

THE USE OF PRINCIPAL COMPONENTS AND UNIVARIATE CHARTS TO CONTROL MULTIVARIATE PROCESSES

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Abstract

In this article, we evaluate the performance of the T^2 chart based on the principal components (PC chart) and the simultaneous univariate control charts based on the original variables (SU \bar{X} charts) or based on the principal components (SUPC charts). The main reason to consider the PC chart lies on the dimensionality reduction. However, depending on the disturbance and on the way the original variables are related, the chart is very slow in signaling, except when all variables are negatively correlated and the principal component is wisely selected. Comparing the SU \bar{X} , the SUPC and the T^2 charts we conclude that the SU \bar{X} charts (SUPC charts) have a better overall performance when the variables are positively (negatively) correlated. We also develop the expression to obtain the power of two S^2 charts designed for monitoring the covariance matrix. These joint S^2 charts are, in the majority of the cases, more efficient than the generalized variance $|S|$ chart.

Keywords: principal component; simultaneous univariate control charts; multivariate process control.

Resumo

Neste artigo, avaliamos o desempenho do gráfico de T^2 baseado em componentes principais (gráfico PC) e dos gráficos de controle simultâneos univariados baseados nas variáveis originais (gráfico SU \bar{X}) ou baseados em componentes principais (gráfico SUPC). A principal razão para o uso do gráfico PC é a redução de dimensionalidade. Entretanto, dependendo da perturbação e da correlação entre as variáveis originais, o gráfico é lento em sinalizar, exceto quando todas as variáveis são negativamente correlacionadas e a componente principal é adequadamente escolhida. Comparando os gráficos SU \bar{X} , SUPC e T^2 concluímos que o gráfico SU \bar{X} (gráfico SUPC) tem um melhor desempenho global quando as variáveis são positivamente (negativamente) correlacionadas. Desenvolvemos também uma expressão para obter o poder de detecção de dois gráficos de S^2 projetados para controlar a matriz de covariâncias. Os gráficos conjuntos de S^2 são, na maioria dos casos, mais eficientes que o gráfico da variância generalizada $|S|$.

Palavras-chave: componentes principais; gráficos de controle simultâneos univariados; controle de processos multivariados.

1. Introduction

The control charts are often used to observe whether a process is in-control or not. When there is only one quality characteristic, Shewhart charts are usually applied to detect process shifts. The power of the Shewhart charts lies in their ability to separate the assignable causes of variation from the uncontrollable or inherent causes of variation. Shewhart charts are relatively easy to construct and to interpret. As a result, they are readily implemented in manufacturing environments.

However, there are many situations in which it is necessary to control two or more related quality characteristics simultaneously. Hotelling (1947) provided the first solution to this problem by suggesting the use of the T^2 statistic. Although the T^2 chart can be designed in a straightforward manner, it is difficult to relate an out-of-control signal to the variables whose parameters have moved away from their in-control values.

To overcome this difficulty, one of the approaches appearing in the literature is the simultaneous use of p univariate \bar{X} charts. Woodall & Ncube (1985) and Pignatiello & Runger (1990) suggested using univariate CUSUMs on each of the original variables. Runger & Montgomery (1997) presented a simple geometrical description of the directional sensitivity of a procedure based on simultaneous univariate control charts. Serel *et al.* (2000) studied the use of separate \bar{X} control charts for each characteristic from an economic perspective.

Principal components analysis (PCA) is a method of transforming a given set of variables into a new set of composite variables. These new variables are orthogonal to each other and account for the variance in the original data. It may be found that fewer principal components than the number of original variables are enough to summarize the variance. It is for these reasons that principal components are often used in exploratory data analysis and data reduction. Jackson (1980) suggested the use of principal components in quality control in conjunction with the T^2 control chart. The disadvantage of using principal components and the T^2 statistic is that both statistics may not have any physical meaning.

Schall & Chandra (1987) presented a method based on the principal components properties and multivariate regression analysis to predict the cause of variation. Souza & Rigão (2005) proposed procedures to identify the variables responsible for process instability. They considered the cases of weakly correlated and strongly correlated variables. Initially the T^2 chart is used to verify the state of the process. When the process is considered to be out-of-control, another investigation is carried out. For variables strongly correlated, an \bar{X} chart based on principal components is considered. For variables weakly correlated, an \bar{X} chart with Bonferroni limits is used.

The Bonferroni method is an alternative method for multiple comparisons developed from a probability inequality (see Johnson & Wichern (2002)). Let A_i denote the event that the sample mean for the i th quality characteristic, $i = 1, 2, \dots, p$, plots within specified control limits. Then, Bonferroni's inequality states that $P(A_1 \cap A_2 \cap \dots \cap A_p) \geq 1 - \alpha$. Therefore, p individual charts would be constructed, each with type I error equals to α/p (Alt, 1985).

According to Hayter & Tsui (1994), the overall error given by the system based on the Bonferroni inequality tends to be much smaller than α , because of the correlation between

the variables. To improve, they proposed a procedure based on the construction of exact simultaneous confidence intervals for each of the variables means, which offers easy identification of errant variables as well as easy quantification of any changes in the variable means. Their approach involves utilizing the existing tables of a multivariate normal distribution which give the desired percentage points corresponding to some selected correlation structures and α values. For those combinations of correlations and α that are not in the table, the authors suggest using simulation instead.

Similarly to what happens with the mean vector, it is also necessary to control the possible shifts in Σ_0 . In the univariate case, the well-known R, S and S^2 charts are the standard charts for the purpose of monitoring process variability (see Montgomery (2004)). Various alternative techniques for monitoring process dispersion have been introduced and gained wide acceptance in practice, as the use of CUSUM and EWMA control charts. While extension of these techniques to the multivariate case is of great importance in practice, control chart procedures for monitoring the covariance of a multivariate process have received very little attention (see Surtihadi *et al.* (2004)). Perhaps this lack of progress is due to the fact that it is not easy to define uniquely the shifts in the covariance matrix that need to be detected. Another difficulty in designing a multivariate control procedure for dispersion is the identification of the out-of-control process parameter(s) when the control chart signals.

The first multivariate control chart for monitoring the covariance matrix Σ was based on the charting statistic obtained from the generalized likelihood ratio test (see Alt (1985)). For the case of two variables Alt (1985) proposed the generalized variance $|S|$ statistic to control the covariance matrix Σ .

Aparisi *et al.* (1999) extended the $|S|$ statistic to the case of more than two variables and also considered this statistic to propose their bivariate control chart with adaptive sample size (see Aparisi *et al.* (2001)). A recent review of multivariate control charts for monitoring the covariance matrix was elaborated by Yeh *et al.* (2006).

The aim of this paper is to evaluate the performance of the T^2 chart based on the principal components and the simultaneous univariate control charts based on the original variables or based on the principal components. Moreover, we propose the use of simultaneous S^2 charts for monitoring the covariance matrix. We also develop the expression to obtain the power of this new monitoring procedure (see the Appendix II).

This paper is organized as follows: the next section presents a revision of different types of control charts for monitoring multivariate processes. In Section 3, we first investigate the use of principal components to control the mean vector of bivariate and trivariate processes, with positive or negative correlations. Second, we investigate the use of simultaneous univariate \bar{X} charts for monitoring the mean vector of bivariate processes. Alternatively, we also consider the use of two simultaneous univariate charts based on the principal components. In Section 4, we investigate the performance of two simultaneous S^2 charts designed to detect shifts in the covariance matrix. Conclusions are in Section 5. There are also three appendixes: in the Appendix I we describe the algorithm given in Serel *et al.* (2000) to obtain the control limits for univariate \bar{X} charts; in the Appendix II we present the expression to obtain the power of the simultaneous S^2 charts, and Appendix III brings Tables A1 through A5.

2. Control charts for monitoring multivariate processes

2.1 Control chart based on the principal components

One approach to controlling a process with several measured variables is based on principal components analysis (PCA). A principal component analysis is concerned with explaining the variance-covariance structure of a set of variables through a few linear combinations of these variables. Its general objectives are data reduction and interpretation.

Algebraically, principal components are particular linear combinations of the p random variables X_1, X_2, \dots, X_p . Geometrically, these linear combinations represent the selection of a new coordinate system obtained by rotating the original system with X_1, X_2, \dots, X_p as the coordinate axes. The new axes represent the directions with maximum variability and provide a simpler and more parsimonious description of the covariance structure.

Consider the special linear combinations

$$\begin{aligned} Y_1 &= \mathbf{e}'_1 \mathbf{X} = e_{11}X_1 + e_{12}X_2 + \dots + e_{1p}X_p \\ Y_2 &= \mathbf{e}'_2 \mathbf{X} = e_{21}X_1 + e_{22}X_2 + \dots + e_{2p}X_p \\ &\vdots \\ Y_p &= \mathbf{e}'_p \mathbf{X} = e_{p1}X_1 + e_{p2}X_2 + \dots + e_{pp}X_p \end{aligned} \quad (1)$$

where

$$\text{Var}(Y_i) = \mathbf{e}'_i \mathbf{\Sigma} \mathbf{e}_i = \lambda_i \quad i = 1, 2, \dots, p \quad (2)$$

$$\text{Cov}(Y_i, Y_k) = \mathbf{e}'_i \mathbf{\Sigma} \mathbf{e}_k = 0 \quad i \neq k = 1, 2, \dots, p \quad (3)$$

being $\mathbf{\Sigma}$ the covariance matrix of the random vector $\mathbf{X}' = [X_1, X_2, \dots, X_p]$ with the eigenvalues given by $\lambda_1 \geq \lambda_2 \geq \dots \geq \lambda_p \geq 0$.

The principal components are those uncorrelated linear combinations Y_1, Y_2, \dots, Y_p whose variances in (2) are as large as possible.

Suppose \mathbf{X} is a p dimensional normal vector with mean and covariance matrix given by $\boldsymbol{\mu}$ and $\mathbf{\Sigma}$, respectively, that is, $N_p(\boldsymbol{\mu}, \mathbf{\Sigma})$. The density of \mathbf{X} is constant on the $\boldsymbol{\mu}$ centered ellipsoids

$$(\mathbf{x} - \boldsymbol{\mu})' \mathbf{\Sigma}^{-1} (\mathbf{x} - \boldsymbol{\mu}) = c^2 \quad (4)$$

which have axes $\pm c \sqrt{\lambda_i} \mathbf{e}_i$, $i = 1, 2, \dots, p$, where the $(\lambda_i, \mathbf{e}_i)$ are the eigenvalue-eigenvector pairs of $\mathbf{\Sigma}$. The c^2 statistic is well-known in the literature as the Hotelling T^2 statistic, see section 2.3.

According to Johnson & Wichern (2002)

$$c^2 = \mathbf{x}' \mathbf{\Sigma}^{-1} \mathbf{x} = \frac{1}{\lambda_1} (\mathbf{e}'_1 \mathbf{x})^2 + \frac{1}{\lambda_2} (\mathbf{e}'_2 \mathbf{x})^2 + \dots + \frac{1}{\lambda_p} (\mathbf{e}'_p \mathbf{x})^2 \quad (5)$$

where $\mathbf{e}'_1\mathbf{x}, \mathbf{e}'_2\mathbf{x}, \dots, \mathbf{e}'_p\mathbf{x}$ are recognized as the principal components of \mathbf{x} . Setting $y_1 = \mathbf{e}'_1\mathbf{x}, y_2 = \mathbf{e}'_2\mathbf{x}, \dots, y_p = \mathbf{e}'_p\mathbf{x}$ we have

$$c^2 = \frac{1}{\lambda_1}(y_1)^2 + \frac{1}{\lambda_2}(y_2)^2 + \dots + \frac{1}{\lambda_p}(y_p)^2. \quad (6)$$

In this way, the Hotelling T^2 statistic can be expressed as a function of the X values (expression (5)) or as a function of the Y values (expression (6)). Recommendations for selecting an appropriate number of principal component variables for multivariate statistical process control are typically the same as those proposed for traditional PCA in which the objective is to summarize a complex dataset. Following some guidelines suggested by Runger & Alt (1996):

- 1) Choose k such that $\sum_{i=1}^k \lambda_i \geq 0.9 \sum_{j=1}^p \lambda_j$
- 2) Increment k such that $\lambda_i \geq \lambda_m$, where $\lambda_m = \frac{\sum_{j=1}^p \lambda_j}{p}$ and $i = 1, 2, \dots, k$
- 3) Plot λ_i against i and select k at the “knee” in the curve

Although these are useful guidelines in general, process control has a different objective than a summary of variation in a random sample of in-control data. Because the goal of statistical process control is to detect assignable causes in a stream of data collected over time, an approach to PCA is to investigate the performance of a control chart as a function of k .

2.2 Univariate charts for monitoring multivariate processes

As an example of how to control several variables with \bar{X} charts, let us consider two quality characteristics, represented by the normally distributed variables X_1 and X_2 . First we consider the case where both characteristics are independent. If the two variables are monitored separately a univariate \bar{X} chart with, for example, 3-sigma limits can be constructed for each characteristic. Each chart has a probability $\alpha = 0.0027$ (the type I error) of exceeding the 3-sigma control limits. The probability that both variables fall inside the control limits when the process is in-control is $(1-0.0027)(1-0.0027) = 0.994607$. So the overall type I error for this case is $\alpha' = 1-0.994607 = 0.0054$. If there are p statistically independent quality characteristics and charts with α type I error are used, the overall type I error α' is

$$\alpha' = 1 - (1 - \alpha)^p \quad (7)$$

So if we want to set the type I error for the process as a whole, having p independent variables, equation (7) can be used to calculate the suitable type I error for each chart, and then, to obtain the correct control limits (see Montgomery (2004)). If the variables are not independent, which is the most common case, a more complex procedure has to be employed to obtain the control limits to have an α' value. For simplicity, let us continue with the bivariate case

supposing that the variables follow a bivariate normal distribution with the in-control mean vector $\boldsymbol{\mu}'_0 = (\mu_{0,1}, \mu_{0,2})$ and the in-control covariance matrix $\boldsymbol{\Sigma}_0 = \begin{pmatrix} \sigma_{0,1}^2 & \rho\sigma_{0,1}\sigma_{0,2} \\ \rho\sigma_{0,1}\sigma_{0,2} & \sigma_{0,2}^2 \end{pmatrix}$ and \bar{X} charts are used. So, the control limits are $\mu_{0,1} \pm a\sigma_{0,1}/\sqrt{n}$ for \bar{X}_1 and $\mu_{0,2} \pm a\sigma_{0,2}/\sqrt{n}$ for \bar{X}_2 , where n is the sample size. Given α' , the control limit coefficient a can be obtained by the following relationship:

$$\begin{aligned} \alpha' &= 1 - \Pr\left(-a < \frac{\bar{X}_1 - \mu_{0,1}}{\sigma_{0,1}/\sqrt{n}} < a \cap -a < \frac{\bar{X}_2 - \mu_{0,2}}{\sigma_{0,2}/\sqrt{n}} < a\right) & (8) \\ &= 1 - \Pr(-a < Z_1 < a \cap -a < Z_2 < a) \\ &= 1 - \int_{-a}^a \int_{-a}^a f(z_1, z_2) dz_1 dz_2 \end{aligned}$$

where $f(z_1, z_2)$ is the joint density function of a bivariate standard normal distribution with correlation ρ . For example, using expression (8), if the variables X_1 and X_2 are uncorrelated ($\rho = 0$) $a = 3.2005$. On the other hand, if X_1 and X_2 are correlated ($\rho = 0.7$) $a = 3.1828$.

Note that if the characteristics measured are not independent, the probability of a type I error is very difficult to calculate by expression (8) and may be distorted if it is computed by expression (7). This distortion gets worse as p increases.

2.3 Multivariate control charts

The most common chart used to control the mean vector of multivariate processes is the T^2 chart introduced by Hotelling (1947). The first multivariate control chart for monitoring the covariance matrix $\boldsymbol{\Sigma}$ was based on the charting statistic obtained from the generalized likelihood ratio test (Alt, 1985).

Consider that p correlated characteristics are being measured simultaneously and these characteristics follow a multivariate normal distribution with mean vector $\boldsymbol{\mu}'_0 = (\mu_{0,1}, \mu_{0,2}, \dots, \mu_{0,p})$ and covariance matrix $\boldsymbol{\Sigma}_0$ when the process is in-control. When the i th sample of size n is taken we have n values of each characteristic and it is possible to calculate the $\bar{\mathbf{X}}_i$ vector, which represents the i th sample average vector for the p characteristics.

The charting statistic

$$T_i^2 = n(\bar{\mathbf{X}}_i - \boldsymbol{\mu}_0)' \boldsymbol{\Sigma}_0^{-1} (\bar{\mathbf{X}}_i - \boldsymbol{\mu}_0) \tag{9}$$

is called Hotelling's T^2 statistic. T_i^2 is distributed as a chi-square variate with p degrees of freedom.

When the process is in-control, $\boldsymbol{\mu} = \boldsymbol{\mu}_0$, there is a probability α that this statistic exceeds a critical point $\chi_{p,\alpha}^2$, so that the overall type I error can be maintained exactly at the level α by triggering a signal when $T_i^2 > \chi_{p,\alpha}^2$. If $\boldsymbol{\mu} \neq \boldsymbol{\mu}_0$, T_i^2 is distributed as a non-central chi-squared distribution with p degrees of freedom and with non-centrality parameter $\lambda = n(\boldsymbol{\mu} - \boldsymbol{\mu}_0)' \boldsymbol{\Sigma}_0^{-1} (\boldsymbol{\mu} - \boldsymbol{\mu}_0)$.

The first multivariate control chart for monitoring the covariance matrix $\boldsymbol{\Sigma}$ was based on the following statistic:

$$A_1 = -pn + pn \ln n - n \ln \left(\frac{|\mathbf{S}|}{|\boldsymbol{\Sigma}_0|} \right) + tr(\boldsymbol{\Sigma}_0^{-1} \cdot \mathbf{S}) \quad (10)$$

where \mathbf{S} is the sample covariance matrix,

$$\mathbf{S} = \begin{bmatrix} s_{11} & s_{12} & \cdots & s_{1p} \\ s_{21} & s_{22} & \cdots & s_{2p} \\ \vdots & \vdots & \cdots & \vdots \\ s_{p1} & s_{p2} & \cdots & s_{pp} \end{bmatrix}$$

being s_{ii} the sample variance of the i th variable and s_{ij} the sample covariance between the i th and j th variables. $|\mathbf{M}|$ is the determinant of a matrix \mathbf{M} and $tr(\mathbf{M})$ is the trace of a matrix \mathbf{M} (the sum of the diagonal elements).

When the process is in-control, that is $\boldsymbol{\Sigma} = \boldsymbol{\Sigma}_0$, A_1 is distributed asymptotically as a chi-square with $p(p+1)/2$ degrees of freedom; thus, it is possible to define a control chart limit to obtain the desired type I error.

For the case of two variables Alt (1985) proposed the generalized variance $|\mathbf{S}|$ statistic to control the covariance matrix $\boldsymbol{\Sigma}$. \mathbf{S} is the sample covariance matrix

$$\mathbf{S} = \begin{bmatrix} s_{11} & s_{12} \\ s_{12} & s_{22} \end{bmatrix}.$$

When the process is in-control $\frac{2 \cdot (n-1) \cdot |\mathbf{S}|^{1/2}}{|\boldsymbol{\Sigma}_0|^{1/2}}$ is distributed as a chi-square variable with

$2n - 4$ degrees of freedom.

Consequently, the control limit for the $|\mathbf{S}|$ chart is:

$$CL = \frac{(\chi_{2n-4,\alpha}^2)^2 \cdot |\boldsymbol{\Sigma}_0|}{4 \cdot (n-1)^2} \quad (11)$$

3. Performance of the control charts for monitoring the mean vector

3.1 Comparing the standard T^2 chart with the T^2 chart based on PCVs

The efficiency of a control chart in detecting a process change can be measured by the average run length (ARL). During the in-control period the $ARL=1/\alpha$ and is called ARL_0 , and during the out-of-control period the $ARL=1/(1-\beta)$. The risks α and β are the well-known Type I and Type II errors, respectively.

When a process is in-control it is desirable that the expected number of samples taken since the beginning of the monitoring until a signal (ARL_0) be large, to guarantee few false alarms. When a process is out-of-control it is desirable that the expected number of samples taken since the occurrence of the assignable cause until a signal (ARL) be small, in order to guarantee fast detection of process changes.

In this study we compare the performance of the standard T^2 chart based on the original variables and the T^2 chart based on PCVs. The control limits (CL) for different p values are given by $CL = \chi^2_{p,\alpha=0.005}$, reminding that p is the number of variables used to obtain the T^2 statistic.

It is assumed that when $p=2$ the original variables follow a bivariate normal distribution with the in-control mean vector $\mu'_0 = (0,0)$ and the covariance matrix $\Sigma_0 = \begin{pmatrix} 1 & \sigma_{12} \\ \sigma_{12} & 1 \end{pmatrix}$.

The principal components analysis requires the computation of the eigenvalues and their corresponding eigenvectors. The eigenvalues and the eigenvectors are in Table 1. The ARL values for the bivariate case are in Tables 2, A1 and A2, where $\rho = 0.0, \pm 0.3, \pm 0.5, \pm 0.7$. The process mean vector changes from $\mu'_0 = (0,0)$ to $\mu'_1 = (\mu_{0,1} + \delta_1\sigma_1; \mu_{0,2} + \delta_2\sigma_2)$, where δ_1 and $\delta_2 = 0, 0.5, 1.0, 1.5$.

Table 1 – Eigenvalues (λ) and eigenvectors (e_1, e_2) for the bivariate case.

ρ		variable 1	variable 2	ρ		variable 1	variable 2
0.0	λ	1.0	1.0	-0.3	λ	1.3	0.7
	e_1	1.0	0.0		e_1	0.7071	0.7071
	e_2	0.0	1.0		e_2	-0.7071	0.7071
0.3	λ	1.3	0.7	-0.5	λ	1.5	0.5
	e_1	0.7071	0.7071		e_1	0.7071	0.7071
	e_2	0.7071	-0.7071		e_2	-0.7071	0.7071
0.5	λ	1.5	0.5	-0.7	λ	1.7	0.3
	e_1	0.7071	0.7071		e_1	0.7071	0.7071
	e_2	0.7071	-0.7071		e_2	-0.7071	0.7071
0.7	λ	1.7	0.3				
	e_1	0.7071	0.7071				
	e_2	0.7071	-0.7071				

Tables 2, A1 and A2 compare the standard T^2 control chart based on the two original variables with the control chart based on the first PCV (PC1 chart) and the control chart based on the second PCV (PC2 chart). According to the results, the use of the PC1 chart or the PC2 chart instead of the standard T^2 chart is risky, specially when the practitioner does not know the nature of the disturbance. Runger & Alt (1996) also dealt with the choice of the principal components for multivariate statistical process control. Their procedure to select the principal components variables (PCVs) considers a specific shift in the mean vector. In our study we show that control charts based on selected PCVs are very efficient to detect a shift in the mean vector for which they were designed. However, there are other shifts for which the control chart might be insensitive.

When the two original variables are uncorrelated ($\rho = 0$) the PC1 chart is insensitive to any shift on the X_2 variable and the PC2 chart is insensitive to any shift on the X_1 variable. When the two original variables are correlated ($\rho > 0$) the PC2 chart is insensitive to shifts of the same magnitude in μ_1 and μ_2 , that is $\delta_1 = \delta_2$. When the correlation is negative ($\rho < 0$), the PC2 chart is the one that performs better. Depending on the shift, one of the three charts leads to the lowest *ARL* (*ARL* in bold).

Table 2 – The *ARL* values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 2$ and $\rho = \pm 0.3$)

		ρ								
		-0.3			0			0.3		
δ_1	δ_2	PC1	PC2	T^2	PC1	PC2	T^2	PC1	PC2	T^2
0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.5	139.35	109.04	110.44	200.0	90.93	115.54	139.35	109.04	110.44
0.0	1.0	68.12	39.97	37.96	200.0	28.21	41.92	68.12	39.97	37.96
0.0	1.5	32.93	16.16	13.85	200.0	10.46	15.78	32.93	16.16	13.85
0.5	0.0	139.35	109.04	110.44	90.93	200.0	115.54	139.35	109.04	110.44
0.5	0.5	200.0	39.97	57.78	90.93	90.93	76.87	68.12	200.0	91.64
0.5	1.0	139.35	16.16	22.75	90.93	28.21	32.95	32.93	109.04	40.09
0.5	1.5	68.12	7.57	9.39	90.93	10.46	13.64	17.06	39.97	15.75
1.0	0.0	68.12	39.97	37.96	28.21	200.0	41.92	68.12	39.97	37.96
1.0	0.5	139.35	16.16	22.75	28.21	90.93	32.95	32.93	109.04	40.09
1.0	1.0	200.0	7.57	11.28	28.21	28.21	18.49	17.06	200.0	25.81
1.0	1.5	139.35	4.10	5.65	28.21	10.46	9.36	9.57	109.04	13.03
1.5	0.0	32.93	16.16	13.85	10.46	200.0	15.78	32.93	16.16	13.85
1.5	0.5	68.12	7.57	9.39	10.46	90.93	13.64	17.06	39.97	15.75
1.5	1.0	139.35	4.10	5.65	10.46	28.21	9.36	9.57	109.04	13.03
1.5	1.5	200.0	2.54	3.40	10.46	10.46	5.76	5.82	200.0	8.53

When $p=3$ the original variables also follow a trivariate normal distribution with the in-control mean vector $\boldsymbol{\mu}'_0 = (0,0,0)$ and the covariance matrix $\boldsymbol{\Sigma}_0 = \begin{pmatrix} 1 & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & 1 & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & 1 \end{pmatrix}$.

The eigenvalues and the eigenvectors are in Table 3. The *ARL* values for the trivariate case are in Tables 4, A3 and A4, where $(\rho_{12}, \rho_{13}, \rho_{23}) = (0.0,0.0,0.0)$; $(0.3,0.3,0.3)$; $(0.8,0.5,0.2)$. The process mean vector changes from $\boldsymbol{\mu}'_0 = (0,0,0)$ to $\boldsymbol{\mu}'_1 = (\mu_{0,1} + \delta_1\sigma_1; \mu_{0,2} + \delta_2\sigma_2; \mu_{0,3} + \delta_3\sigma_3)$ where δ_1, δ_2 and $\delta_3 = 0, 0.5, 1.0, 1.5$. It is adopted $ARL_0=200.0$.

Tables 4, A3 and A4 compare the standard T^2 chart based on the three original variables with the control charts based on: the first PCV (PC1 chart), the second PCV (PC2 chart), the third PCV (PC3 chart), the first and the second PCVs (PC12 chart), the first and the third PCVs (PC13 chart) and the second and the third PCVs (PC23 chart), being $\rho_{ij} \geq 0.0$. The conclusions are the same as for the bivariate case. The cases where $\rho_{ij} < 0.0$ were also investigated. The main conclusion is that the PC3 chart has, in some cases, a better overall performance, for instance, when $(\rho_{12}, \rho_{13}, \rho_{23})$ is $(-0.3,-0.3,-0.3)$ or $(-0.8,-0.5,-0.2)$. For the cases of mixing positive and negative correlations, the control chart based on the principal components is very slow in signaling some disturbances.

Today, with electronic and other automated methods of data collection, it is usual to deal with a larger number of variables ($p > 3$). In this way, the reduction of the original p variables to k principal components is worthwhile. However, our study with $p = 2$ and 3 suggests that before adopting a T^2 chart based on the k principal components, the user should investigate how this chart responds to different types of disturbances.

Table 3 – Eigenvalues (λ) and eigenvectors (e_1, e_2, e_3) for the trivariate case.

$(\rho_{12}, \rho_{13}, \rho_{23})$		variable 1	variable 2	variable 3
(0.0,0.0,0.0)	λ	1.0	1.0	1.0
	e_1	1.0	0.0	0.0
	e_2	0.0	1.0	0.0
	e_3	0.0	0.0	1.0
(0.3, 0.3,0.3)	λ	1.6	0.7	0.7
	e_1	0.5774	0.5774	0.5774
	e_2	0.8165	-0.4082	-0.4082
	e_3	0.7071	0.0	-0.7071
(0.8,0.5,0.2)	λ	2.041	0.822	0.137
	e_1	0.6706	0.5993	0.4372
	e_2	-0.0996	-0.5113	0.8536
	e_3	0.7351	-0.6159	-0.2832

Table 4 – The *ARL* values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 3$ and $\rho_{12} = \rho_{13} = \rho_{23} = 0$).

δ_1	δ_2	δ_3	chart						T^2
			PC1	PC2	PC3	PC12	PC13	PC23	
0.0	0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.0	1.5	200.0	200.0	10.46	200.0	15.78	15.78	20.41
0.0	0.5	1.5	200.0	90.94	10.46	115.55	15.78	13.64	17.65
0.0	1.0	1.5	200.0	28.21	10.46	41.92	15.78	9.36	12.07
0.0	1.5	1.5	200.0	10.46	10.46	15.78	200.0	15.78	20.41
0.5	1.0	0.0	90.94	28.21	200.0	32.95	115.55	41.92	41.76
0.5	1.0	0.5	90.94	28.21	90.94	32.95	76.87	32.95	34.05
0.5	1.0	1.0	90.94	28.21	28.21	32.94	32.95	18.49	20.41
0.5	1.0	1.5	90.94	28.21	10.46	32.95	13.64	9.36	10.79
1.0	0.0	0.0	28.21	200.0	200.0	41.92	41.92	200.0	52.41
1.0	0.5	0.5	28.21	90.94	90.94	32.95	32.95	76.87	34.05
1.0	1.0	1.0	28.21	28.21	28.21	18.49	18.49	18.49	13.58
1.0	1.5	1.5	28.21	10.46	10.46	9.36	9.36	5.76	5.35
1.5	0.0	0.0	10.46	200.0	200.0	15.78	15.78	200.0	20.41
1.5	0.0	0.5	10.46	200.0	90.94	15.78	13.64	115.55	17.65
1.5	0.0	1.0	10.46	200.0	28.21	15.78	9.36	41.92	12.07
1.5	0.0	1.5	10.46	200.0	10.46	15.78	5.76	15.78	7.33

3.2 Univariate \bar{X} charts to control bivariate processes

In this section we study the simultaneous use of two univariate \bar{X} charts (SU \bar{X} charts) to control bivariate processes. Alternatively, we also consider the use of two simultaneous univariate charts based on the principal components (SUPC charts). The subroutine to compute the control limits for the SU \bar{X} charts uses an algorithm given in Serel *et al.* (2000), see the Appendix I. The control limit for each one of the two SUPC charts is given by $CL = \chi_{1,0.0025}^2$, considering that the overall type I error α' is 0.005 and the type I error α for each chart is computed by expression (7).

Tables 5 and 6 compare the *ARL* values for the SU \bar{X} charts with the *ARL* values for the T^2 control chart and for the SUPC charts, where δ_1 and $\delta_2 = 0, 0.5, 1.0, 1.5$ and $\rho = 0.0, \pm 0.3, \pm 0.5, \pm 0.7$. In these tables, we consider only the case where δ_2 is equal or larger than δ_1 . The inverse condition ($\delta_2 < \delta_1$) leads to the same *ARL* values.

When the correlation is positive ($\rho > 0$), the scheme based on the SU \bar{X} charts has a better overall performance, see Table 5. When the correlation is negative ($\rho < 0$), the scheme based on the SUPC charts has a better overall performance, see Table 6. If it is well known that the assignable cause only affects one variable at a time, then the T^2 chart is always the best option, except when $\rho = 0.0$. However, even in this case when $\rho = 0.0$, the *ARL*

reduction provided by the SU \bar{X} charts or by the SUPC charts is very small. For the case where the variables are uncorrelated ($\rho = 0.0$) the SUPC charts and the SU \bar{X} charts have the same performance for any shift.

Table 5 – ARL values for the standard T^2 chart and for the SU \bar{X} charts ($\rho \geq 0.0$).

		ρ										
		0.0		0.3			0.5			0.7		
		SU \bar{X}	T^2	SU \bar{X}	SUPC	T^2	SU \bar{X}	SUPC	T^2	SU \bar{X}	SUPC	T^2
<i>UCL</i>		3.023	10.597	3.021	9.138	10.597	3.015	9.138	10.597	2.996	9.138	10.597
<i>LCL</i>		-3.023	-	-3.021	-	-	-3.015	-	-	-2.996	-	-
δ_1	δ_2											
0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.5	117.4	115.6	117.4	115.1	110.5	117.5	104.2	99.7	115.8	81.5	78.0
0.0	1.0	41.6	41.9	41.6	43.6	38.0	41.5	34.7	30.6	40.3	20.8	19.0
0.0	1.5	15.1	15.8	15.1	17.5	13.9	15.0	12.8	10.5	14.5	6.65	5.94
0.5	0.5	83.2	76.9	84.0	93.0	91.7	85.4	101.3	99.7	87.0	108.4	106.7
0.5	1.0	36.4	33.0	36.9	43.3	40.1	37.5	46.5	41.9	37.8	44.7	38.7
0.5	1.5	14.4	13.6	14.5	19.4	15.8	14.6	19.3	15.0	14.5	15.0	11.4
1.0	1.0	23.44	18.5	24.1	25.2	25.8	24.93	30.0	30.60	25.96	34.8	35.25
1.0	1.5	11.89	9.36	12.3	13.3	13.0	12.65	15.9	15.01	13.01	17.8	15.73
1.5	1.5	8.09	5.76	8.50	8.02	8.53	8.91	9.94	10.51	9.42	12.0	12.58

Table 6 – ARL values for the standard T^2 chart and for the SU \bar{X} charts ($\rho \leq 0.0$).

		ρ										
		0.0		-0.3			-0.5			-0.7		
		SU \bar{X}	T^2	SU \bar{X}	SUPC	T^2	SU \bar{X}	SUPC	T^2	SU \bar{X}	SUPC	T^2
<i>UCL</i>		3.023	10.597	3.021	9.138	10.597	3.015	9.138	10.597	2.996	9.138	10.597
<i>LCL</i>		-3.023	-	-3.021	-	-	-3.015	-	-	-2.996	-	-
δ_1	δ_2											
0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.5	117.4	115.6	117.4	115.1	110.5	117.5	104.2	99.7	115.8	81.5	78.0
0.0	1.0	41.6	41.9	41.6	43.6	38.0	41.5	34.7	30.6	40.3	20.8	19.0
0.0	1.5	15.1	15.8	15.1	17.5	13.9	15.0	12.8	10.5	14.5	6.65	5.94
0.5	0.5	83.2	76.9	82.6	58.0	57.8	81.7	41.6	41.9	78.3	22.7	23.4
0.5	1.0	36.4	33.0	36.1	23.1	22.8	35.7	14.9	15.0	34.1	7.06	7.35
0.5	1.5	14.4	13.6	14.3	10.1	9.39	14.1	6.27	6.10	13.6	2.99	3.04
1.0	1.0	23.44	18.5	23.1	10.7	11.3	22.8	6.44	6.88	21.8	3.02	3.23
1.0	1.5	11.89	9.36	11.7	5.42	5.65	11.5	3.30	3.48	11.1	1.72	1.80
1.5	1.5	8.09	5.76	7.85	3.18	3.40	7.71	2.03	2.16	7.43	1.25	1.29

We also investigated the use of three simultaneous univariate \bar{X} charts to control trivariate processes. However, the results were not encouraging.

4. Performance of the control charts for monitoring the covariance matrix

4.1 Univariate S^2 charts to control bivariate processes

Two simultaneous univariate S^2 charts (SU S^2 charts) based on the statistics

$$S_1^2 = \frac{\sum_{j=1}^n (X_{1j} - \mu_1)^2}{n} \quad \text{and} \quad S_2^2 = \frac{\sum_{j=1}^n (X_{2j} - \mu_2)^2}{n}$$

are considered to control the process covariance matrix Σ , being X_1 and X_2 two quality characteristics. As an alternative to the use of two S^2 charts we might consider a single chart based on the statistic $\max(S_1^2, S_2^2)$.

This is equivalent to using two S^2 charts.

We assume that X_1 and X_2 follow a bivariate normal distribution with mean vector $\mu_0 = 0$ and covariance matrix $\Sigma_0 = \begin{pmatrix} 1 & \sigma_{12} \\ \sigma_{12} & 1 \end{pmatrix}$. Following Surtihadi *et al.* (2004) we consider two kinds of assignable causes that change the initial covariance matrix to $\Sigma_1 = \begin{pmatrix} \gamma_1^2 & \gamma_1 \gamma_2 \sigma_{12} \\ \gamma_1 \gamma_2 \sigma_{12} & \gamma_2^2 \end{pmatrix}$, being $\sigma_{12} = \rho$. For the case I $\gamma_1^2 = c^2$ and $\gamma_2^2 = 1$ (or $\gamma_2^2 = c^2$ and $\gamma_1^2 = 1$) and for the case II $\gamma_1 = \gamma_2 = \gamma$ and $\gamma^2 = c$, being $c^2 > 1$. In the Appendix II we develop the expression to obtain the *ARL* for the SU S^2 charts. In both cases ρ remains unaltered.

In this section we present the *ARL* values for the SU S^2 charts considering only bivariate processes ($p = 2$). The cases where $p > 2$ are already under investigation and the results will be presented in a future paper. The *ARL* values are obtained for $\rho = 0, 0.1, 0.5, 0.7, 0.9$ and $c^2 = 1.0, 1.1, 1.2, 1.3, 1.4, 1.5, 2.0, 3.0, 5.0$.

The $|\mathbf{S}|$ chart's performance is independent of ρ , while ρ has a minor influence on the SU S^2 charts' properties, see Table 7.

Table 8 compares the *ARL* for the SU S^2 charts with the *ARL* for the $|\mathbf{S}|$ chart (the generalized variance $|\mathbf{S}|$ chart) proposed by Alt (1985). It was built fixing $\rho = 0.0$. According to this table the univariate S^2 charts are always more effective than the generalized variance $|\mathbf{S}|$ chart, except in case II, with $\rho = 0.9$. In this case the difference is small, so, in the great majority of cases the univariate S^2 charts are preferable.

Table 7 – The *ARL* for the $SU S^2$ charts ($n=5$).

		case I					case II				
		ρ					ρ				
		0.0	0.1	0.5	0.7	0.9	0.0	0.1	0.5	0.7	0.9
c^2	<i>CL</i>	3.677	3.676	3.668	3.646	3.569	3.677	3.676	3.668	3.646	3.569
1.0		200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
1.1		132.10	132.10	132.48	132.77	132.07	139.14	139.14	139.72	140.50	142.13
1.2		86.49	86.49	86.79	86.79	84.48	101.64	101.65	102.44	103.56	105.78
1.3		58.12	58.12	58.30	58.11	55.45	77.14	77.16	78.03	79.25	81.63
1.4		40.60	40.60	40.70	40.44	38.09	60.46	60.48	61.36	62.58	64.94
1.5		29.52	29.52	29.57	29.31	27.42	48.69	48.71	49.57	50.75	53.00
2.0		9.62	9.62	9.62	9.50	8.91	21.63	21.65	22.33	23.19	24.78
3.0		3.38	3.38	3.38	3.34	3.21	8.64	8.66	9.09	9.59	10.48
5.0		1.67	1.67	1.67	1.66	1.63	3.73	3.74	3.98	4.25	4.71

Table 8 – The *ARL* for the $SU S^2$ charts and for the $|\mathbf{S}|$ chart.

		n								
		4			5			6		
		$ \mathbf{S} $	$SU S^2 *$	$SU S^2 **$	$ \mathbf{S} $	$SU S^2 *$	$SU S^2 **$	$ \mathbf{S} $	$SU S^2 *$	$SU S^2 **$
c^2	<i>CL</i>	6.134	4.106	4.106	5.375	3.677	3.677	4.820	3.375	3.375
1.0		200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
1.1		146.78	136.23	142.54	141.44	132.10	139.14	136.03	128.50	136.20
1.2		112.48	92.14	106.24	104.60	86.49	101.64	97.77	81.69	97.72
1.3		89.13	63.74	82.02	80.45	58.12	77.14	73.39	53.50	73.05
1.4		73.30	45.60	65.23	64.08	40.60	60.46	57.38	36.60	56.52
1.5		60.35	33.80	53.19	51.91	29.52	48.69	45.62	26.19	45.01
2.0		30.24	11.57	24.67	24.11	9.62	21.63	19.99	8.21	19.27
3.0		13.64	4.10	10.23	10.16	3.38	8.64	8.05	2.89	7.48
5.0		6.37	1.95	4.48	4.58	1.67	3.73	3.58	1.49	3.21

*case I; **case II

4.2 An example of application

In this section we consider the example given by Aparisi *et al.* (2001) to explain the use of a single chart based on the $\max(S_1^2, S_2^2)$ statistic and the generalized variance $|\mathbf{S}|$ chart. For monitoring the mean vector, Costa & Machado (2007) presented an interesting example that illustrates the use of a synthetic T^2 control chart with two-stage sampling to control bivariate processes.

The part in Figure 1 has two dimensions to be controlled, X_1 (distance between centers of the two interior holes) and X_2 (distance between the centers of the two lateral holes), correlated to each other with a correlation coefficient $\rho = 0.7$.

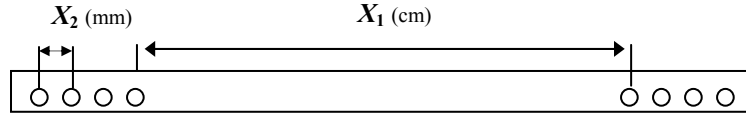


Figure 1 – Part of the example of application.

When the process is in-control the mean vector and the covariance matrix are known:

$$\boldsymbol{\mu}_0 = \begin{pmatrix} 10.0 \\ 10.5 \end{pmatrix}, \boldsymbol{\Sigma}_0 = \begin{pmatrix} 0.45 & 0.332 \\ 0.332 & 0.5 \end{pmatrix}. \text{ So, } |\boldsymbol{\Sigma}_0| = 0.114776.$$

We initially generate 30 samples of size $n = 5$ with the process in-control. The last 15 samples were simulated with $c^2 = 3.0$ and the same sample size. We consider the case I where the assignable cause increases only the variability of the first variable X_1 . In this case $\boldsymbol{\Sigma}_1$ is given by:

$$\boldsymbol{\Sigma}_1 = \begin{pmatrix} 1.35 & 0.575 \\ 0.575 & 0.5 \end{pmatrix}.$$

Table A5 presents the data of (X_1, X_2) , the sample variances, the sample covariances, the statistics $|\mathbf{S}|$, S_1^2 , S_2^2 and $\max(S_1^2, S_2^2)$.

The control limit of $CL = 1.747$ for the proposed model was determined by expression (A8) with $\gamma_1 = \gamma_2 = 1.0$, see the Appendix II. The control limit of $CL = 0.617$ for the $|\mathbf{S}|$ chart was determined by expression (11). For this example, a probability of Type I error of 5 per one thousand ($\alpha = 0.005$) is adopted.

Figures 2 and 3 show the generalized $|\mathbf{S}|$ chart and the control chart based on the $\max(S_1^2, S_2^2)$ statistic, respectively. Figure 2 shows that the disturbance is signaled at sample 44 (run length = 14) while Figure 3 shows that the chart signals at samples 39, 40, 43 and 44 (run length = 9), that is, the control chart based on the $\max(S_1^2, S_2^2)$ statistic is much more sensitive than its competitor.

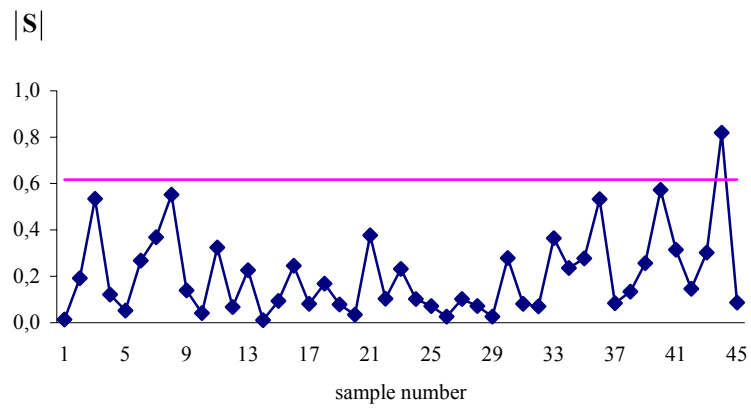


Figure 2 – Generalized variance $|S|$ chart.

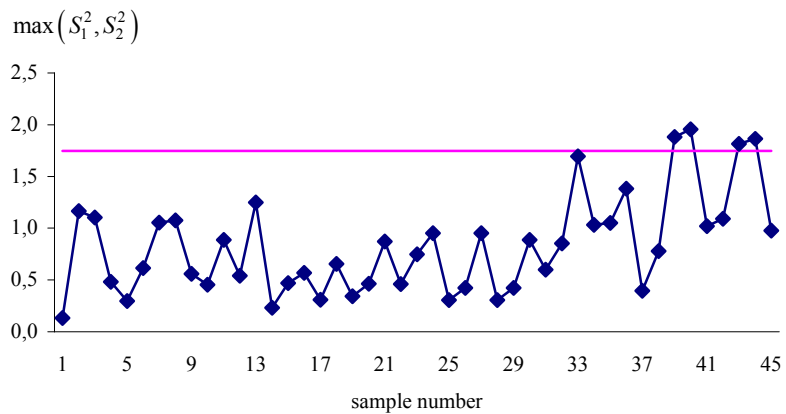


Figure 3 – Control chart based on the $\max(S_1^2, S_2^2)$ statistic.

5. Conclusions

In this article we provided an evaluation of the performance of the T^2 chart based on the principal components (PC chart) and the simultaneous univariate control charts based on the original variables (SU \bar{X} charts) or based on the principal components (SUPC charts).

The main reason to consider the T^2 chart based on the principal components lies on the dimensionality reduction. However, depending on the disturbance and on the way the original variables are related, the chart is very slow in signaling, except when all variables are negatively correlated and the principal component is wisely selected.

Comparing the SU \bar{X} , the SUPC and the T^2 charts we concluded that the SU \bar{X} charts (SUPC charts) have a better overall performance when the variables are positively (negatively) correlated.

We also developed the expression to obtain the power of two S^2 charts designed for monitoring the covariance matrix. The univariate S^2 charts always perform better than the generalized variance $|S|$ chart, except in case II, with $\rho=0.9$. In this case the difference is small, so, in the great majority of cases the univariate S^2 charts are preferable. These conclusions hold for the case of two variables. Whether they can be generalized for a large number of variables is still an open issue.

Additionally, the univariate S^2 charts have also better diagnostic feature, that is, with them it is easier to relate an out-of-control signal to the variables whose parameters have moved away from their in-control values.

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Appendix I – The Algorithm given in Serel *et al.* (2000) to obtain the control limits for univariate \bar{X} charts

Serel *et al.* (2000) developed numerical methods to obtain the two-sided control limits for the individual charts such that the overall type I risk of the system is near or equal to the desired value of α . We will describe here the method used to obtain the control limits for the bivariate case. They also studied higher-order cases.

When α_i is the type I risk of the Shewhart chart for variable X_i , its upper and lower control limits, $\mu_0 \pm h_i \sigma_i$ ($h_i > 0$), satisfy

$$\alpha_i = 2[1 - \Phi(h_i)], \text{ for } i = 1, 2, \quad (\text{A1})$$

where $\Phi(\cdot)$ denotes the standard normal cumulative distribution function. Let $\boldsymbol{\mu}_0 = (0, 0)$ and $\sigma_i = 1.0$. The out-of-control *ARL* for the specified shift Δ is given by

$$ARL(\Delta) = \left[1 - \Pr(-h_1 - \delta_1 < X_1 \leq h_1 - \delta_1, -h_2 - \delta_2 < X_2 \leq h_2 - \delta_2) \right]^{-1}. \quad (\text{A2})$$

The joint distribution in the right-hand side of (A2) is to be calculated with X_i 's being jointly distributed as a bivariate normal with a zero mean vector and the known covariance structure. The *ARL* given by (A2) is not for a particular chart, but is the joint *ARL* of two charts.

The cumulative distribution function of a bivariate normal with zero mean vector and correlation coefficient ρ is given by

$$B(x_1, x_2; \rho) = \int_{-\infty}^{x_1} \int_{-\infty}^{x_2} f(X_1, X_2) dX_1 dX_2.$$

It can be shown that

$$\begin{aligned} & \Pr(l_1 < X_1 \leq u_1, l_2 < X_2 \leq u_2) \\ &= B(l_1, l_2; \rho) - B(l_1, u_2; \rho) - B(u_1, l_2; \rho) + B(u_1, u_2; \rho). \end{aligned} \quad (A3)$$

The goal is to find the values h_1 and h_2 such that

$$\Pr(-h_1 < X_1 \leq h_1, -h_2 < X_2 \leq h_2) = 1 - \alpha.$$

Using (A3), the probability $(1 - \alpha)$ is given by

$$1 - \alpha = B(-h_1, -h_2; \rho) - B(-h_1, h_2; \rho) - B(h_1, -h_2; \rho) + B(h_1, h_2; \rho) \quad (A4)$$

By substituting the following equalities:

$$B(h_1, -h_2; \rho) = B(+\infty, -h_2; \rho) - B(-h_1, -h_2; -\rho), \quad (A5)$$

$$B(h_1, h_2; \rho) = B(+\infty, h_2; \rho) - B(-h_1, h_2; -\rho), \quad (A6)$$

into (A4) and rearranging, α_2 is given by

$$\alpha_2 = \alpha + B(-h_1, -h_2; \rho) - B(-h_1, h_2; \rho) + B(-h_1, -h_2; -\rho) - B(-h_1, h_2; -\rho). \quad (A7)$$

The Algorithm proposed by Serel *et al.* (2000) recursively finds the exact values of h_1 and h_2 satisfying (A7), given α , ρ , and r , where $r = \alpha_2/\alpha_1$. The underlying idea is to find the zero of an equation by successive substitutions. Subroutine DBNRDF from the IMSL Fortran library (1995) can be used to evaluate $B(x_1, x_2; \rho)$. The Algorithm has eight steps:

Step 0. Set the initial values of h_1 and h_2 based on a Bonferroni region (i.e., $\alpha = \alpha_1 + \alpha_2$):

$$\alpha_1 = \alpha/(1+r) \quad \text{and} \quad \alpha_2 = r\alpha_1,$$

$$\text{such that } h_1 = \Phi^{-1}(1 - \alpha_1/2) \quad \text{and} \quad h_2 = \Phi^{-1}(1 - \alpha_2/2).$$

Step 1. Update α_2 from (A5).

Step 2. Update α_1 from $\alpha_1 = \alpha_2/r$.

Step 3. Compute new values of h_1 and h_2 (from (A1)):

$$h_m = \Phi^{-1}(1 - 0.5\alpha_i), \quad i = 1, 2.$$

Step 4. If $|h_{2n} - h_2| < 0.0001$ go to step 7.

Step 5. $h_2 = h_{2n}$, $h_1 = h_{1n}$.

Step 6. Go to step 1.

Step 7. Stop. Current values of h_1 and h_2 are the solutions.

Appendix II – The power of the simultaneous univariate S^2 charts

Consider the statistics $S_1^2 = \frac{\sum_{j=1}^n x_{1j}^2}{n}$ and $S_2^2 = \frac{\sum_{j=1}^n x_{2j}^2}{n}$, where $x_{1j} = X_{1j} - \mu_1$, $x_{2j} = X_{2j} - \mu_2$. Let X_1 and X_2 be bivariate normal variables with mean vector $\mu_0 = (0,0)$ and covariance matrix $\Sigma_0 = \begin{pmatrix} 1 & \sigma_{12} \\ \sigma_{12} & 1 \end{pmatrix}$. The power of the SU S^2 is given by:

$$1 - \beta = 1 - \Pr[(S_1^2 < CL) \cap (S_2^2 < CL)]$$

where CL is the control limit.

The occurrence of the assignable cause changes the initial covariance matrix to $\Sigma_1 = \begin{pmatrix} \gamma_1^2 & \gamma_1 \gamma_2 \sigma_{12} \\ \gamma_1 \gamma_2 \sigma_{12} & \gamma_2^2 \end{pmatrix}$, being $\sigma_{12} = \rho$. For the case I $\gamma_1^2 = c^2$ and $\gamma_2^2 = 1$ (or $\gamma_2^2 = c^2$ and $\gamma_1^2 = 1$) and for the case II $\gamma_1 = \gamma_2 = \gamma$ and $\gamma^2 = c$, being $c^2 > 1$.

We know that

$$\frac{nS_1^2}{\gamma_1^2} = \sum_{i=1}^n \left(\frac{x_{1i}}{\gamma_1} \right)^2 \sim \chi_n^2.$$

The conditional density of a bivariate normal distribution is

$$x_{2i} | x_{1i} \sim N \left(\rho \frac{\gamma_2}{\gamma_1} x_{1i}, \gamma_2^2 (1 - \rho^2) \right).$$

Then

$$\frac{x_{2i} | x_{1i}}{\gamma_2 \sqrt{1 - \rho^2}} \sim N \left(\frac{\rho x_{1i}}{\gamma_1 \sqrt{1 - \rho^2}}, 1 \right).$$

Consequently

$$\frac{nS_2^2 | x_{11}, x_{12}, \dots, x_{1n}}{\gamma_2^2 (1 - \rho^2)} = \sum_{i=1}^n \left(\frac{x_{2i} | x_{1i}}{\gamma_2 \sqrt{1 - \rho^2}} \right)^2 \sim \chi_{n, (\rho^2 / (1 - \rho^2)) \chi_n^2}^2.$$

and

$$\Pr[(S_1^2 < CL) \cap (S_2^2 < CL)] = \int_0^{nCL/\gamma_1^2} \Pr\left[\chi_{n,(\rho^2/1-\rho^2)}^2 < \frac{nCL}{\gamma_2^2(1-\rho^2)}\right] \frac{1}{2^{n/2}\Gamma(n/2)} e^{-t/2} t^{(n/2)-1} dt \quad (A8)$$

During the in-control period $\gamma_1^2 = \gamma_2^2 = 1$, $\Pr[(S_1^2 < CL) \cap (S_2^2 < CL)] = 1 - \alpha$ and the expression (A8) is used to obtain the control limit CL for specified values of ARL_0 , reminding that $ARL_0 = 1/\alpha$. We used the subroutine DCSNDF available on the IMSL Fortran library (1995) to compute the probability in the expression (A8).

Appendix III – Tables A1 through A5

Table A1 – The ARL values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 2$ and $\rho = \pm 0.5$).

		ρ								
		-0.5			0			0.5		
δ_1	δ_2	PC1	PC2	T^2	PC1	PC2	T^2	PC1	PC2	T^2
0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.5	145.43	90.93	99.72	200.0	90.93	115.54	145.43	90.93	99.72
0.0	1.0	75.53	28.21	30.60	200.0	28.21	41.92	75.53	28.21	30.60
0.0	1.5	38.10	10.46	10.51	200.0	10.46	15.78	38.10	10.46	10.51
0.5	0.0	145.43	90.93	99.72	90.93	200.0	115.54	145.43	90.93	99.72
0.5	0.5	200.0	28.21	41.92	90.93	90.93	76.87	75.53	200.0	99.72
0.5	1.0	145.43	10.46	15.01	90.93	28.21	32.95	38.10	90.93	41.92
0.5	1.5	75.53	4.77	6.10	90.93	10.46	13.64	20.30	28.21	15.01
1.0	0.0	75.53	28.21	30.60	28.21	200.0	41.92	75.53	28.21	30.60
1.0	0.5	145.43	10.46	15.01	28.21	90.93	32.95	38.10	90.93	41.92
1.0	1.0	200.0	4.77	6.88	28.21	28.21	18.49	20.30	200.0	30.60
1.0	1.5	145.43	2.64	3.48	28.21	10.46	9.36	11.58	90.93	15.01
1.5	0.0	38.10	10.46	10.51	10.46	200.0	15.78	38.10	10.46	10.51
1.5	0.5	75.53	4.77	6.10	10.46	90.93	13.64	20.30	28.21	15.01
1.5	1.0	145.43	2.64	3.48	10.46	28.21	9.36	11.58	90.93	15.01
1.5	1.5	200.0	1.73	2.16	10.46	10.46	5.76	7.08	200.0	10.51

Table A2 – The *ARL* values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 2$ and $\rho = \pm 0.7$).

		ρ								
		-0.7			0			0.7		
δ_1	δ_2	PC1	PC2	T^2	PC1	PC2	T^2	PC1	PC2	T^2
0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.5	150.40	64.09	77.97	200.0	90.93	115.54	150.40	64.09	77.97
0.0	1.0	82.17	15.44	18.98	200.0	28.21	41.92	82.17	15.44	18.98
0.0	1.5	43.02	5.21	5.94	200.0	10.46	15.78	43.02	5.21	5.94
0.5	0.0	150.40	64.09	77.97	90.93	200.0	115.54	150.40	64.09	77.97
0.5	0.5	200.0	15.44	23.38	90.93	90.93	76.87	82.17	200.0	106.69
0.5	1.0	150.40	5.21	7.35	90.93	28.21	32.95	43.02	64.09	38.73
0.5	1.5	82.17	2.43	3.04	90.93	10.46	13.64	23.50	15.44	11.36
1.0	0.0	82.17	15.44	18.98	28.21	200.0	41.92	82.17	15.44	18.98
1.0	0.5	150.40	5.21	7.35	28.21	90.93	32.95	43.02	64.09	38.73
1.0	1.0	200.0	2.43	3.23	28.21	28.21	18.49	23.50	200.0	35.25
1.0	1.5	150.40	1.51	1.80	28.21	10.46	9.36	13.63	64.09	15.73
1.5	0.0	43.02	5.21	5.94	10.46	200.0	15.78	43.02	5.21	5.94
1.5	0.5	82.17	2.43	3.04	10.46	90.93	13.64	23.50	15.44	11.36
1.5	1.0	150.40	1.51	1.80	10.46	28.21	9.36	13.63	64.09	15.73
1.5	1.5	200.0	1.17	1.29	10.46	10.46	5.76	8.40	200.0	12.58

Table A3 – The *ARL* values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 3$ and $\rho_{12} = \rho_{13} = \rho_{23} = 0.3$).

			chart						
δ_1	δ_2	δ_3	PC1	PC2	PC3	PC12	PC13	PC23	T^2
0.0	0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.0	1.5	58.34	12.07	52.12	13.73	41.73	13.23	13.43
0.0	0.5	1.5	34.25	23.60	29.75	18.42	21.43	17.05	13.87
0.0	1.0	1.5	20.88	50.61	17.77	20.39	11.67	17.98	11.56
0.0	1.5	1.5	13.29	113.25	11.16	18.01	6.83	15.24	8.21
0.5	1.0	0.0	58.34	43.17	200.0	36.91	80.48	61.90	46.50
0.5	1.0	0.5	34.25	131.43	158.05	44.27	46.97	133.87	52.04
0.5	1.0	1.0	20.88	185.14	93.58	30.95	25.78	114.19	32.56
0.5	1.0	1.5	13.29	69.98	52.11	15.82	14.35	46.27	15.16

1.0	0.0	0.0	100.80	150.54	29.75	109.10	35.78	40.84	42.34
1.0	0.5	0.5	34.25	185.14	93.58	49.17	39.01	114.19	48.16
1.0	1.0	1.0	13.29	200.0	200.0	20.12	20.12	200.0	25.94
1.0	1.5	1.5	6.13	185.14	93.58	8.94	8.14	114.19	10.39
1.5	0.0	0.0	58.34	113.25	11.16	64.00	12.82	15.24	15.21
1.5	0.0	0.5	34.25	196.11	17.77	49.94	15.12	26.78	19.50
1.5	0.0	1.0	20.88	82.37	29.75	24.69	15.73	33.08	17.19
1.5	0.0	1.5	13.29	27.30	52.12	11.01	14.35	25.26	11.07

Table A4 – The *ARL* values for the standard T^2 chart and for the T^2 chart based on PCVs ($p = 3$ and $\rho_{12} = 0.8$, $\rho_{13} = 0.5$, $\rho_{23} = 0.2$).

δ_1	δ_2	δ_3	chart						T^2
			PC1	PC2	PC3	PC12	PC13	PC23	
0.0	0.0	0.0	200.0	200.0	200.0	200.0	200.0	200.0	200.0
0.0	0.0	1.5	100.18	12.26	20.61	16.21	26.05	9.10	10.69
0.0	0.5	1.5	60.60	21.35	4.91	22.39	6.04	4.65	5.14
0.0	1.0	1.5	37.02	39.68	1.99	26.80	2.26	2.28	2.40
0.0	1.5	1.5	23.32	77.57	1.25	26.51	1.32	1.39	1.42
0.5	1.0	0.0	62.76	68.33	60.33	51.50	47.76	50.22	41.37
0.5	1.0	0.5	43.65	182.43	25.14	60.79	21.82	36.80	27.64
0.5	1.0	1.0	30.80	135.82	11.75	40.82	10.60	16.63	13.02
0.5	1.0	1.5	22.13	45.08	6.20	20.21	5.68	7.05	5.89
1.0	0.0	0.0	97.78	190.00	4.86	119.41	6.48	7.00	8.24
1.0	0.5	0.5	41.20	194.73	47.49	58.91	31.86	66.80	40.24
1.0	1.0	1.0	18.69	151.38	104.04	26.63	24.15	111.82	29.41
1.0	1.5	1.5	9.45	100.79	8.00	12.66	4.68	10.75	5.54
1.5	0.0	0.0	55.69	178.67	1.76	74.39	2.06	2.19	2.40
1.5	0.0	0.5	38.89	140.50	2.40	50.49	2.76	3.12	3.28
1.5	0.0	1.0	27.60	46.87	3.62	24.16	3.84	4.27	4.10
1.5	0.0	1.5	19.95	16.82	6.08	10.99	5.39	5.06	4.37

Table A5 – Data for the illustrative example.

#	Observations					S_i	S_{12}	S	S_1^2	S_2^2	$\max(S_1^2, S_2^2)$	
	1	2	3	4	5							
1	X_1	9.79	9.72	10.44	10.51	10.04	0.13	-0.01	0.01	0.11	0.13	0.13
	X_2	10.59	10.56	10.71	10.48	11.28	0.10					
2		9.62	11.91	8.92	9.72	9.11	1.43	0.57	0.19	1.17	0.49	1.17
		9.85	11.07	9.57	10.09	9.67	0.36					
3		10.44	10.17	8.78	8.84	8.87	0.66	0.51	0.53	0.87	1.10	1.10
		11.53	10.33	10.26	8.48	9.99	1.19					
4		9.88	10.02	8.92	10.34	11.05	0.60	0.20	0.12	0.48	0.23	0.48
		10.84	10.57	9.80	11.21	10.55	0.27					
31		10.93	9.73	9.35	11.19	10.47	0.61	-0.01	0.08	0.60	0.20	0.60
		10.76	10.41	11.26	11.10	10.52	0.13					
32		10.76	8.82	10.41	11.25	10.75	0.87	0.14	0.07	0.85	0.18	0.85
		10.64	10.48	10.28	11.14	10.75	0.11					
33		11.09	10.29	10.96	12.51	9.89	1.00	-0.12	0.36	1.69	0.31	1.69
		11.37	10.34	10.63	9.73	10.13	0.38					
34		10.61	10.24	10.73	9.02	11.80	1.01	0.40	0.24	1.03	0.32	1.03
		10.24	10.48	10.23	10.07	11.62	0.40					
35		10.99	9.49	9.35	11.37	11.31	1.00	0.43	0.28	1.05	0.41	1.05
		10.94	9.65	10.53	11.52	10.80	0.47					
36		11.27	9.93	11.04	8.87	8.29	1.71	0.87	0.53	1.38	0.64	1.38
		11.64	10.63	11.34	10.44	9.41	0.76					
37		10.79	10.62	9.50	10.24	10.63	0.27	0.21	0.08	0.34	0.39	0.39
		10.70	10.01	9.47	10.48	11.29	0.48					
38		10.60	10.10	10.68	9.22	8.43	0.93	0.31	0.13	0.78	0.24	0.78
		10.54	10.15	10.79	10.51	9.51	0.25					
39		11.52	7.45	10.03	10.32	10.70	2.35	0.27	0.26	1.88	0.11	1.88
		10.91	10.10	10.73	10.58	10.07	0.14					
40		9.87	8.15	11.72	9.03	8.44	2.05	0.86	0.57	1.96	0.78	1.96
		10.02	9.38	11.19	10.17	9.14	0.64					
41		9.48	10.55	10.92	9.47	11.84	1.02	0.28	0.31	1.02	0.95	1.02
		11.52	11.11	10.80	10.81	12.28	0.38					
42		11.13	10.97	10.70	11.53	9.34	0.70	0.47	0.15	1.09	0.59	1.09
		11.34	11.23	11.02	11.33	9.63	0.53					
43		10.56	10.07	10.13	12.94	9.68	1.69	0.56	0.30	1.81	0.59	1.81
		10.84	11.08	10.43	12.04	10.84	0.36					
44		10.60	7.82	10.22	9.12	11.84	2.32	0.68	0.82	1.86	0.50	1.86
		11.44	10.43	10.46	9.84	11.59	0.55					
45		8.37	10.99	10.12	8.98	10.41	1.16	0.35	0.09	0.98	0.15	0.98
		10.10	11.20	10.63	10.24	10.66	0.18					

#: Sample Number