Nulls and Side lobe Levels Control in a Time Modulated Linear Antenna Array by Optimizing Excitations and Element Locations Using RGA

Bipul Goswami and Durbadal Mandal Department of Electronics and Communication Engineering National Institute of Technology Durgapur West Bengal, India- 713209 Email: {durbadal.bittu, goswamibipul}@gmail.com

Abstract—In this paper a novel approach based on the Real coded Genetic Algorithm (RGA) is proposed to improve nulling performance as well as suppression of Side Lobe Level (SLL) of a Time Modulated Linear Antenna Arrays (TMLA). RGA adjusts the static excitation amplitudes as well as the location of each element from the origin to place deeper nulls in the desired direction. Three design examples are presented that illustrate the use of the RGA, and the optimization goal in each example is easily achieved.

Index terms — Time Modulated Linear Antenna Array; Far-field Pattern; Genetic Algorithm; Amplitude Excitation; Deeper Null; Side Lobe Level.

I. INTRODUCTION

Antenna Array is formed by assembling the radiating elements in a particular electrical or geometrical configuration. In most cases the elements are identical. Total field of the antenna array is found by vector addition of the fields radiated by each individual element. There are five control parameters in an antenna array that can be used to shape the pattern properly, they are, the geometrical configuration (linear, circular, rectangular, spherical etc.) of the overall array, relative displacement between elements, excitation amplitude of the individual elements, excitation phase of the individual elements [1-4]. In many communication applications it is required to design a highly directional antenna. Antenna Arrays have high gain and directivity compared to an individual radiating element.

As compared to conventional antenna arrays, the time modulated antenna arrays introduce a fourth dimension 'time' into the design [5-13]. By using the additional degree of freedom, time, more specifically, by properly turning on and off the array elements according to suitable time sequences, the stringent requirements on various error tolerances can be relaxed to the levels of those in conventional SLLs. However the major disadvantage of time modulated array is that, there are many

sideband signals spaced at multiples of modulation frequency, which implies that part of electromagnetic energy radiated or received by the antenna array was shifted to the sidebands.

The increasing pollution of electromagnetic environment has prompted the study of array pattern nulling techniques. These techniques are very important in radar, sonar and communication systems for minimizing degradation in signal to noise ratio performance due to undesired interference [3-4]. A lot of research works are going on for reducing the signal at nulls and Side Lobe Levels [5-20]. Time modulated antenna arrays are attractive for the synthesis of low/ultralow side lobes [6–7, 11-13]. In [6-7, 11], a differential evolution algorithm has been used to optimize the static-mode coefficients as well as the durations of the time pulses leading to a significant reduction of the sideband level. An approach to induce deeper nulls by controlling excitations amplitude of antenna elements in a time modulated array using Genetic Algorithm has been proposed in [8]. An approach for estimating direction of arrivals (DOA) in TMLAs with unidirectional phase center motion (UPCM) scheme is proposed in [9].

Design goal of this paper is to introduce deeper null/nulls to some desired direction and to suppress the relative SLL with respect to main beam for a TMLA of isotropic elements. This is done by designing the relative spacing between the elements, with a non-uniform excitation over the array aperture. This involves non-monotonic variation in antenna element parameters, which becomes a highly complex optimization problem. The classical optimization methods cannot bear the demand of such complex optimization problem.

Classical optimization methods have several disadvantages such as: i) highly sensitive to starting points when the number of solution variables and hence the size of the solution space increase, ii) frequent convergence to local optimum solution or divergence or revisiting the same suboptimal solution, iii) requirement of continuous and differentiable objective cost function (gradient search methods), iv) requirement of the piecewise linear cost approximation (linear programming), and v) problem of convergence and algorithm complexity (non-linear programming). For the optimization of such complex, highly non-linear, discontinuous, and non-differentiable array factors; various heuristic search evolutionary techniques were adopted. In this paper, the evolutionary technique, Real coded Genetic Algorithm (RGA) [3-4, 21-23] is used to get the desired pattern of the array. The time modulation period is divided into numerous minimal time steps with the same length, where the ON-OFF status for each time step is followed by a scheme given in the paper.

A broadside uniform linear array with uniform inter-element spacing is considered for reference. The array is symmetric with respect to the origin with equal spacing between any two consecutive elements. The phase difference between any two elements is kept zero. The RGA adjusts the excitation coefficients and location of elements from array centre for imposing deeper nulls at predefined directions. A cost function is defined which helps to keep the nulls and side lobes at lower levels.

The rest of the paper is arranged as follows: in section II, the general design equations for the nonuniformly excited and unequally spaced linear antenna array are stated. Then, in section III, a brief introduction for the Genetic Algorithm is presented. Numerical simulation results are presented in section IV. Finally the paper concludes with a summary of the work in section V.

II. DESIGN EQUATIONS

A broadside linear array of 2M isotropic radiators [1-2] is considered as shown in Figure 1, in which each element is controlled by a high speed RF switch and excited with non uniform current excitation. The array elements are assumed to be uncoupled and having equal inter-elements spacing along the z-axis with its centre at the origin. The array is symmetric in both, geometry and excitation with respect to the array centre. Only Amplitude excitations and spacing between each element are used to change the antenna pattern.



Fig. 1. Geometry of a 2M element symmetric linear array along the z axis.

The free space far-field pattern [1-2] in azimuth plane (x-y plane) with symmetric amplitude distributions is given by (1):

$$AF(I,\varphi,d,t) = 2\sum_{n=1}^{M} U_n(t)I_n \cos[kX_n\cos(\theta) + \varphi_n]$$
(1)

Brazilian Microwave and Optoelectronics Society-SBMO Brazilian Society of Electromagnetism-SBMag received 26 June 2012; for review 25 June 2012; accepted 02 July 2013 © 2013 SBMO/SBMag ISSN 2179-1074 where, θ denotes the angle measured from the broadside direction of the array. I_n, φ_n and X_n are respectively, current excitation amplitude, excitation phase, and location of the nth element from the origin. In this paper φ_n is kept as zero. $k = 2\pi/\lambda$, the propagation constant where λ being the signal wave length, d is the spacing between elements, 2M is total number of elements in the array. $U_n(t)$ =periodic switch ON-OFF time sequences function for nth where each element is switched ON for τ , where $0 \le \tau \le T$.

The array elements are numbered 1 to M from the origin in a symmetric array where total numbers of elements are 2M. Firstly the left most P elements (P < M) are turned on for time step τ , where

$$\tau = \frac{T}{M - P + 1} \tag{2}$$

Here T is the time modulation period. In first time step, the P consecutive elements numbered from 1 to P are switched ON. In the next time step, 2 to P+1 are switched ON and so on. In this work $U_n(t)$ is taken as [6-7]:

$$U_n(t) = \begin{cases} 1 & , \quad \varepsilon_1 \tau \le t \le \varepsilon_2 \tau \\ 0 & , \quad otherwise \end{cases}$$
(3)

where

$$\mathcal{E}_1 = \begin{cases} 0 &, \quad n \le P \\ n - P &, \quad otherwise \end{cases}$$
(4)

$$\varepsilon_{2} = \begin{cases} n & , \quad n \le M - P + 1 \\ M - P + 1 & , \quad otherwise \end{cases}$$
(5)

To illustrate the $U_n(t)$ in detail, an example of a time modulated linear array with M=8 and P=4 is shown in Fig. 2.



Fig. 2. Switch on time sequences of a 16 element (M=8) TMLA with P=4.

After defining the far-field radiation pattern, the next step in the design process is to formulate the objective function which is to be minimized. The objective function "Cost Function" (*CF*) or Fitness function which to be minimized with RGA for introducing deeper null is given in (6).

$$CF = C_1 \times \frac{\left| \prod_{i=1}^m AF(null_i) \right|}{\left| AF_{\max} \right|} + C_2 \times \sum_{k=1}^K H(k) \times (Q_k - \delta)$$
(6)

Where *m* is the maximum number of positions where null can be imposed. In this paper, one and two has been considered as the value of '*m*'. $AF(null_i)$ is the array factor value at the particular null position. AF_{max} is the maximum value of the array factor. The second term in the CF is added to reduce the side lobe up to a desired level. Here K denotes number of side lobes in the original pattern. Q_k is the side lobe level in dB generated by the individual population at some peak point θ_k . δ is the desired value of the side lobe level in dB. H(k) is defined as

$$H(k) = \begin{cases} 1 & , & (Q_k - \delta) > 0 \\ 0 & , & (Q_k - \delta) \le 0 \end{cases}$$
(7)

The side lobes whose peak exceeds threshold δ , that side lobe must be suppressed and for this purpose H(k) is adopted in the "cost function" expression. In cost function, for the first term, both the numerator and denominator are absolute. Further C_1 and C_2 are the weighting factors. The weight C_1 and C_2 are chosen in such a way that optimization of null remains more dominant, since the prime aim of this work is to achieve deeper null, C_1 value is taken higher than C_2 . Smaller value of the CF means that array factor values at predefined null positions are less. The RGA technique employed for optimizing current excitation weight and spacing between each elements resulting in the minimization of CF.

III. EVOLUTIONARY TECHNIQUE: REAL-CODED GENETIC ALGORITHM

GA is mainly a probabilistic search technique, based on the principles of natural selection and evolution. At each generation it maintains a population of individuals where each individual is a coded form of a possible solution of the problem at hand and called chromosome. Chromosomes are constructed over some particular alphabet, e.g., the binary alphabet $\{0, 1\}$, so that chromosomes' values are uniquely mapped onto the decision variable domain. Each chromosome is evaluated by a function known as fitness function, which is usually the fitness function or the objective function of the corresponding optimization problem.

Steps of RGA as implemented for optimization of spacing between the elements and current excitations are [3-4], [18-20]:

- Initialization of real chromosome strings of *n_p* population, each consisting of a set of excitations. Size of the set depends on the number of excitation elements in a particular array design.
- Decoding of strings and evaluation of *CF* of each string.
- Selection of elite strings in order of increasing *CF* values from the minimum value.
- Copying of the elite strings over the non-selected strings.
- Crossover and mutation to generate off-springs.
- Genetic cycle updating.

The iteration stops when the maximum number of cycles is reached. The grand minimum *CF* and its corresponding chromosome string or the desired solution are finally obtained.

The working principle of a GA has been explained briefly in the following figure based on the problem in hand.



Fig. 3. The GA flow for determining the optimized excitation amplitude and optimum location of array elements.

Desired pattern is generated by jointly optimizing amplitude distributions and location of array elements from the array centre. Here, both excitation amplitude and element location distributions are assumed symmetric with respect to the centre of the array. The chromosomes are corresponded to current excitation weights of antenna elements and location of individual elements from the array centre. Because of symmetry, each chromosome consists of 2M number of genes where M is the number of antenna elements on either side of array centre. Here 1st to Mth genes represent current excitation weights of antenna elements and $(M + 1)^{th}$ to $2M^{th}$ genes represent optimal element locations from the array centre. As an example chromosome one $\overline{W_1}$ can be represented by (8).

$$\overline{W_1} = [W_{11}, W_{12}, \dots, W_{1M}, W_{1(M+1)}, W_{1(M+2)}, \dots, W_{1(2M)}]$$
(8)

Here, $W_{11}, W_{12}, \dots, W_{1M}$ are the antenna elements amplitude distributions and $W_{1(M+1)}, W_{1(M+2)}, \dots, W_{1(2M)}$ are the locations of array elements from the array centre. Each of this

current excitation weights and element locations has boundaries with upper and lower limit. The random set of chromosome can be easily constructed using following relation represented by (9).

$$\overline{W}_n = (u_1 - u_2) \times \overline{r} + u_2 \quad , \quad u_2 < \overline{W}_n \le u_1 \tag{9}$$

Where, u_1 and u_2 are the maximum and minimum limit value of the weights and \bar{r} is real random vector between zero and one. RGA technique generates a set of normalized non-uniform current excitation weights and optimal spacing for all sets of time modulated linear antenna arrays.

IV. NUMERICAL RESULTS

A 12, 16, and 20 elements linear array of isotropic radiating elements, with $\lambda/2$ inter-element spacing, is considered for time modulated linear antenna array with T=16 μ s. The required "switch-on" time intervals for each element can be calculated using (2). RGA is applied to get deeper nulls. Every time RGA executed with 400 iterations. The population size was fixed at 120. For the real coded GA, the mutation probability was set to 0.01 and uniform crossover with crossover probability 1 was taken. RGA algorithm is initialized using random values of excitation ($0 < I_n < 1$) and spacing between elements ($\lambda/2 \le d < \lambda$). For predefined nulls of the radiation pattern, the nulling performances are improved. Similarly at predefined peak positions, the nulls are imposed. The programming has been written in Matlab language using MATLAB 7.8.0(R2009a) version on core (TM) 2 duo processor, 3.00 GHz with 2 GB RAM.

The Initial values of maximum SLL and Beam width between first nulls (BWFN) for uniform amplitude excitation ($I_n = 1$) and uniform spacing ($\lambda/2$ between adjacent elements) has been given in TABLE I.

TABLE I. SLL AND BWFN For Uniform Excitation ($I_n=1$) with $\lambda/2$ Inter-Elements Spacing Linear

Set No.	Total number of elements (2M)	SLL (dB)	BWFN (degree)
Ι	12	-13.06	19.10
II	16	-13.14	14.40
III	20	-13.19	11.52

Figures 4-6 show the imposing of deeper nulls over 3^{rd} null. For 12, 16, 20-element, the nulls have improved up to -80 dB, -80 dB, and -90 dB with initial values of -53.93 dB, -50.60 dB, -77.20 dB respectively. TABLE II shows the resulting amplitude excitation distribution, optimal elements location, initial and final null depth obtained by optimizing the cost function using RGA. In this case the weighting for the array elements I_1, I_2, \ldots, I_M are normalized using max (I_M) =1 and

ARRAY

 X_1, X_2, \ldots, X_M are normalized using $\lambda/2$. Figures 4-6 also depict the substantial reductions in maximum peak of the SLL with non-uniform current excitation weights and optimal placement of array elements, as compared to the uniform current excitation weights $(I_M = 1)$ and uniform interelements spacing $(\lambda/2)$ between adjacent elements) case. For example, in optimized pattern the SLL is reduced by more than 1 dB from -13.06 dB down to -14.27 dB for 12 elements array. For 16 elements array in optimized pattern SLL is reduced by more than 1 dB from -13.06 dB. For 20 elements array in optimized pattern SLL is reduced from -13.19 dB down to -14.22 dB. The improved values are shown in TABLE II and TABLE IIA.



Fig. 4. Best array pattern found by GA for the 12-elements array case with an improved null at 3rd nulls i.e. $\theta = 60^{\circ}$ and $\theta = 120^{\circ}$.



Fig. 5. Best array pattern found by GA for the 16-elements array case with an improved null at 3rd null i.e. $\theta = 68^{\circ}$ and $\theta = 112^{\circ}$.



Fig. 6. Best array pattern found by GA for the 20-elements array case with an improved null at 3rd null i.e. $\theta = 72.50^{\circ}$ and $\theta = 107.50^{\circ}$.

TABLE II. Current Excitation Weights, Initial and Final Null Depth for Non-Uniformly Excited Time Modulated Linear Array With Optimal Position of Elements (X_n) From Origin For One Null Imposed In The 3RD Null Position

No. of	$I_1, I_2,, I_M;$	Initial null	Final null
Elements	$X^{}_1, X^{}_2,, X^{}_M$ (Normalized with respect to $\lambda/2$)	depth (dB)	depth (dB)
12	0.9903 0.6311 0.2147 0.2657 0.1023 0.0823; 0.5498	-53.93	-92.04
	1.5952 2.6712 3.8133 4.9673 5.9893		
16	0.9960 0.8629 0.1854 0.4579 0.2219 0.1788 0.1667	-50.60	-88.29
	0.0557; 0.6064 1.7209 2.8607 3.9623 5.2483 6.3040		
	7.3990 8.5710		
20	0.9278 0.9769 0.7940 0.2258 0.2171 0.3373 0.3796	-77.20	-90.00
	0.2747 0.1890 0.2138; 0.5502 1.6514 2.6933 3.7407		
	4.9030 5.9060 6.9263 8.0007 9.1267 10.1433		

TABLE IIA. SLL and BWFN for Non-Uniformly Excited Time Modulated Linear Array With Optimal Spacing (X_n) from Array Centre For One Null Imposed at 3^{RD} Null Position.

No. of Elements	SLL Final (dB)	BWFN Final (degree)
12	-14.27	21.02
16	-14.51	14.40
20	-13.36	11.52

Figures 7-9 show the imposing of nulls at the 3rd peak for 12, 16 and 20 element structures respectively. For 12, 16, 20-element, the nulls have improved up to -79.60 dB, -83.17 dB, -92.00 dB

with initial values of -19.56 dB, -20.10 dB, -20.35 dB respectively. Figures 7-9 also depict the substantial reductions in maximum peak of the SLL with nonuniform current excitation weights and optimal placement of array elements, as compared to the uniform current excitation weights and uniform inter-elements spacing. For example, in optimized pattern the SLL is reduced by more than 1 dB from -13.06 dB down to -14.57 dB for 12 elements array. For 16 elements array in optimized pattern SLL is reduced by more than 4 dB from -13.14 dB down to -17.45 dB. For 20 elements array in optimized pattern SLL is reduced by more than 1 dB from -13.19 dB down to -14.22 dB. The improved values are shown in TABLE III and TABLE IIIA.



Fig. 7. Best array pattern found by GA for the 12-elements array case with a null introduced at 3rd peak i.e. $\theta = 54.50^{\circ}$ and 125.50° .



Fig. 8. Best array pattern found by GA for the 16-elements array case with a null introduced at 3rd peak i.e. $\theta = 64.40^{\circ}$ and

 $\theta = 115.60^{\circ}$



Fig. 9. Best array pattern found by GA for the 20-elements array case with a null introduced at 3rd peak i.e. $\theta = 69.70^{\circ}$ and $\theta = 110.30^{\circ}$.

TABLE III. Current Excitation Weights, Initial Peak and Final Null Depth for Non-Uniformly Excited Time Modulated Linear Array With Optimal Position of Elements (X_n) From Origin For One Null Imposed in The 3^{RD} Peak Position.

No. of Elements	$I_1, I_2,, I_M \ ; \label{eq:constraint} X_1, X_2,, X_M \ (\text{Normalized with respect to } \lambda/2 \)$	Initial Peak depth (dB)	Final Null depth (dB)
12	0.8596 0.4000 0.1975 0.1290 0.1447 0.1109; 0.5629	-19.56	-79.60
	1.8224 2.9448 3.9963 5.0663 6.2200		
16	0.8363 0.2757 0.4528 0.3001 0.2213 0.1470 0.1286	-20.10	-83.17
	0.0387; 0.5786 1.6428 2.7752 3.9237 5.0387 6.2760		
	7.5177 8.6637		
20	0.9278 0.9769 0.7940 0.2258 0.2171 0.3373 0.3796	-20.35	-92.00
	0.2747 0.1890 0.2138; 0.5502 1.6514 2.6933 3.7407		
	4.9030 5.9060 6.9263 8.0007 9.1267 10.1433		

TABLE IIIA. SLL and BWFN Obtained For Non-Uniformly Excited Time Modulated Linear Array With Optimal Spacing (X_n) from Array Centre For One Null Imposed at 3RD Peak Position.

No. of Elements	No. of Elements SLL Final (dB) BWFN F	
12	-14.57	18.00
16	-17.45	17.10
20	-14.22	10.00

Figures 10-12 show the imposing of nulls at the 2nd and 3rd peaks for 12, 16 and 20 element structures respectively. For 12, 16, 20-element, the pair of nulls has improved up to (-93.32 dB, -102.9 dB), (-

91.75 dB, -72 dB), (-71 dB,-78.92 dB) with initial values of (-17.22 dB,-19.56 dB), (-17.49 dB,-20.1 dB), (-17.61 dB, -20.40 dB) respectively. Figures 10-12 also depict the substantial reductions in maximum peak of the SLL with non-uniform current excitation weights and optimal placement of array elements, as compared to the uniform current excitation weights and uniform inter-elements spacing. For example, in optimized pattern the SLL is reduced by more than 1 dB from -13.06 dB down to -14.52 dB for 12 element array. For 16 element array SLL is reduced by more than 1 dB from -13.14 dB down to -15.05 dB. For 20 element array in optimized pattern SLL is reduced by more than 1 dB from -13.19 dB down to -15.85 dB. The improved values are shown in TABLE IV and TABLE IVA.



Fig. 10. Best array pattern found by GA for the 12-elements array case with nulls introduced at 2^{nd} ($\theta = 65.70^{\circ}$, 114.30°) and 3^{rd} ($\theta = 54.50^{\circ}$, 125.50°) peaks.



Fig. 11. Best array pattern found by GA for the 16-elements array case with nulls introduced at 2^{nd} ($\theta = 72.00^{\circ}$, 108°) and 3^{rd} ($\theta = 64.40^{\circ}$, 115.60°) peaks.



Fig. 12. Best array pattern found by GA for the 20-elements array case with nulls introduced at 2^{nd} ($\theta = 75.60^{\circ}$, 104.40°) and 3^{rd} ($\theta = 69.70^{\circ}$, 110.30°) peaks.

TABLE IV. CURRENT EXCITATION WEIGHTS, INITIAL PEAK AND FINAL NULL DEPTH FOR NON-UNIFORMLY EXCITED TIME MODULATED LINEAR ARRAY WITH OPTIMAL POSITION OF ELEMENTS (X_n) From Origin For Nulls Imposed In The 2ND and 3RD Peaks.

No. of	$I_1, I_2,, I_M$;	Initial Peak	Final Nulls
Elements	$X_1, X_2,, X_M$ (Normalized with respect to $\lambda/2$)	depth (dB) (2 nd ; 3 rd)	depth (dB) (2 nd ; 3 rd)
12	0.6604 0.3441 0.1941 0.1308 0.0860 0.0503; 0.5356	-17.22;	-93.32 ;
	1.7864 2.7942 3.9160 5.0453 6.0603	-19.56	-102.9
16	0.8590 0.7156 0.3911 0.2827 0.2771 0.2201 0.0535	-17.49 ;	-91.75 ;
	0.1513; 0.5415 1.7543 2.9376 4.2217 5.492 6.731	-20.10	-72.00
	8.016 9.204		
20	0.8771 0.3660 0.2959 0.4444 0.3665 0.3140 0.3425	-17.61 ;	-71.00 ;
	0.0162 0.3844 0.5038; 0.5516 1.5616 2.6270 3.7403	-20.40	-78.92
	4.8253 5.8977 6.9420 8.0433 9.1363 10.155		

TABLE IVA. SLL and BWFN for Non-Uniformly Excited Time Modulated Linear Array With Optimal Spacing (X_n) from Array Centre For Nulls Imposed at 2^{ND} And 3^{RD} Peak Positions.

No. of Elements	SLL Final (dB)	BWFN Final(deg)
12	-14.52	20
16	-15.05	12.20
20	-15.85	11.52

Figures 13-15 show the imposing of nulls at the 2nd and 3rd nulls for 12, 16 and 20 element structures respectively. For 12, 16, 20-element, the pair of nulls has improved up to (-74.89 dB, -64 dB), (-56.00 dB, -86.07 dB), (-68.60 dB, -86.36 dB) with initial values of (-55.83 dB, -53.93 dB), (-45.35 dB, 50.60 dB), (-56.62 dB, -77.2 dB) respectively. Figures 13-15 also depict the substantial reductions in

maximum peak of the SLL with non-uniform current excitation weights and optimal placement of array elements, as compared to the uniform current excitation weights and uniform inter-elements spacing ($\lambda/2$ spacing between adjacent elements). The improved values are shown in TABLE V and TABLE VA.



Fig. 13. Best array pattern found by GA for the 12-elements array case with improved nulls at 2^{nd} ($\theta = 70.60^{\circ}$, 109.40°) and 3^{rd} ($\theta = 60^{\circ}$, 120°) nulls.



Fig. 14. Best array pattern found by GA for the 16-elements array case with improved nulls at 2^{nd} ($\theta = 75.60^{\circ}$, 104.40°) and 3^{rd} ($\theta = 68^{\circ}$, 112°) nulls.



Fig. 15. Best array pattern found by GA for the 20-elements array case with improved nulls at 2^{nd} ($\theta = 78.50^{\circ}$, 101.50°) and 3^{rd} ($\theta = 72.50^{\circ}$, 107.50°) nulls.

TABLE V. CURRENT EXCITATION WEIGHTS, INITIAL AND FINAL NULL DEPTH FOR NON-UNIFORMLY EXCITED TIME MODULATED LINEAR ARRAY WITH OPTIMAL POSITION OF ELEMENTS (X_n) From Origin For Nulls Imposed In The 2ND and 3RD Null Positions.

No. of	$I_1, I_2,, I_M$;	Initial Null	Final Null
Elements	$X_1, X_2,, X_M$ (Normalized with respect to $\lambda/2$) $(2^{nd}; 3^{rd})$	depth (dB) (2 nd ; 3 rd)
12	0.8441 0.4070 0.1905 0.1380 0.1720 0.060); -55.83 ;	-74.89 ;
	0.5802 1.7421 2.8254 3.8373 4.8923 5.9727	-53.93	-64.00
16	0.9678 0.3873 0.3874 0.1390 0.1039 0.18	45 -45.35 ;	-56.00 ;
	0.0651 0.0248 ; 0.5375 1.6652 2.8013 3.94	-50.60	-86.07
	5.0710 6.1620 7.2737 8.3113		
20	0.4808 0.6124 0.5053 0.0760 0.2163 0.43	-56.62 ;	-68.60 ;
	0.2510 0.0659 0.2217 0.2998; 0.5324 1.57	88 -77.20	-86.36
	2.7307 3.8283 4.9587 6.0257 7.0400 8.12	20	
	9.2620 10.4107		

TABLE VA. SLL and BWFN for Non-Uniformly Excited Time Modulated Linear Array With Optimal Spacing (X_n) From Array Centre For Nulls Imposed at 2^{ND} and 3^{RD} Null Positions.

No. of Elements	SLL Final (dB)	BWFN Final (deg)
12	-13.56	19.10
16	-15.18	16.90
20	-13.27	11.62

V. CONCLUSIONS

In this paper, the design of a non-uniformly excited symmetric time modulated linear antenna array with optimized non-uniform spacing between the elements has been described using the optimization technique of Real-coded Genetic Algorithm. Simulated results reveal that optimizing the excitation amplitude of the elements with optimal spacing of the array antenna elements can impose deeper nulls at a desired direction as well as can reduce SLL for a given number of the array elements with respect to corresponding uniformly excited linear array with uniform inter-element spacing of $\lambda/2$. In almost all the cases nulls depth are improve by more than -80 dB. On the other hand maximum SLL also reduced in all cases. The BWFN of the initial and final radiation pattern remains approximately same. It is worth noting that, although the algorithm used here is implemented to constrained synthesis for a linear array with isotropic elements, one can see from the proposed technique it is not limited to this case. It can easily be implemented to non-isotropic elements antenna arrays with different geometries for the design of various array patterns.

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