

Revisiting the First-Principles Approach to the Granular Gas Steady State

R. C. Proleon and W. A. M. Morgado

Departamento de Física, Pontifícia Universidade Católica do Rio de Janeiro

CP 38071, 22452-970 Rio de Janeiro, Brazil

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We extend a Fokker-Planck formalism, previously used to describe the behavior of a cooling granular gas, with a Hertzian contact potential and viscoelastic radial friction, giving a velocity dependent coefficient of restitution. In the present work, we study the more general case of a steady-state with finite kinetic energy, far from equilibrium, due to the coupling to an external energy-feeding mechanism. Also from first-principles, we extend the validity of the former results.

1 Introduction

The problem of a granular gas (GG) at a steady-state, under the action of an energy feeding mechanism, has been extensively studied by means of theoretical [1, 2, 3] and experimental methods [4, 5]. A GG presents many interesting and non-trivial properties concerning its statistical behavior, such as non-Gaussian velocity distributions [4, 6], energy equipartition breakdown [6, 7], vortices and clustering [8, 9, 10]. These interesting properties are a direct consequence of the inelastic behavior of a GG. No matter how small, any amount of inelasticity will make a GG completely different, in long times, from an elastic molecular gas. For instance, no matter how small the inelasticity is, the GG will eventually lose all its internal kinetic energy [11]. However, a more fundamental approach unifying all these aspects of granular physics is still lacking [13].

With the goal of obtaining a basic first-principles approach to the problem of an inelastic GG, Schofield and Oppenheim [12] derived a set of Fokker-Planck equations for the distribution of positions and velocities for the grain's centers of mass of a GG at the (not necessarily homogeneous) cooling state (no energy-feeding mechanism) tending to true thermal equilibrium. This is a very general method that depends on a time-scale separation between the internal relaxation processes of a grain (fast variables) and the evolution of the long wavelength phenomena for the GG (slow variables) [14]. It gives the velocity dependence for the coefficient of restitution found elsewhere [15, 16, 17].

In the present work, we introduced a well known energy-feeding mechanism to extend the validity of that previous approach to a GG in a steady-state of finite granular kinetic energy. The basic steps leading to an equation describing the time-evolution for the distribution include postulating the inelastic Boltzmann-Enskog equation [8, 9], adding energy feeding mechanisms such as the “democratic” vibration model [1], and deriving Fokker-Planck equations based

on a first-principles expansion around equilibrium [12], kinetic theory methods [18], Monte Carlo methods or molecular dynamics simulations [19]. Most of these are effective approaches that ignore the detailed collisional dynamics. Some authors did indeed take the time dependence for the collisional dynamics into account in their models [20]. Naturally, most models in the literature are based on *a posteriori* justifications for their assumptions.

We believe our model can show its usefulness in helping to set some of the stochastic and kinetic theory models used to describe granular gases in better theoretical footing. It explores the same expansion methods [14] used to derive stochastic equations for granular gases in the rapid flow state. In special, careful steps are taken to ensure that an appropriate non-equilibrium steady-state is correctly taken into account as the basis for the expansions methods. The Fokker-Planck equation thus obtained can be used as the starting point for the development of kinetic theory methods appropriate for granular gases. For didactic reasons, we keep most of the calculation details in the main body of the text.

In order to maintain our model system in a constant energy steady-state, we make use of the democratic model of energy feeding and derive the inelastic Boltzmann equation in that context. This mechanism is used because of its practicality. More realistic energy-feeding mechanisms can be modeled [6, 7]. It should be noticed that the typical granular energies for the GG steady state, compared to that of the thermal equilibrium situation, may typically be of the order of 10^{12} or larger.

This paper is organized as follows. In Section II, we describe the microscopic model. In Section III, we describe the energy-feeding mechanism used in the paper. In Section IV, we eliminate the fast degrees of freedom for the system and obtain the appropriate Fokker-Planck equations and the viscoelastic friction coefficient. In Sections V, VI, VII and VIII, we obtain the BBGKY hierarchy and proceed to

make the multiple time-scale analysis and to obtain the appropriate Boltzmann equation for the GG. In Section IX, a Sonine polynomials expansion is obtained for the distribution and its moments analyzed. In Section X, we analyze the properties of the steady-state distribution. In Section XI, we summarize the results and make our concluding remarks.

2 Fokker-Plank approach

We will follow closely the method used by Schofield and Oppenheim [12] and study a system of N spherical, smooth and identical grains of mass m constituted by M atoms, $M \gg 1$. The grains are large enough making quantum effects irrelevant. The only frictional forces acting on the particles are radial, along the collisional axis for two parti-

cles. The positions and momenta of the grains are defined below:

$$\mathbf{r}^N \equiv \{\mathbf{r}_1, \mathbf{r}_2, \dots, \mathbf{r}_N\} \text{ and } \mathbf{p}^N \equiv \{\mathbf{p}_1, \mathbf{p}_2, \dots, \mathbf{p}_N\}.$$

The microscopic degrees of freedom are atomic coordinates ξ^{MN} and atomic momenta π^{MN} ($\sum_{i=1}^M \pi_i^N = 0$) associated to each atom of every grain. We can simplify the notation by grouping these two sets of coordinates into:

$$\chi_I \equiv \{\xi^{MN}, \pi^{MN}\}, \text{ and } \chi_T \equiv \{\mathbf{r}^N, \mathbf{p}^N\}.$$

Thus, the complete Hamiltonian can be partitioned as

$$H(\chi_T, \chi_I) \equiv H_t(\chi_T) + H_i(\chi_I) + \phi(\chi_T, \chi_I), \quad (1)$$

where the terms above are given in the sequence.

The granular Hamiltonian:

$$H_t(\chi_T) = \sum_{i=1}^N \frac{\mathbf{p}_i^2}{2m} + U(\mathbf{r}^N) \equiv \frac{\mathbf{p}^{N2}}{2m} + U(\mathbf{r}^N). \quad (2)$$

The internal Hamiltonian:

$$H_i(\chi_I) = \sum_{i=1}^N \sum_{l=1}^M \frac{\pi_{il}^2}{2\mu} + V(\xi^{NM}) \equiv \frac{\pi^{N2}}{2\mu} + V(\xi^N). \quad (3)$$

The interaction (coupling) term:

$$\phi(\chi_T, \chi_I) = \sum_{i,j=1}^N \sum_{l,m=1}^M \phi(\mathbf{r}_i, \mathbf{r}_j, |\xi_{jm} - \xi_{il}|) \equiv \phi(\mathbf{r}^N, \xi^N). \quad (4)$$

The probability density for the system evolves according to the Liouvillian operator defined by:

$$L = L_I + L_T + L_\phi$$

where

$$L_T = -\frac{\mathbf{P}^N}{m} \cdot \nabla_{\mathbf{r}^N} + \nabla_{\mathbf{r}^N} U \cdot \nabla_{\mathbf{p}^N},$$

$$L_I = -\frac{\pi^N}{\mu} \cdot \nabla_{\xi^N} + \nabla_{\xi^N} V \cdot \nabla_{\pi^N},$$

and

$$L_\phi = \nabla_{\mathbf{r}^N} \phi \cdot \nabla_{\mathbf{p}^N} + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N}.$$

The Liouville equation reads

$$\partial_t \rho(\chi_T, \chi_I, t) = L \rho(\chi_T, \chi_I, t) \quad (5)$$

In the expression above, we need to average out the terms containing internal degrees of freedom in order to obtain an effective equation for the remaining granular degrees of freedom.

3 Energy feeding - Democratic Model

For dissipative systems, the rate of kinetic energy (E) loss due to the inelasticity during the collisions is given by

$$\begin{aligned} \left. \frac{\partial E}{\partial t} \right)_{Dissipation} &\equiv \frac{\partial}{\partial t} \left\langle \frac{\mathbf{P}^N \cdot \mathbf{P}^N}{2m} \right\rangle_{Dissipation} \\ &= \int d\chi_T d\chi_I \frac{\mathbf{P}^N \cdot \mathbf{P}^N}{2m} L \rho(\chi_T, \chi_I, t) \end{aligned} \quad (6)$$

In order to keep the system in a non-trivial steady-state, it is necessary to feed kinetic energy into it. In the sequence, we describe the so-called democratic model [1], which is equivalent to coupling the GG with a granular heat-bath.

We assume that each grain in the system will periodically gain random momentum. That momentum is assumed to be a vectorial random variable, with fixed amplitude (in fact it is a set of N random variables)

$$\vec{\zeta}^N = \zeta \hat{\zeta}^N,$$

where the unit vector $\hat{\zeta}$ is uniformly distributed on the sphere. It obeys:

$$\langle \vec{\zeta} \rangle = 0 \quad \text{and} \quad \langle \vec{\zeta}^2 \rangle = \frac{1}{2}\zeta^2.$$

The effect on the distribution $\rho(r^N, p^N, \chi_I, t)$ corresponds

to a shift that can be written as

$$\rho(r^N, p^N + \zeta^N, \chi_I, t) = e^{\zeta^N \cdot \nabla_p} \rho(r^N, p^N, \chi_I, t). \quad (7)$$

We assume that all grains are hit periodically, and simultaneously, with a period τ_0 . The heating rate corresponds to

$$\begin{aligned} \left(\frac{\partial E}{\partial t} \right)_{\text{Heating}} &\equiv \frac{\partial}{\partial t} \left\langle \frac{\mathbf{P}^N \cdot \mathbf{P}^N}{2m} \right\rangle_{\text{Heating}} = \frac{1}{\tau_0} \left\langle \int dp \frac{(\mathbf{P}^N)^2}{2m} (\rho(r^N, p^N + \zeta^N, \chi_I, t) - \rho(r^N, p^N, \chi_I, t)) \right\rangle \\ &= \int dp \frac{(\mathbf{P}^N)^2}{2m} \left\{ \frac{1}{2} \frac{\zeta^2}{\tau_0} \nabla_{p^N} \cdot \nabla_{p^N} \rho(r^N, p^N, \chi_I, t) \right\} + \mathcal{O}\left(\frac{\zeta^2}{\tau_0}\right). \end{aligned}$$

It is necessary to take the limits $\zeta, \tau_0 \rightarrow 0$, keeping the ratio $\frac{\zeta^2}{2\tau_0} \equiv M_\zeta$ fixed. We obtain exactly:

$$\left(\frac{\partial E}{\partial t} \right)_{\text{Heating}} = M_\zeta \int dp \frac{(\mathbf{P}^N)^2}{2m} \{ \nabla_{p^N} \cdot \nabla_{p^N} \rho(r^N, p^N, \chi_I, t) \}.$$

Hence, the time evolution term for the distribution, corresponding to the interaction with the heat bath, will be:

$$M_\zeta \nabla_{p^N} \cdot \nabla_{p^N} \rho(r^N, p^N, \chi_I, t).$$

The full Liouville-like Master Equation for the GG (now an open system) becomes

$$\frac{\partial}{\partial t} \rho(\chi_T, \chi_I, t) = \{ L + M_\zeta \nabla_{p^N} \cdot \nabla_{p^N} \} \rho(\chi_T, \chi_I, t). \quad (8)$$

Steady-state distribution:

In order to study the GG's steady-state, we need to make suitable expansions around a reference state. Our goal is to use a reference state that approximates the true steady-state solution $\rho_{SS}(\chi_I, \chi_T)$. That state can be chosen by noticing that a typical steady-state has its internal and granular degrees of freedom almost uncorrelated. A suitable state for expansions is given by

$$\frac{1}{Z} f(\chi_T) e^{-\beta(H_I + \phi)}, \quad (9)$$

where $f(\chi_T) \equiv \int d\chi_I \rho_{SS}(\chi_I, \chi_T)$, and

$$Z = \int d\chi_I d\chi_T f(\chi_T) e^{-\beta(H_I + \phi)}. \quad (10)$$

The form of Eq. 9 is not the same as the steady-state solution ρ_{SS} but it will stand for the expansion reference state used for obtaining a stochastic equation for the distribution of the granular degrees of freedom.

4 Elimination of fast degrees of freedom

The exact Liouville-like equation, Eq. 8, is unmanageable and can only be made tractable by eliminating the micro-

scopic (fast) degrees of freedom through an averaging process [21]. Thus, our goal is to find an effective equation for the reduced granular distribution:

$$W(\chi_T, t) = \int d\chi_I \rho(\chi_T, \chi_I, t) \quad (11)$$

We use the method of eliminating the fast variables [14, 21]. The idea is to consider some naturally occurring small parameter that sets the time-scale differences. In previous models for granular systems, that role was played by the mass ratio $\varepsilon = \sqrt{\frac{\mu}{m}}$ [12] reflecting the large number of atoms constituting a grain. However, for a realistic granular steady-state, the parameter ε has to be modified in order to take into account that the granular temperature

$$T_g \equiv \left\langle \frac{\mathbf{p}^2}{3m} \right\rangle$$

obeys $T_g \gg k_B T$. Since

$$\frac{P^2}{m} \sim m v_g^2 \sim T_g, \quad \text{and} \quad \frac{\pi^2}{\mu} \sim \mu \dot{\xi}^2 \sim k_B T,$$

the parameter $\varepsilon \sim \frac{v_g}{\xi} \sim \sqrt{\frac{\mu}{m} \frac{T_g}{k_B T}}$ sets the time scale separation for the granular gas. A typical value for it is of the order 10^{-3} whereas for previous models [12] it was of the order of 10^{-9} . The Liouville equation can be rewritten in a way that makes explicit the role of ε , associated with the slow part of L [12]

$$\partial_t \rho = L^{(0)} \rho + \varepsilon L^{(1)} \rho, \quad (12)$$

where

$$L^{(0)} = L_I + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N}$$

and

$$L^{(1)} = L_T + \nabla_{r^N} \phi \cdot \nabla_{p^N} + \frac{1}{2} \xi^2 \nabla_{p^N} \cdot \nabla_{p^N}.$$

In order to average over the fast degrees of freedom, we define a projection operator \mathcal{P} , projecting ρ onto the fast variables, and its complement $\mathcal{Q} = 1 - \mathcal{P}$. The projection operator must satisfy [14] (see appendix)

$$\mathcal{P}L^{(0)} = 0 \quad \text{and} \quad L^{(0)}\mathcal{P} = 0. \quad (13)$$

A solution is given by the projection operator \mathcal{P} acting upon a dynamical variable $g \equiv g(\chi_T, \chi_I, t)$ as

$$\mathcal{P}g = \tilde{q}(r, \chi_I) \int d\chi'_I g(\chi_T, \chi'_I, t) \quad (14)$$

where \tilde{q} is a function of the form of Eq. 9:

$$\tilde{q}(r, \chi_I) \equiv \frac{e^{-\beta(H_I + \phi)}}{\int d\chi_I e^{-\beta(H_I + \phi)}},$$

where we see that $\int d\chi_I \tilde{q}(r, \chi_I) = 1$.

The following identities guarantee that the condition given by Eq. 13 is satisfied:

$$\int d\chi_I (L_I + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N}) \equiv 0$$

and

$$(L_I + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N}) \tilde{q} = 0$$

We multiply Eq. 12 on the left by \mathcal{P} and also by \mathcal{Q} in order to obtain

$$\partial_t \mathcal{P}\rho = \varepsilon \mathcal{P}L^{(1)}\mathcal{P}\rho + \varepsilon \mathcal{P}L^{(1)}\mathcal{Q}\rho, \quad (15)$$

$$\partial_t \mathcal{Q}\rho = \mathcal{Q}L^{(0)}\mathcal{Q}\rho + \varepsilon \mathcal{Q}L^{(1)}\mathcal{P}\rho + \varepsilon \mathcal{Q}L^{(1)}\mathcal{Q}\rho. \quad (16)$$

By using the fact that the projectors obey

$$\mathcal{P}^2 \equiv \mathcal{P}, \quad \mathcal{P}\mathcal{Q} = \mathcal{Q}\mathcal{P} = 0, \quad \text{and} \quad \mathcal{Q}^2 \equiv \mathcal{Q},$$

we can write

$$\partial_t y = \varepsilon Ay + \varepsilon Bz, \quad (17)$$

$$\partial_t z = Ez + \varepsilon Cy + \varepsilon Dz, \quad (18)$$

where

$$y = \mathcal{P}\rho, \quad z = \mathcal{Q}\rho,$$

$$A = \mathcal{P}L^{(1)}\mathcal{P}, \quad B = \mathcal{P}L^{(1)}\mathcal{Q}, \quad C = \mathcal{Q}L^{(1)}\mathcal{P},$$

$$D = \mathcal{Q}L^{(1)}\mathcal{Q}, \quad E = \mathcal{Q}L^{(0)}\mathcal{Q}.$$

By switching to the slow time scale $s = \varepsilon t$ we obtain

$$\partial_s y = Ay + Bz, \quad (19)$$

$$\partial_s z = \frac{1}{\varepsilon} Ez + Cy + Dz. \quad (20)$$

We use an expansion for z as a function of the parameter ε

$$z = z^{(0)} + \varepsilon z^{(1)} + \varepsilon^2 z^{(2)} + \dots \quad (21)$$

and substitute it for z in Eq. 20. By grouping terms of equal order in ε we have

$$Ez^{(0)} = 0, \quad (22)$$

$$\partial_s z^{(0)} = Ez^{(1)} + Cy + Dz^{(0)}. \quad (23)$$

From above, we obtain the solution for $z^{(0)}$ and $z^{(1)}$:

$$z^{(0)} = 0 \quad \text{and} \quad z^{(1)} = -E^{-1}Cy. \quad (24)$$

By substituting the expression for $z^{(1)}$ in Eq. 19, we obtain an equation for y

$$\partial_s y = Ay - \varepsilon BE^{-1}Cy. \quad (25)$$

Now, it is necessary to compute the right hand side of the equation above. The first term is given by:

$$Ay = \mathcal{P}L^{(1)}y = \tilde{q}(r, \chi_I) (L_T + \langle \nabla_{r^N} \phi \rangle_o \cdot \nabla_{p^N} + M_\zeta \nabla_{p^N} \cdot \nabla_{p^N}) W(\chi_T, t), \quad (26)$$

where $\langle \nabla_{r^N} \phi \rangle_o = \int d\chi_I \tilde{p} \nabla_{r^N} \phi$. In order to find the second term, we need to calculate

$$\begin{aligned} Cy &= \mathcal{Q}L^{(1)}Py \\ &= \{ \tilde{q}(r, \chi_I) \} \{ L_T + M_\zeta \nabla_{p^N} \cdot \nabla_{p^N} \} W(\chi_T, t) \\ &\quad + W(\chi_T, t) \mathcal{Q} \{ L_T \tilde{q}(r, \chi_I) \} + \nabla_{p^N} W(\chi_T, t) \cdot \mathcal{Q} \{ \tilde{q}(r, \chi_I) \nabla_{r^N} \phi \}, \end{aligned} \quad (27)$$

where the first term of the right hand side cancels identically. By writing L_T explicitly in the second term we obtain

$$W(\chi_T, t) \mathcal{Q} \{ L_T \tilde{q}(r, \chi_I) \} = W(\chi_T, t) \mathcal{Q} \{ (-\frac{p^N}{m} \cdot \nabla_{r^N}) \tilde{q}(r, \chi_I) \} = W(\chi_T, t) \{ -\frac{p^N}{m} \cdot \nabla_{r^N} \tilde{q}(r, \chi_I) \}$$

It is easy to show that [12]

$$\nabla_{r^N} \tilde{q}(r, \chi_I) = -\beta \tilde{q}(r, \chi_I) \widehat{\nabla_{r^N} \phi}$$

where

$$\widehat{A}_{(\chi_T, \chi_I, t)} \equiv A_{(\chi_T, \chi_I, t)} - \int d\chi_I \tilde{q}(r, \chi_I) A_{(\chi_T, \chi_I, t)}.$$

Hence

$$W_{(\chi_T, t)} \mathcal{Q}\{L_T \tilde{\varrho}(r, \chi_I)\} = W_{(\chi_T, t)} \beta \tilde{\varrho}(r, \chi_I) \frac{P^N}{m} \cdot \widehat{\nabla_{r^N} \phi},$$

and

$$Cy = \tilde{\varrho}(r, \chi_I) \widehat{\nabla_{r^N} \phi} \cdot \left\{ \beta \frac{P^N}{m} + \nabla_{p^N} \right\} W_{(\chi_T, t)}. \tag{28}$$

In order to operate B onto Cy , we write B in a suitable way

$$\begin{aligned} B &\equiv \mathcal{P}L^{(1)}\mathcal{Q} \\ &\equiv \tilde{\varrho}(r, \chi_I) \int d\chi_I (L_T + \nabla_{r^N} \phi \cdot \nabla_{p^N} + M_\zeta \nabla_{p^N} \cdot \nabla_{p^N}) \mathcal{Q} \\ &\equiv \tilde{\varrho}(r, \chi_I) (L_T + \nabla_{r^N} \phi \cdot \nabla_{p^N}) \int d\chi_I \mathcal{Q} + \tilde{\varrho}(r, \chi_I) \int d\chi_I \nabla_{r^N} \phi \cdot \nabla_{p^N} \mathcal{Q}. \end{aligned}$$

Using that

$$\int d\chi_I \mathcal{Q} \equiv 0,$$

we obtain

$$B \equiv \tilde{\varrho}(r, \chi_I) \int d\chi_I \widehat{\nabla_{r^N} \phi} \cdot \nabla_{p^N} \mathcal{Q}. \tag{29}$$

Therefore

$$BE^{-1}Cy = \tilde{\varrho}(r, \chi_I) \int d\chi_I \widehat{\nabla_{r^N} \phi} \cdot \nabla_{p^N} \mathcal{Q} E^{-1} \tilde{\varrho}(r, \chi_I) \widehat{\nabla_{r^N} \phi} \cdot \left\{ \beta \frac{P^N}{m} + \nabla_{p^N} \right\} W_{(\chi_T, t)} \tag{30}$$

where the inverse operator of E can be written as [12, 21]

$$E^{-1} = - \int_0^\infty e^{\tau L^{(0)}} d\tau$$

By substituting this into Eq. 30, we have

$$BE^{-1}Cy = -\tilde{\varrho}(r, \chi_I) \int d\chi_I \left\{ \int_0^\infty d\tau \tilde{\varrho}(r, \chi_I) \widehat{\nabla_{r^N} \phi} e^{\tau L^{(0)\dagger}} \widehat{\nabla_{r^N} \phi} \right\} : \nabla_{p^N} \left\{ \beta \frac{P^N}{m} + \nabla_{p^N} \right\} W_{(\chi_T, t)} \tag{31}$$

Since $L^{0\dagger} = (L_I + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N})^\dagger = -(L_I + \nabla_{\xi^N} \phi \cdot \nabla_{\pi^N})$, we obtain

$$BE^{-1}Cy = -\tilde{\varrho}(r, \chi_I) \Gamma(r^N) : \nabla_{p^N} \left\{ \beta \frac{P^N}{m} + \nabla_{p^N} \right\} W_{(\chi_T, t)} \tag{32}$$

where

$$\Gamma(r^N) = \int_0^\infty d\tau \langle \widehat{\nabla_{r^N} \phi} e^{-\tau L^{(0)}} \widehat{\nabla_{r^N} \phi} \rangle_0. \tag{33}$$

Adding up the results above, and switching back to the time-scale $t = \varepsilon s$, we obtain a Fokker-Planck equation for the reduced granular distribution

$$\begin{aligned} \partial_t W_{(\chi_T, t)} &= \varepsilon (L_T + \langle \nabla_{r^N} \phi \rangle_o \cdot \nabla_{p^N} + M_\zeta dp \cdot \nabla_{p^N}) W_{(\chi_T, t)} \\ &\quad + \varepsilon^2 \Gamma(r^N) : \nabla_{p^N} \left\{ \beta \frac{P^N}{m} + \nabla_{p^N} \right\} W_{(\chi_T, t)}. \end{aligned} \tag{34}$$

The equation above can be expressed in a more convenient form as [12]

$$\begin{aligned} \partial_t W_{(\chi_T, t)} &= \varepsilon (L_T + \langle \nabla_{r^N} \phi \rangle_o \cdot \nabla_{p^N} + M_\zeta \nabla_{p^N} \cdot \nabla_{p^N}) W_{(\chi_T, t)} \\ &\quad + \frac{1}{2} \varepsilon^2 \sum_{ik} \gamma_{ik} \hat{\Gamma}_{ik} (\nabla_{p_i} - \nabla_{p_k}) \left\{ (\nabla_{p_i} - \nabla_{p_k}) + \beta \frac{(p_i - p_k)}{m} \right\} W_{(\chi_T, t)}, \end{aligned} \tag{35}$$

where, for short-ranged potentials, the radial friction coefficient is given by [1,15,22]

$$\gamma_{ik} \equiv \int_0^\infty d\tau \Gamma(r_{ik}, r_{ik}, \tau) = \int_0^\infty d\tau \langle \widehat{\nabla_{r_{ik}} \phi} [e^{-\tau L^{(0)}}] \widehat{\nabla_{r_{ik}} \phi} \rangle_0 \tag{36}$$

Eq. 35 has the same form as the one obtained by Schofield and Oppenheim [12], except for a new energy-injecting term. This fact shows their coherence and *a posteriori* justifies their use in deriving the behavior of a system of grains with $T_g \gg k_B T$ [15]. We have now established the correct form for the basic equation of our model and can proceed to study some of their physical properties. The Fokker-Planck equation 35 is the starting point for the hydrodynamic analysis. Its validity is based on the separation of internal and granular time-scales given by the condition that the parameter ε has to be small. However, in order to derive, from Eq. 35, the hydrodynamic equations appropriated for the granular steady-state, we need a few more physical assumptions, concerning the rate of energy dissipation, the

number density of the system and the rate of energy feeding.

5 BBGKY Hierarchy

In the following we simplify the notation by letting x_n stand for $(\mathbf{r}_n, \mathbf{p}_n)$. We define the reduced distributions below

$$f^{(n)} = \frac{N!}{(N-n)!} \int d\chi_{n+1} \dots d\chi_N W(\chi_{\mathbf{T}}, t). \quad (37)$$

By integrating Eq. 35 and using the definition of Eq. 37, we can compute the equations for the one-particle density $f^{(1)}$ and pair density $f^{(2)}$. For $f^{(1)}$ that reads [12]:

$$\begin{aligned} \frac{\partial}{\partial t} f^{(1)} + \frac{1}{m} p_1 \cdot \nabla_{r_1} f^{(1)} &= \int dx_2 (\nabla_{r_{12}} U(r_{12}) + \widehat{\nabla_{r_{12}} \phi(r_{12})}) \cdot \nabla_{p_1} f^{(2)} \\ &+ \int dx_2 \gamma_{12} \hat{\mathbf{r}}_{12} \hat{\mathbf{r}}_{12} (\nabla_{p_1}^2 + \frac{\beta}{m} \nabla_{p_1} p_1 - \frac{\beta}{m} \nabla_{p_1} p_2) f^{(2)} \\ &+ M_\zeta \frac{\partial^2}{\partial^2 p_1} f^{(1)}. \end{aligned} \quad (38)$$

Similarly for $f^{(2)}$ [12]:

$$\begin{aligned} \frac{\partial}{\partial t} f^{(2)} &= - \sum_{i=1}^2 \frac{p_i}{m} \cdot \nabla_{r_i} f^{(2)} - (\nabla_{r_{12}} U(r_{12}) + \widehat{\nabla_{r_{12}} \phi(r_{12})}) \cdot (\nabla_{p_1} - \nabla_{p_2}) f^{(2)} \\ &+ \gamma_{12} \hat{\mathbf{r}}_{12} \hat{\mathbf{r}}_{12} (\nabla_{p_1} - \nabla_{p_2}) (\nabla_{p_1} - \nabla_{p_2} + \frac{\beta}{m} (p_1 - p_2)) f^{(2)} \\ &- \sum_{i=1,2} \int dx_3 (\nabla_{r_{i3}} U(r_{i3}) + \widehat{\nabla_{r_{i3}} \phi(r_{i3})}) \cdot \nabla_{p_i} f^{(3)} \\ &+ \sum_{i=1,2} \int dx_3 \gamma_{i3} \hat{\mathbf{r}}_{i3} \hat{\mathbf{r}}_{i3} (\nabla_{p_i} - \nabla_{p_3} + \frac{\beta}{m} (p_i - p_3)) f^{(3)} \\ &+ M_\zeta (\frac{\partial^2}{\partial^2 p_1} f^{(2)} + \frac{\partial^2}{\partial^2 p_2} f^{(2)}) \end{aligned} \quad (39)$$

We shall estimate the order of magnitude of each term in both Eqs. 38 and 39). We assume the distribution to be uniform, that is $f^{(n)} \equiv f(p)$, we obtain [12]

$$\frac{\partial}{\partial s} f^{(1)} = -n^* L^1 f^{(2)} + n^* \theta N^1 f^{(2)} - K^1 f^{(1)} + n^* \theta M_\zeta \frac{\partial^2}{\partial^2 p_1} f^{(1)} \quad (40)$$

where

$$\begin{aligned} K^1 &= \frac{p_1}{m} \frac{\partial}{\partial r_1} \\ L^1 &= \int dx_2 F_{12} \frac{\partial}{\partial p_1} \\ N^1 &= \int dx_2 \gamma_{12} \hat{\mathbf{r}}_{12} \hat{\mathbf{r}}_{12} : \left(\frac{\partial}{\partial p_1} - \frac{\partial}{\partial p_2} \right) \left(\frac{\partial}{\partial p_1} - \frac{\partial}{\partial p_2} + \beta (p_1 - p_2) \right) \end{aligned}$$

and

$$\begin{aligned} \frac{\partial}{\partial t} f^{(2)} &= -K^2 f^{(2)} - I^2 f^{(2)} + \theta M^2 f^{(2)} - n^* L^2 f^{(3)} + n^* \theta N^2 f^{(3)} \\ &+ n^* \theta M_\zeta \left(\frac{\partial^2}{\partial^2 p_1} f^{(2)} + \frac{\partial^2}{\partial^2 p_2} f^{(2)} \right) \end{aligned} \quad (41)$$

with

$$\begin{aligned}
 K^2 &= \frac{P_1}{m} \frac{\partial}{\partial r_1} + \frac{P_2}{m} \frac{\partial}{\partial r_2} \\
 I^2 &= F_{12} \frac{\partial}{\partial P_1} + F_{21} \frac{\partial}{\partial P_2} \\
 M^2 &= \gamma_{12} \hat{f}_{12} \hat{f}_{12} : \left(\frac{\partial}{\partial p_1} - \frac{\partial}{\partial p_2} \right) \left(\frac{\partial}{\partial p_1} - \frac{\partial}{\partial p_2} + \frac{\beta}{m} (p_1 - p_2) \right) \\
 L^2 &= \int dx_3 F_{13} \frac{\partial}{\partial p_1} + \int dx_3 F_{23} \frac{\partial}{\partial p_2} \\
 N^2 &= \int dx_3 \gamma_{13} \hat{f}_{13} \hat{f}_{13} : \frac{\partial}{\partial p_1} \left(\frac{\partial}{\partial p_1} + \frac{\beta}{m} (p_1 - p_3) \right) \\
 &\quad + \int dx_3 \gamma_{23} \hat{f}_{23} \hat{f}_{23} : \frac{\partial}{\partial p_2} \left(\frac{\partial}{\partial p_2} + \frac{\beta}{m} (p_2 - p_3) \right)
 \end{aligned}$$

In the next section we use the time-scale separation method in order to obtain an inelastic Boltzmann equation for the granular gas in the democratic vibration regime.

6 Time-scale separation

We shall express the distribution functions as depending implicitly on the variable t through explicit variables [23] $\tau_0, \tau_1, \tau_2, \tau_3, \tau_4, \dots$, defined by

$$\tau_0 = s, \tau_1 = \theta s, \tau_2 = n^* s, \tau_3 = \theta^2 s, \tau_4 = n^* \theta s, \dots$$

Then, the time derivative becomes

$$\frac{\partial}{\partial s} = \frac{\partial}{\partial \tau_0} + \theta \frac{\partial}{\partial \tau_1} + n^* \frac{\partial}{\partial \tau_2} + \theta^2 \frac{\partial}{\partial \tau_3} + n^* \theta \frac{\partial}{\partial \tau_4} + \dots \quad (42)$$

The distributions $f^{(n)}$ will be expanded perturbatively as

$$f^{(n)} = f_0^n + \theta f_1^n + n^* f_2^n + \theta^2 f_3^n + n^* \theta f_4^n + \dots \quad (43)$$

We substitute equations (42) and (43) into (38) and collect terms to the correct order in the small parameters obtaining

$$\begin{aligned}
 \frac{\partial}{\partial \tau_0} f_0^1 &= -K^1 f_0^1 = 0 \\
 \frac{\partial}{\partial \tau_1} f_0^1 + \frac{\partial}{\partial \tau_0} f_1^1 &= 0 \\
 \frac{\partial}{\partial \tau_2} f_0^1 + \frac{\partial}{\partial \tau_0} f_2^1 &= -L^1 f_0^2 \\
 \frac{\partial}{\partial \tau_3} f_0^1 + \frac{\partial}{\partial \tau_1} f_1^1 + \frac{\partial}{\partial \tau_0} f_3^1 &= 0 \\
 \frac{\partial}{\partial \tau_4} f_0^1 + \frac{\partial}{\partial \tau_2} f_1^1 + \frac{\partial}{\partial \tau_0} f_4^1 + \frac{\partial}{\partial \tau_1} f_2^1 &= -L^1 f_1^2 + N^1 f_0^2 + M_\zeta \frac{\partial^2}{\partial^2 p_1} f_0^1
 \end{aligned} \quad (44)$$

Similarly for (39)

$$\frac{\partial}{\partial \tau_0} f_0^2 = -(K^2 + I^2) f_0^2 = -H^2 f_0^2 \quad (45)$$

$$\frac{\partial}{\partial \tau_1} f_0^2 + \frac{\partial}{\partial \tau_0} f_1^2 = -K^2 f_1^2 - I^2 f_1^2 + M^2 f_0^2 \quad (46)$$

For τ_0 we impose the initial condition

$$f_{i \gg 1}^{s > 1} = 0 \quad \text{e} \quad f_0^{s > 2} = \frac{N!}{N^s (N-s)!} \prod_s f_0^1 \quad (47)$$

By canceling the secular terms (for $\tau \rightarrow \infty$) we obtain

$$f_1^1 = f_3^1 = 0,$$

$$\frac{\partial}{\partial \tau_0} f_2^1 = \frac{\partial}{\partial \tau_0} f_4^1 = 0.$$

The following consistency equations must be satisfied

$$\frac{\partial}{\partial \tau_2} f_0^1 = -L^1 f_0^2 \quad (48)$$

$$\frac{\partial}{\partial \tau_4} f_0^1 = -L^1 f_1^2 + N^1 f_0^2 + M_\zeta \frac{\partial^2}{\partial^2 p_1} f_0^1 \quad (49)$$

The solutions for the Eqs. 45 and 46 are respectively

$$f_0^2(\tau_0) = e^{-H^2 \tau_0} f_0^2(0) \quad (50)$$

$$f_1^2(\tau_0) = e^{-H^2 \tau_0} \int_0^{\tau_0} d\lambda e^{H^2 \lambda} M^2 e^{-H^2 \lambda} f_0^1 f_0^1 \quad (51)$$

7 The Boltzmann collisional term

When $\tau_0 \rightarrow \infty$, we obtain from Eqs. 48 and 50

$$\frac{\partial}{\partial \tau_2} f_0^1 = -L^1 S_{12} f_0^1 f_0^1 \quad (52)$$

where $S_{12} = \lim_{\tau_0 \rightarrow \infty} e^{-H^2 \tau_0}$. Using the definitions of L^1 and S_{12} , we obtain

$$\frac{\partial}{\partial \tau_2} f_0^1 = \int dx_2 dp_2 F_{12} \frac{\partial}{\partial p_1} S_{12} f_0^1 f_0^1 \quad (53)$$

Using the property

$$K^2 S_{12} f_0^1 f_0^1 = I^2 S_{12} f_0^1 f_0^1 \quad \text{para} \quad \tau_0 \rightarrow \infty,$$

yields

$$\frac{\partial}{\partial \tau_2} f_0^1 = \int dx_2 dp_2 \frac{(p_1 - p_2)}{m} \frac{\partial}{\partial x_{12}} S_{12} f_0^1 f_0^1.$$

Making use of the Bogoliubov's scheme integration[23]

$$\frac{\partial}{\partial \tau_2} f_0^1 = \int dp_2 \frac{|p_1 - p_2|}{m} \int bdbd\epsilon \int dx \frac{\partial}{\partial x} S_{12} f_0^1 f_0^1,$$

we finally obtain the collisional term

$$\frac{\partial}{\partial \tau_2} f_0^1 = \int dp_2 d\Omega \frac{|p_1 - p_2|}{m} \sigma(\Omega) (f_0^1(p'_1) f_0^1(p'_2) - f_0^1(p_1) f_0^1(p_2)), \quad (54)$$

where $\sigma(\Omega) = bdbd\epsilon$ [24] and p'_1 and p'_2 are the momenta of grains before the collision that generate p_1 and p_2 .

$$+ N^1 S_{12} f_0^1 f_0^1 + M_\zeta \frac{\partial^2}{\partial^2 p_1} f_0^1 \quad (55)$$

8 The dissipative contribution and the energy feeding term

Equation (49) gives us

$$\frac{\partial}{\partial \tau_4} f_0^1 = -L^1 S_{12} \int_0^\infty d\lambda e^{H^2 \lambda} M^2 e^{-H^2 \lambda} f_0^1 f_0^1$$

The first term on the right hand side of the equation above is negligibly small when $\tau_0 \rightarrow \infty$. It is due to the application of operator $L^1 S_{12}$ to the integral [23]. Hence, by using explicitly the operator N^1 , the above equations becomes

$$\frac{\partial}{\partial \tau_4} f_0^1 = \int dx_2 dp_2 \gamma_{12} \hat{\mathbf{r}}_{12} \hat{\mathbf{r}}_{12} : \frac{\partial}{\partial \mathbf{p}_1} \left(\frac{\partial}{\partial p_1} + \frac{p_1 - p_2}{mk_B T} \right) S_{12} f_0^1 f_0^1 + M_\zeta \frac{\partial^2}{\partial^2 p_1} f_0^1. \quad (56)$$

We can write this last equation as a Fokker-Planck equation

$$\begin{aligned} \frac{\partial}{\partial \tau_4} f_0^1 &= \frac{\partial}{\partial \mathbf{p}_1} \int d\mathbf{x}_2 d\mathbf{p}_2 \gamma_{12} \hat{\mathbf{r}}_{12} \frac{\hat{\mathbf{r}}_{12} \cdot (\mathbf{p}_1 - \mathbf{p}_2)}{mk_B T} S_{12} f_0^1 f_0^1 \\ &+ \frac{\partial}{\partial \mathbf{p}_1} \frac{\partial}{\partial \mathbf{p}_1} : \int d\mathbf{x}_2 d\mathbf{p}_2 \gamma_{12} \hat{\mathbf{r}}_{12} \hat{\mathbf{r}}_{12} S_{12} f_0^1 f_0^1 + M_\zeta \frac{\partial}{\partial \mathbf{p}_1} \frac{\partial}{\partial \mathbf{p}_1} f_0^1 \end{aligned} \quad (57)$$

At low dissipation, we can approximate [22]

$$\begin{aligned} S_{12} f_0^1 f_0^1 &= S_{12} f_0^1(\mathbf{p}_1) f_0^1(\mathbf{p}_2) \\ &\approx f_0^1(\mathbf{p}_1) f_0^1(\mathbf{p}_2) e^{-\frac{\phi_{12}}{k_B T_g(\tau_4)}}, \end{aligned} \quad (58)$$

where ϕ_{12} is the elastic potential energy between grains. We define the granular temperature T_g by

$$T_g = \frac{1}{3mk_B} \langle \mathbf{p}^2 \rangle .$$

At the low density, low dissipation limit, the distribution is nearly Gaussian:

$$f_0^1(\mathbf{p}) \approx n \left(\frac{1}{2\pi m T_g(\tau_4)} \right)^{3/2} . \tag{59}$$

The inelastic contribution is then

$$\frac{\partial}{\partial \tau_4} f_0^1 = \frac{1}{mk_B T} \frac{\partial}{\partial \mathbf{p}_1} (f_0^1 \mathbf{p} \cdot \mathbf{A}) + \frac{\partial}{\partial \mathbf{p}_1} \frac{\partial}{\partial \mathbf{p}_1} : (f_0^1 \mathbf{A}) + M_\zeta \frac{\partial}{\partial \mathbf{p}_1} \frac{\partial}{\partial \mathbf{p}_1} f_0^1 \tag{60}$$

where \mathbf{A} is given by [22]

$$\mathbf{A} \approx \frac{4\pi\sigma^2}{3} \int_0^\infty dr \gamma(r) e^{-\frac{\phi_{12}}{k_B T_g(\tau_4)}} \propto T_g^{\frac{3}{5}} , \tag{61}$$

for a Hertzian potential ϕ_{12} .

The dissipative contribution reads

$$\frac{\partial}{\partial \tau_4} f_0^1 = A \frac{\partial}{\partial \mathbf{p}_1} \cdot \left[\frac{\partial}{\partial \mathbf{p}_1} + \frac{1}{mk_B T} \mathbf{p}_1 \right] f_0^1 + M_\zeta \frac{\partial}{\partial \mathbf{p}_1} \cdot \frac{\partial}{\partial \mathbf{p}_1} f_0^1 . \tag{62}$$

We finally obtain the Inelastic Boltzmann Equation:

$$\begin{aligned} \frac{\partial f_0^1}{\partial t} &= \int d\mathbf{p}_2 d\Omega \frac{|\mathbf{p}_1 - \mathbf{p}_2|}{m} \sigma(\Omega) (f_0^1(\mathbf{p}'_1) f_0^1(\mathbf{p}'_2) - f_0^1(\mathbf{p}_1) f_0^1(\mathbf{p}_2)) \\ &+ A \frac{\partial}{\partial \mathbf{p}_1} \cdot \left[\frac{\partial}{\partial \mathbf{p}_1} + \frac{1}{mk_B T} \mathbf{p}_1 \right] f_0^1 + M_\zeta \frac{\partial}{\partial \mathbf{p}_1} \cdot \frac{\partial}{\partial \mathbf{p}_1} f_0^1 \end{aligned} \tag{63}$$

The form of Eq. 63 is slightly different from the one used in reference [25]. However, a similar form has been proposed recently for a driven elastic hard sphere model that reproduces the physics of an inelastic GG [26]. These distinct equations should reproduce the same physics in the limit of a low density, low dissipation GG. We will check this in the next section.

the non-Gaussian velocity distribution has been obtained for systems with constant coefficients of restitution [28]. However, this is an approximation that becomes invalid as instabilities develop [29]. Since our model shows a velocity dependent coefficient of restitution, we need to study whether these instabilities are indeed present at long times, or disappear as shown for systems with velocity dependent coefficients of restitution [25].

9 Homogeneous Cooling State - HCS

By turning off the energy source, the granular temperature will tend to zero [27]. For an initially homogeneous system,

9.1 Sonine Polynomials Expansion

Eq. 63 is the starting point for the asymptotic analysis. We express it in terms of the velocity:

$$\begin{aligned} \frac{\partial}{\partial t} f(\mathbf{v}_1) &= \int d\mathbf{v}_2 d\Omega |\mathbf{v}_1 - \mathbf{v}_2| \sigma(\Omega) (f(\mathbf{v}'_1) f(\mathbf{v}'_2) - f(\mathbf{v}_1) f(\mathbf{v}_2)) \\ &+ \frac{A}{mk_B T} \frac{\partial}{\partial \mathbf{v}_1} \cdot \mathbf{v}_1 f(\mathbf{v}_1) , \end{aligned} \tag{64}$$

where $M_\zeta = 0$ and $\frac{k_B T}{T_g} \approx 0$.

We assume that the distribution scales with the granular velocity v_0 as [1]

$$f(\mathbf{v}, t) = \frac{n}{v_0^3} \tilde{f}(\mathbf{c}, t) \tag{65}$$

where

$$\mathbf{c} = \frac{\mathbf{v}}{v_0}, \quad n = \int d\mathbf{v} f(\mathbf{v}, t), \quad \tilde{\sigma} = \frac{\sigma(\Omega)}{\sigma_0^2}, \quad (66)$$

σ_0 being the granular diameter and $v_0 \equiv v_0(t)$ is given by $T_g(t) = \frac{1}{2} m v_0^2(t)$.

We obtain

$$-\frac{1}{v_0^2} \frac{d v_0}{d t} \left(3 + \mathbf{c} \cdot \frac{\partial}{\partial \mathbf{c}} \right) \tilde{f} + \frac{1}{v_0} \frac{\partial}{\partial t} \tilde{f} = \frac{\mu_2}{3} \left(3 + \mathbf{c} \cdot \frac{\partial}{\partial \mathbf{c}} \right) \tilde{f} + \frac{1}{v_0} \frac{\partial}{\partial t} \tilde{f} = n \sigma_0^2 I(\tilde{f}, \tilde{f}), \quad (67)$$

where

$$I(\tilde{f}, \tilde{f}) = I_1(\tilde{f}, \tilde{f}) + I_2(\tilde{f}),$$

and

$$I_1(\tilde{f}, \tilde{f}) = \int d\mathbf{c}_2 d\Omega |\mathbf{c}_1 - \mathbf{c}_2| \tilde{\sigma}(\Omega) (\tilde{f}(\mathbf{c}'_1) \tilde{f}(\mathbf{c}'_2) - \tilde{f}(\mathbf{c}_1) \tilde{f}(\mathbf{c}_2)), \quad (68)$$

$$I_2(\tilde{f}) = \frac{A}{n \sigma_0^2 m v_0 k_B T} \frac{\partial}{\partial \mathbf{c}_1} \cdot [\mathbf{c}_1 \tilde{f}(\mathbf{c}_1)]. \quad (69)$$

The approximations obey

$$\frac{m v_0^2}{k_B T} \ll 1, \quad A \ll n \sigma_0^2 m v_0 k_B T.$$

The function $\tilde{f}(c, t)$ will be expanded by means of Sonine polynomials

$$\tilde{f}(c, t) = \phi(c) \left\{ 1 + \sum_{p=1}^{\infty} a_p(t) S_p(c^2) \right\},$$

where

$$\phi(c) = \frac{1}{(2\pi)^{\frac{3}{2}}} e^{-\frac{c^2}{2}}.$$

We define the coefficients

$$\mu_n = - \int d\mathbf{c} |\mathbf{c}|^n I(\tilde{f}, \tilde{f}). \quad (70)$$

these will be useful in the sequence.

9.1.1 Calculation of μ_2

In this case, the term corresponding to $I_1(\tilde{f}, \tilde{f})$ cancels out due to the symmetry of the integrand [24]:

$$\int d\mathbf{c} c^2 I_1(\tilde{f}, \tilde{f}) = 0.$$

The second term does contribute to μ_2 :

$$\mu_2 = - \int d\mathbf{c} c^2 I_2 = \frac{3A}{n \sigma_0^2 m v_0 k_B T}, \quad (71)$$

where we used $\langle O \rangle = \int d\mathbf{c} \tilde{f} O \Rightarrow \langle c^2 \rangle = \frac{3}{2}$.

9.1.2 Calculation of μ_4

From the definition:

$$\mu_4 = - \int d\mathbf{c} c^4 \tilde{I}(\tilde{f}, \tilde{f}) = - \int d\mathbf{c} c^4 \left[\tilde{I}_1(\tilde{f}, \tilde{f}) + \tilde{I}_2(\tilde{f}) \right]. \quad (72)$$

We use the results in Ref. [25] to obtain

$$- \int d\mathbf{c} c^4 I_1(\tilde{f}, \tilde{f}) = 4\sqrt{2\pi} \left\{ a_2 + \frac{1}{32} a_2^2 \right\}, \quad (73)$$

and

$$- \int d\mathbf{c} c^4 I_2(\tilde{f}) = 15(1 + a_2) \frac{A}{n \sigma_0^2 m v_0 k_B T}. \quad (74)$$

The coefficient μ_4 then reads

$$\mu_4 = 4\sqrt{2\pi} \left\{ a_2 + \frac{1}{32} a_2^2 \right\} + 15(1 + a_2) \frac{A}{n \sigma_0^2 m v_0 k_B T}. \quad (75)$$

9.2 Long-time behavior

The granular temperature $T_g \equiv \frac{1}{2} m v_o(t)^2$ satisfies [25]

$$\frac{dT_g}{dt} = -\frac{1}{3} n \sigma_0^2 m v_0^3 \mu_2 = -\frac{2}{3} B T_g \mu_2 = -2 \frac{A}{m} \frac{T_g}{k_B T}, \quad (76)$$

where $A = \gamma T_g^{3/5}$ and $B = v_0(t) n \sigma_0^2$.

Expressing Eq. 76 as a function of the variable $u = T_g/T_{g0}$, where T_{g0} is the initial granular temperature, we obtain

$$\frac{d}{dt} u = -\frac{2\gamma}{m} \frac{T_{g0}^{3/5}}{k_B T} u^{8/5}. \quad (77)$$

The solution is given by

$$u = \left(1 + \frac{t}{\tau_o} \right)^{-5/3}, \quad v_0 = \sqrt{\frac{2T_{g0}}{m}} \left(1 + \frac{t}{\tau_o} \right)^{-5/6} \quad (78)$$

where

$$\tau_o = \frac{5m k_B T}{6\gamma T_{g0}^{3/5}}.$$

It is the equivalent of Haff's law [27] for systems with velocity dependent coefficients of restitution. The time dependence of a_2 is given by [25]:

$$\begin{aligned}
 \frac{d}{dt} a_2 &= \frac{4}{3} B \mu_2 (1 + a_2) - \frac{4}{15} B \mu_4 \\
 &= \frac{4}{3} n v_0 \sigma_0^2 \frac{3A}{n \sigma_0^2 m v_0 k_B T} (1 + a_2) \\
 &\quad - \frac{4}{15} n v_0 \sigma_0^2 \left[4\sqrt{2\pi} \left\{ a_2 + \frac{1}{32} a_2^2 \right\} + 15(1 + a_2) \frac{A}{n \sigma_0^2 m v_0 k_B T} \right] \\
 &= -\frac{16}{15} n v_0 \sigma_0^2 \sqrt{2\pi} \left\{ a_2 + \frac{1}{32} a_2^2 \right\}.
 \end{aligned} \tag{79}$$

The equation above agrees with Eq. (53) from the first article on Ref. [25]. Rewriting Eq. 79 as a function of u gives us

$$\frac{d}{dt} a_2 + c_2 \left\{ a_2 + \frac{a_2^2}{32} \right\} \left(1 + \frac{t}{\tau_0} \right)^{-5/6} = 0, \tag{80}$$

where

$$c_2 = \frac{32}{15} n \sigma_0^2 \sqrt{\frac{2\pi T_{g0}}{m}}.$$

At this order of approximation, the solution is given by

$$\begin{aligned}
 a_2(t) &= \frac{a_2(0)}{\left(1 + \frac{a_2(0)}{32} \right) e^{c_2 \tau_0 \left(1 + \frac{t}{\tau_0} \right)^{1/6}} - \frac{a_2(0)}{32}} \\
 &\Rightarrow a_2(t \rightarrow \infty) \rightarrow 0.
 \end{aligned} \tag{81}$$

The system tends to exhibit a Gaussian velocity distribution at long-times, as it becomes more elastic [25].

cooling state for low densities and low dissipation is thus well described by Eq. 63.

10 Steady-state

We now check the validity of our model against the results obtained from the inelastic Boltzmann-Enskog method [25] at the low density, low dissipation limit.

10.1 Collision operators

When the GG is acted upon by an energy-feeding mechanism, such as the democratic model defined earlier ($M_\zeta > 0$), a steady-state distribution tends to develop at the point where the rate of energy injection equals the rate of energy dissipation. The Dissipation-Vibration operator is given by

$$I_2(\tilde{f}) = \frac{A}{n \sigma_0^2 m v_0 k_B T} \frac{\partial}{\partial \mathbf{c}_1} \cdot \left[\mathbf{c}_1 \tilde{f}(\mathbf{c}_1) \right] + \frac{M_\zeta}{n \sigma_0^2 m^2 v_0^3} \frac{\partial}{\partial \mathbf{c}_1} \cdot \frac{\partial}{\partial \mathbf{c}_1} \tilde{f}. \tag{82}$$

At the steady state, the granular temperature is a constant and

$$\int d\mathbf{c} c^2 I_2(\tilde{f}) = 0 \Rightarrow 0 = \frac{A}{n \sigma_0^2 m v_0 k_B T} \int d\mathbf{c} c^2 \frac{\partial}{\partial \mathbf{c}} \cdot \left[\mathbf{c} \tilde{f} \right] + \frac{M_\zeta}{n \sigma_0^2 m^2 v_0^3} \int d\mathbf{c} c^2 \frac{\partial}{\partial \mathbf{c}} \cdot \frac{\partial}{\partial \mathbf{c}} \tilde{f},$$

giving the steady-state value

$$T_g(\infty) = \left(\frac{M_\zeta k_B T}{3\gamma} \right)^{5/8},$$

where we used $A = \gamma T_g^{3/5}$.

Thus, the operator I_2 can be put on the convenient form:

$$I_2(\tilde{f}) = \frac{M_\zeta T_g^{-3/2}}{2n \sigma_0^2 \sqrt{2m}} \left\{ 2 \left(\frac{T_g}{T_g(\infty)} \right)^{5/8} \frac{\partial}{\partial \mathbf{c}_1} \cdot \left[\mathbf{c}_1 \tilde{f}(\mathbf{c}_1) \right] + \frac{\partial}{\partial \mathbf{c}_1} \cdot \frac{\partial}{\partial \mathbf{c}_1} \tilde{f} \right\},$$

10.2 Distribution Tail

It is important to understand the behavior of distribution on the limit of largest velocities [1]. We shall study $I(\tilde{f}, \tilde{f}) = I_1(\tilde{f}, \tilde{f}) + I_2(\tilde{f}, \tilde{f})$, when $c \gg 1$, separately. In order to determine the behavior of the system at large velocities we will follow the Ansatz

$$f(c) \sim e^{-\varphi(t) c}. \quad (83)$$

For I_1 , we shall use the well known form [1]

$$I_1(\tilde{f}, \tilde{f}) \approx -\pi c \tilde{f}. \quad (84)$$

For I_2 , we notice that

$$\frac{\partial}{\partial \mathbf{c}} \cdot \frac{\partial}{\partial \mathbf{c}} \tilde{f} = -\frac{2\varphi}{c} \tilde{f} + \varphi^2 \tilde{f},$$

and

$$\frac{\partial}{\partial \mathbf{c}} \cdot (\mathbf{c} \tilde{f}) = 3\tilde{f} - \varphi c \tilde{f}.$$

The operator $I_2(\tilde{f})$ thus becomes

$$I_2(\tilde{f}) \approx -\frac{M_\zeta}{n\sigma_0^2 \sqrt{2mT_g(\infty)}^{\frac{8}{5}}} T_g^{\frac{1}{10}} \varphi c \tilde{f},$$

for $c \gg 1$.

For all values of c , we have

$$\frac{\mu_2}{3}(3+c) \cdot \frac{\partial}{\partial c} f + B^{-1} \frac{\partial}{\partial t} f = I(\tilde{f}, \tilde{f}),$$

In the limit of large c , and using

$$\frac{\partial}{\partial t} f = -\frac{d\varphi}{dt} c \tilde{f},$$

we derive an equation that allows us to calculate φ (at highest order on c):

$$\begin{aligned} -\frac{\mu_2}{3} \varphi c \tilde{f} - B^{-1} \frac{d\varphi}{dt} c \tilde{f} &= -c \tilde{f} \left[\pi + \frac{M_\zeta}{n\sigma_0^2 \sqrt{2mT_g(\infty)}^{\frac{8}{5}}} T_g^{\frac{1}{10}} \varphi \right], \\ \Rightarrow \frac{d\varphi}{dt} &= - \left[n\sigma_0^2 \mu_2 - \frac{3M_\zeta}{\sqrt{2mT_g(\infty)}^{\frac{8}{5}}} T_g^{\frac{1}{10}} \right] \left(\frac{2T_g}{9m} \right)^{\frac{1}{2}} \varphi + \pi n\sigma_0^2 \left(\frac{2T_g}{m} \right)^{\frac{1}{2}} \\ &= \pi n\sigma_0^2 \sqrt{\frac{2}{m}} T_g^{\frac{1}{2}}. \end{aligned} \quad (85)$$

The solution for the equation above is given by

$$\varphi(t) = \varphi(0) + \pi n\sigma_0^2 \sqrt{\frac{2}{m}} \int_0^t dt' T_g^{1/2}(t'). \quad (86)$$

Since

$$\lim_{t \rightarrow \infty} T_g(t) = T_g(\infty) = \left(\frac{M_\zeta k_B T}{3\gamma} \right)^{\frac{5}{8}} > 0,$$

the integral in Eq. 86 diverges as

$$\lim_{t \rightarrow \infty} \int_0^t dt T_g^{1/2} \sim t \rightarrow \infty. \quad (87)$$

Thus,

$$\lim_{t \rightarrow \infty} \varphi(t) \sim t \rightarrow \infty. \quad (88)$$

The result above shows that the overpopulation of the velocity tails will decrease with time, as was shown previously in Ref. [25].

11 Conclusions

The main motivation for the present work is to reformulate a first-principles approach to the stochastic behavior of a granular gas [12], done previously in the context of a cooling granular system, in order to include an energy feeding mechanism, in this case, the democratic model [1]. We believe this to be important since the results obtained in Ref. [12] have been successfully applied to describe the inelastic behavior of grains during a collision [15] and to derive the hydrodynamics of dilute granular gases [22].

Technically, we eliminate the fast (internal) degrees of freedom from the most general Liouville-like Master-Equation for the complete system. That is in fact a Liouville equation plus an energy-feeding term coupling the system to a thermal bath. A naturally occurring small parameter setting the time-scales is (typically) in this case

$$\varepsilon \equiv \sqrt{\frac{m k_B T}{\mu T_g}} \sim 10^{-3} \ll 1.$$

The expansion leads to a Fokker-Planck equation that incorporates the energy feeding term, and shows to be consistent,

in form, with the one obtained previously [12]. In order to study the granular hydrodynamic from it, we use the time-extension method [23] and obtain, as a consistency condition, a modified Boltzmann Equation appropriate for low density, low dissipation limit. Comparing with Ref. [25], we re-obtain the Sonine expansion results in lower order in density and dissipation, as expected. We also study the distribution's large velocity dependence for the cooling state and the constant energy steady-state and conclude that the results are consistent, on the correct approximation order, to the ones obtained by rather different methods [25].

In summary, the method satisfactorily describes the physics of inelastic, energy-fed systems at the low density, low dissipation limit. The stochastic equations obtained are consistent with the ones obtained by other methods, thus being able to serve as a basis for other theories describing flowing granular systems.

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