3)	24.79	11.13	7.55	5.02	
13	(1/3,0,1/3,1/3)	21.58	12.37	8.31	5.81	
14	$(0, \frac{1}{3}, \frac{1}{3}, \frac{1}{3})$	19.99	10.12	6.92	4.77	
15 ^b	(1/4, 1/4, 1/4, 1/4, 1/4)	22.47	10.75	7.51	5.25	
Control ^b	(0,0,0,0)	1.42	0.88	0.25	0.20	

^aProportions of TBHQ, BHT, BHA, PG; ^baverage of triplicate.

It is observed that BHT used alone (treatment 2), presented the lowest values of IP in all assay temperatures, indicating lower efficiency when compared to other antioxidants, alone or in mixtures. However, it showed higher values than those observed in control samples. All treatments containing PG showed greater values of IP in all temperatures, even though it was added at lower concentration than the other antioxidants. Among the others antioxidants, TBHQ (treatment 1) is the most effective, followed by BHA (treatment 3) and BHT (treatment 2). The best response was achieved in the mixture containing TBHQ and PG, indicating synergism between them. The Tukey test applied to averages showed that IP of treatment 7 presented significant difference related to the responses of these isolated antioxidants (treatments 1 and 4), at a level of 5%.

The higher effectiveness of PG may be attributed to its chemical structure, which is more susceptible to donate hydrogen radical (H•) due to greater stabilization of the radical formed by the ring substituents.^{28,29} TBHQ has two hydroxyl groups, whereas both BHA and BHT have only one hydroxyl and various substituents, including ($-OCH_3$) and ($-CH_3$) bonded on the *para*-position of the ring. The hydroxyl group of BHA is more likely to release hydrogens compared to the hydroxyl group of BHT, because this one cannot stabilise its radical by resonance. Additionally, BHA has higher thermal stability than BHT, especially at a temperature of 110 °C.²⁹⁻³¹ The structures of the antioxidants are depicted in Figure 1.

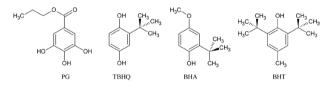


Figure 1. Chemical structures of the investigated antioxidants.

Santos *et al.*³¹ analysed the thermal profile of synthetic antioxidants at 110 °C, and observed that the stability decreases in the order: PG > TBHQ > BHA > BHT. Maia *et al.*¹¹ evaluated the oxidative stability of B100 biodiesel from soybean oil, with Rancimat, obtaining similar results when used with TBHQ, BHA and BHT at 110 °C. However, this information must be considered with caution, because the cited biodiesel mixture was stored near room temperature.³²

Kinetics and thermodynamics of the oxidation reaction of biodiesel

The rate constants (k) were determined by applying the natural logarithm (ln) on values of electrical conductivity (Λ)

vs. time (*t*), where the slope and intercept represent *k* and $ln \Lambda$, respectively. As result, a linear relationship between conductivity and time is shown in equation 2:

$$\ln \Lambda_0 = k(t_f - t_i) + \ln \Lambda \tag{2}$$

where Λ is the conductivity at time *t*; Λ_0 is the initial conductivity, and t_i and t_f correspond to initial and final time, respectively.

Table 2 presents the average values of k, which showed high coefficients of determination (R^2) ranging from 0.9336 to 0.9858. Galvan *et al.*⁴ also observed high correlation coefficients for the oxidation of biodiesel obtained from a mixture of vegetable oil and animal fat, considering first-order reaction kinetics.

Table 2. Rate constants (k) at different temperatures for all treatments

Treatment	Mixture ^a	k / h^{-1}				
		110 °C	115 °C	120 °C	125 °C	
1	(1,0,0,0)	0.5523	0.9197	1.218	1.548	
2	(0,1,0,0)	0.9251	1.340	1.809	2.112	
3	(0,0,1,0)	0.5853	0.9227	1.291	1.465	
4	(0,0,0,1)	0.1271	0.2245	0.3669	0.6087	
5	(1/2,1/2,0,0)	0.4898	0.7978	1.178	1.650	
6	(1/2,0,1/2,0)	0.4585	1.088	1.193	1.749	
7	(1/2,0,0,1/2)	0.0863	0.1854	0.4160	0.6512	
8	$(0, \frac{1}{2}, \frac{1}{2}, 0)$	0.6597	1.150	1.511	1.555	
9	$(0, \frac{1}{2}, 0, \frac{1}{2})$	0.1744	0.3709	0.5585	0.7307	
10	(0,0,1/2,1/2)	0.1383	0.3075	0.4733	0.6656	
11	(1/3,1/3,1/3,0)	0.5160	1.0316	1.3590	1.8107	
12	(1/3,1/3,0,1/3)	0.1308	0.3073	0.4578	0.6639	
13	(1/3,0,1/3,1/3)	0.1183	0.2215	0.4081	0.6475	
14	$(0, \frac{1}{3}, \frac{1}{3}, \frac{1}{3})$	0.1811	0.3323	0.5077	0.7483	
15 ^b	(1/4, 1/4, 1/4, 1/4, 1/4)	0.1361	0.3217	0.4369	0.6880	
Control ^b	(0,0,0,0)	1.686	1.845	1.945	2.253	

^aProportions of TBHQ, BHT, BHA, PG; ^baverage of triplicate.

According to Table 2, the control presented a value of k, at 125 °C, which is 1.3 times higher than the rate constant at 110 °C. It is observed that the k values increase with increasing temperature for all treatments as consequence of the increase in the rate of consumption of the antioxidant, showing thereby the dependence of the oxidation process with temperature.³³

The high k values can be related to the amount of soybean oil used in the production of biodiesel. However, there is a decrease in the values of the rate constants when antioxidants are present; treatment 2 presented the highest

values of k compared with the others, although they were still lower than those observed for the control. According to Tan *et al.*³⁴ the k value is directly related not only to the presence or absence of antioxidants, but also with the structures of the fatty acids, as having a high content of unsaturation is partly responsible for increasing the constant.

Kinetic data can be expressed by quantitative relationship between assay temperature, rate constant and activation energy through the Arrhenius equation:³⁴

$$\ln(k) = \ln A - E_a/RT \tag{3}$$

where k is the rate constant (h⁻¹), A the pre-exponential factor (h⁻¹), E_a the activation energy (kJ mol⁻¹), R the ideal gas constant (8.31447 J K⁻¹ mol⁻¹) and T the absolute temperature (K).

According to the Arrhenius equation (equation 3), the graph of $ln \ k \ vs$. the reciprocal of temperature $(1/T, \text{ K}^{-1})$ plots a line with slope $(-E_d/R)$ and intercept $(ln \ A)$, which allows determination of E_a and A, respectively.

The oxidation reaction of B100 biodiesel occurs through an energised transitory species of intermediate structure between the reactants and products called activated complex or transition state.⁴ Thus, the thermodynamic parameters (ΔH^{\ddagger} and ΔS^{\ddagger}) were estimated by applying the activated complex theory (ACT), developed by Eyring in 1935. The effect of temperature on reaction rate can be interpreted using ACT as described by equation 4, which is analogous to the Arrhenius equation (equation 3):^{35,36}

$$\ln(k/T) = [\ln(k_{R}/h) + (\Delta S^{\ddagger}/R)] - (\Delta H^{\ddagger}/R)(1/T)$$
(4)

where k_B is the Boltzmann constant (1.38065 × 10⁻²³ J K⁻¹), *h* is Planck's constant (6.62608 × 10⁻³⁴ J s), ΔH^{\ddagger} is the enthalpy of activation (kJ mol⁻¹), ΔS^{\ddagger} is the entropy of activation (J mol⁻¹ K⁻¹) and the notation [‡] refers to the state of activated complex.

According to the Eyring equation (equation 4), the regression of $ln \ k/T \ vs. \ 1/T \ (K^{-1})$ derived from ACT yields a straight line with slope $(-\Delta H^{\ddagger}/R)$ and intercept $[ln \ (k_B/h) + (\Delta S^{\ddagger}/R)]$, which permits the determination of ΔH^{\ddagger} and ΔS^{\ddagger} , respectively.

Figure 2 shows the linear regression of the data obtained by equation 3 for each treatment (Table 2); the coefficients of determination varied between 0.8612 and 0.9994. Chen *et al.*,³⁷ Chen and Luo³⁸ and Xin *et al.*³⁹ obtained a good linear correlation between *ln k vs. 1/T* (K⁻¹) studying the kinetics of oxidation of biodiesel obtained from different raw materials, associated with the use of different synthetic antioxidants.

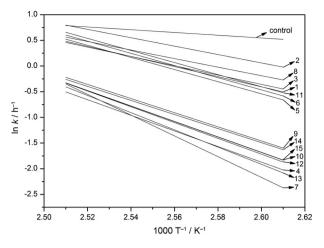


Figure 2. Linear regression of *ln k* as a function of temperature of biodiesel containing different antioxidants, alone or in mixtures.

Considering that E_a is given by the slope, the larger the energy of activation value, the greater the dependence of k with temperature, that is, the slope is more accentuated in the graph.^{40,41} Figure 2 depicts that the control presented the smallest slope, indicating that it is more susceptible to oxidation compared to the other treatments containing antioxidants. On the other hand, the treatment with PG presented bigger slopes, particularly when mixed with TBHQ, leading to higher values of E_a and, thus, greater oxidative stability.

The values of E_a are depicted in Table 3, where the control sample showed the lowest value, followed by the three treatments containing only TBHQ, BHA and BHT. Also, it is observed that there is an occurrence of synergism among the antioxidants when used in mixtures (treatments 5, 6, 7, 11, 12 and 13), because the E_a of the mixtures of antioxidants is greater than the sum of their individual effects. Among the mixtures, E_a of treatment 7 (TBHQ and PG) was about 7.5 times higher than that of the control, followed by the other mixtures with PG (treatments 12 and 13). Among the antioxidants mixture in which PG is absent, treatments 5, 6, 8, and 11, the one containing TBHQ and BHA showed the highest E_a , 4.5 times higher than the control, followed by the other mixtures with TBHQ (treatments 5 and 11).

There is considerable evidence that phenolic antioxidants have synergistic activities, so it is very important to consider these effects when choosing their formulation.¹¹ However, the synergistic effect has not been observed in some mixtures containing BHT and BHA (treatments 8, 9, 10, 14 and 15), and even treatment 8, which showed the lowest value among these mixtures, presented an E_a value 3 times higher than the control. Litwinienko *et al.*⁴² reported that the high degree of unsaturation in the chemical chain of biodiesel leads to lower E_a for the oxidation reaction.

Treatment	Mixture ^a	Kinetics		Thermodynamics		
		$E_a / (\text{kJ mol}^{-1})$	A / h ⁻¹	$\Delta H^{\ddagger} / (\text{kJ mol}^{-1})$	$\Delta S^{\ddagger} / (J \text{ K}^{-1} \text{ mol}^{-1})$	$\Delta G^{\ddagger} / (\text{kJ mol}^{-1})$
1	(1,0,0,0)	85.65	2.84×10^{11}	82.40	-36.20	96.54
2	(0,1,0,0)	70.68	4.21×10^{9}	67.44	-71.22	95.26
3	(0,0,1,0)	78.48	3.18×10^{10}	75.24	-54.42	96.50
4	(0,0,0,1)	131.57	1.13×10^{17}	128.32	71.00	100.58
5	(1/2,1/2,0,0)	102.33	4.58×10^{13}	99.09	6.07	96.72
6	(1/2,0,1/2,0)	104.43	9.45×10^{13}	101.19	12.08	96.47
7	(1/2,0,0,1/2)	174.38	5.49×10^{22}	171.14	179.86	100.88
8	$(0, \frac{1}{2}, \frac{1}{2}, 0)$	72.46	5.71×10^{9}	69.21	-68.69	96.04
9	$(0, \frac{1}{2}, 0, \frac{1}{2})$	119.61	4.06×10^{15}	116.37	43.34	99.44
10	$(0,0,\frac{1}{2},\frac{1}{2})$	130.72	1.05×10^{17}	127.48	70.37	99.99
11	(1/3,1/3,1/3,0)	102.70	5.88×10^{13}	99.46	8.13	96.28
12	(1/3,1/3,0,1/3)	133.96	2.78×10^{17}	130.72	78.49	100.06
13	(1/3,0,1/3,1/3)	144.81	6.83×10^{18}	141.57	105.10	100.51
14	$(0, \frac{1}{3}, \frac{1}{3}, \frac{1}{3})$	118.77	3.02×10^{15}	115.52	40.87	99.55
15 ^b	(1/4, 1/4, 1/4, 1/4)	131.24	1.22×10^{17}	127.99	71.66	100.00
Control ^b	(0,0,0,0)	23.35	2.55×10^{3}	20.10	-190.25	94.42

Table 3. Kinetic and thermodynamic parameters for biodiesel oxidation

^aProportions of: TBHQ, BHT, BHA, PG; ^baverage of triplicate. ΔG^{\sharp} : average of values at different temperatures (383.15, 388.15, 393.15 and 398.15 K).

The biodiesel used was produced with high percentage of soybean oil and contains high content of polyunsaturated FAMEs, which are more susceptible to oxidation reactions, evidenced by the low value of E_a observed in the control (23.35 kJ mol⁻¹).^{4,5}

The influence of temperature on the reactions is determined by the activation energy. Higher values of E_a imply that a small change in temperature is required to induce changes in the oxidation rate, whereas reactions with lower values of E_a are relatively independent of temperature.^{34,40,41} According to Levenspiel,⁴⁰ reactions with values ranging between 40 and 400 kJ mol⁻¹ are considered low and high activation energy, respectively. Therefore, the oxidation of biodiesel obtained from soybean oil predominantly exhibits poor chemical stability, even in the presence of antioxidants, because the values of the activation energy obtained were not high.³²

The biodiesel displayed values of pre-exponential factor (A) varying from 2.55×10^3 h⁻¹, for control, up to 5.49×10^{22} h⁻¹, for the mixture with TBHQ and PG (Table 3). Chen *et al.*³⁷ and Chen and Luo³⁸ reported values of 2.21×10^{13} and 5.66×10^{10} h⁻¹, respectively. According to Tan *et al.*³⁴ small changes in the values of E_a result in significant changes in the pre-exponential factor.

Figure 3 depicts the graph generated by equation 4, through ACT, for the oxidation of biodiesel at different temperatures. The lines presented determination

coefficients (R^2) with values between 0.8497 and 0.9994. Galvan *et al.*⁴ obtained a similar linear correlation between *ln k/T vs. 1/T* (K⁻¹), to evaluate the thermodynamic parameters of the oxidation reaction of an optimised biodiesel from a mixture of vegetable oil and animal fat.

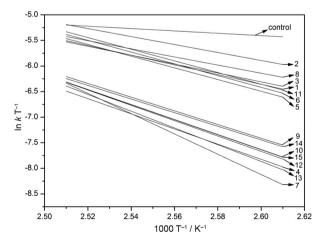


Figure 3. Linear regression of ln k/T as a function of temperature for biodiesel containing different antioxidants, alone or in mixtures.

In Table 3, it can be noted that all treatments, including the control, showed positive ΔH^{\ddagger} values, indicating that the process is endothermic, i.e., an external source of energy is required to raise the energy level of reagents to their transition state. Thus, the higher the value of enthalpy of activation of biodiesel, the greater the oxidative stability.^{35,36,43} ΔH^{\ddagger} values increased with the addition of antioxidants, when compared with the control: mixtures with presence of PG presented the highest values, followed by their mixtures with TBHQ, demonstrating that these two antioxidants are synergistic with each other and with other antioxidants. This effect was not observed in the presence of treatments with BHT and BHA.

Considering values of entropy (Table 3), both positive and negative signals were obtained for the treatments. Negative ΔS^{\ddagger} values may arise as a result of association mechanism; degrees of freedom were lost due to the activated complex formation, which means that reacting species joined themselves to form the state transition during the reaction, thereby having a more ordered state than the reactants in the ground state structure. Positive ΔS^{\ddagger} values indicate an increase of degrees of freedom, i.e., greater system disorder.^{35,36}

The Gibbs free energy of activation (ΔG^{\ddagger}) is used to determine the spontaneity of chemical reactions, and it was determined for all temperatures by the fundamental thermodynamic equation (equation 5):⁴³

$$\Delta G^{\ddagger} = \Delta H^{\ddagger} - T \Delta S^{\ddagger} \tag{5}$$

Table 3 shows that all samples presented positive values of ΔG^{\ddagger} , indicating that they are endergonic and not spontaneous. It can also be noted that all treatments with antioxidants showed values of ΔG^{\ddagger} higher than the control, with treatment 7 being the most endergonic, followed by treatments with PG in the mixtures. The reaction rate decreases with increasing ΔG^{\ddagger} , however, as the temperature increases, the reaction rate also increases.^{35,44}

Activation energy (E_a)

As the kinetic parameters were consistent with the thermodynamics, an analysis was carried out with the objective of obtaining a mixture formulation, which yields higher values of E_a (Table 3).

In the canonical equation 6 fitted to the experimental data, the dependent variable Y is the activation energy, E_a (kJ mol⁻¹), in which significant terms at the 5% level are shown with an asterisk. Also, the addition of antioxidants positively influenced the E_a of the studied biodiesel, since most terms had positive coefficients.

$$Y = 85.69^{*}x_{1} + 70.72^{*}x_{2} + 78.52^{*}x_{3} + 131.61^{*}x_{4} + 95.31^{*}x_{1}x_{2} + 88.11^{*}x_{1}x_{3} + 261.73^{*}x_{1}x_{4} - 9.83^{*}x_{2}x_{3} + 72.59^{*}x_{2}x_{4} + 101.43^{*}x_{3}x_{4} + 147.47^{*}x_{1}x_{2}x_{3} - 236.77^{*}x_{1}x_{2}x_{4} - 78.94^{*}x_{1}x_{3}x_{4} + 213.95^{*}x_{2}x_{3}x_{4}$$
(6)

The validity of the model for predictive purposes was confirmed by analysis of variance (Table 4), in which the model is significant ($p = 2 \times 10^{-6}$), with experimental and adjusted coefficients of determination equal to 99.90 and 99.60%, respectively, and with insignificant regression deviation (p = 0.17).

Table 4.	ANOVA	for res	ponse	E,
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	Degrees of freedom (df)	Sum of squares	Mean squares	F-value	<i>p</i> -value
Model	13	12796.99	984.38	348.18	2×10^{-6}
Total error	5	14.14	2.83	-	_
Lack of fit	1	5.87	5.87	2.84	0.17
Pure error	4	8.26	2.07	_	_
Total	18	12811.13	711.73	-	_

The combination region among the independent variables TBHQ, BHA and PG can be seen in Figure 4, which was generated by setting the least significant variable that corresponds to 0% BHT. The boundary region of the response surface demonstrates that an E_a (dependent variable) greater than 160 kJ mol⁻¹ can be achieved using a mixture containing TBHQ and PG.

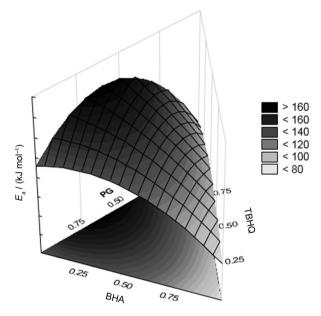


Figure 4. Region of combination among TBHQ, BHA and PG variables obtained by the mathematical model (equation 6) for E_a .

Figure 5 shows the optimisation of the predictive equation that represents the E_a of biodiesel in the presence of synthetic antioxidants. The maximum value (174.46 kJ mol⁻¹) can be obtained when using a mixture containing 33.33% of TBHQ and 66.67% of PG.

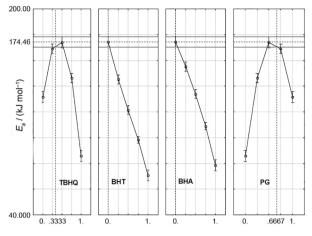


Figure 5. E_a optimisation for biodiesel with synthetic antioxidants.

Conclusions

The Rancimat method was demonstrated to be rapid and appropriate to investigate the kinetic and thermodynamic parameters of oxidation of biodiesel in the presence of synthetic antioxidants, alone or in mixtures. The parameters analysed indicated a low oxidation resistance for B100 biodiesel, however, the addition of antioxidants increased stability in all treatments, and those containing mixtures with PG and TBHQ yielded the best results. The simplex centroid mixture design was found to be a suitable tool to assess the best antioxidant to be added in biodiesel in order to increase its oxidation stability.

Acknowledgements

The authors would like to thank the State University of Londrina (UEL) and CAPES for scholarships.

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Submitted: May 5, 2014 Published online: August 5, 2014