Thermoelectric properties of barium doped calcium cobaltite obtained by simplified chemical route

R.A. M. Machado¹, M. V. Gelfuso^{1*}, D. Thomazini¹

¹Federal University of Itajubá, Development of Functional Materials Group, Av. BPS 1303, 37500-903, Itajubá, MG, Brazil

Abstract

Calcium cobaltite (CCO) thermoelectric ceramics in $Ca_3Co_4O_9$ and $Ca_{2.95}Ba_{0.05}Co_4O_9$ compositions were produced by a simplified chemical route developed in this study. Undoped ceramics sintered at 1193 K for 12 h presented a bulk density equivalent to 77% of the theoretical density, one of the highest values ever found for conventionally sintered undoped calcium cobaltite. The presence of barium improved densification, reaching 80% of the theoretical density. Thermoelectric properties were discussed based on X-ray diffraction patterns, scanning electron micrographs, Seebeck coefficient, electrical and thermal conductivity. Electrical characterizations presented values of about 6200 and 7000 S/m at 873 K for undoped and doped ceramics, respectively. However, all ceramics presented almost the same range of activation energy values, indicating the possibility of non-effective substitution through this methodology. The maximum global PF (power factor) was 0.10 mW.m⁻¹.K⁻² for the densest undoped sample and an overall ZT (dimensionless figure of merit) of 0.07 for the undoped ceramic at 873 K. **Keywords**: thermoelectric ceramics, calcium cobaltite, barium.

INTRODUCTION

The dissipation of energy in the form of heat in automobiles, aircraft turbines, power plants, and factories is hardly recovered since there are several dissipative sources spread throughout the planet. This dissipation accounts for about 70% of the primary energy produced [1, 2]. To minimize this problem, thermal-electric energy converters can be used to partially recover this energy and increase the efficiency of the system. Thus, locally, it is possible to have a thermoelectric generator (TEG) made of semiconducting materials, fitting perfectly into this scenario. The classic thermoelectric generators are produced from intermetallic compounds, such as lead and bismuth tellurides, and silicongermanium. The extent of their application is limited by some factors: decomposition at relatively low temperatures, low availability of precursors, high toxicity, and cost. Therefore, it has been preferred to use thermoelectric oxides to act as charge carriers, because they avoid most of the intermetallic compound limitations [2]. In 1997, the discovery of the thermoelectric (TE) properties of sodium cobaltite (NaCo₂O₄) opened the way to the development of polycrystalline oxides capable of converting waste heat into usable energy [3]. Several high-performance thermoelectric oxides such as Ca₃Co₄O₉ [4], CaMnO₃ [5], SrTiO₃ [6], and donor-doped ZnO [7] were produced and improved. Among these materials, layered cobalt oxide Ca₃Co₄O₉, a CoO₂based oxide, has been the concern of many studies since it is a p-type semiconductor with wide application in the conversion of residual thermal energy. $Ca_3Co_4O_9$ structure consists of alternating layers of a distorted CaO-CoO-CaO rock salt-type layer (RS) and a CdI₂-type CoO₂ layer stacked in the direction of the c-axis. The bulk ceramics combine a high Seebeck coefficient around 125 μ V.K⁻¹ [4] with a relatively high electrical conductivity at room temperature.

Many approaches regarding the enhancement of TE performance of calcium cobaltite (CCO) are conveyed through doping with alkaline metals [8, 9], alkaline earth metals [10-13], transition metals [14, 15], and/or rareearth metals [16] at Ca site. A comparison between some synthetic routes in the obtention of $Ca_2Co_4O_6$ phase shows that attrition milling and chemical methods produce very reactive precursors, reflected in the decomposition of CaCO₂ after a single heat treatment at 1023 K for 12 h. The attrition milling and the classical solid-state methods still contain small amounts of Ca₃Co₂O₆ phase while the chemical method can produce near pure $Ca_3Co_4O_9$ phase [17]. The synthesis of calcium cobaltite by chemical route has been preferred since the reactants are mixed in stoichiometric proportions, which increases the reaction rate, allowing the obtention of a homogeneous powder with nanoscale particle size [2]. However, the synthesis of CCO ceramics with good thermoelectric properties and high density is a challenge due to the plate-like morphology of its particles, which can compromise green bodies packing and densification. Many studies have shown that the preparation methods can drastically influence the final bulk properties of CCO ceramics [17, 18], but synthesis methods have not yet been enough explored. This work consists of the evaluation

of the thermoelectric properties regarding the sintering conditions for undoped and Ba-doped $Ca_3Co_4O_9$ ceramics obtained through a simplified chemical route. The selection of barium ion as a dopant was justified by the enhancement of thermoelectric efficiency for CCO ceramics reported in literature obtained by solid-state reaction [10] and grain boundary segregation [11].

EXPERIMENTAL

Calcium carbonate (CaCO₃, Sigma-Aldrich, 99.0%), cobalt(II) nitrate hexahydrate [Co(NO₃), 6H,O, Sigma-Aldrich, 95.0%), and barium carbonate (BaCO₂, Sigma-Aldrich, 99.0%), used as precursors, were mixed to prepare the compositions Ca₃Co₄O₉ and Ca₂₉₅Ba_{0.05}Co₄O₉ via an alternative method. This simplified chemical route has been successfully used by our research group to prepare other electronic ceramics. In this methodology, only citric acid was used as a dissolving and chelating agent, differing from the sol-gel methodology in which ethylene glycol and/ or polyethylene glycol are used to polymerize the solution [12]. Cobalt nitrate was added to a 1 M aqueous citric acid solution under magnetic stirring at 353 K, until complete solubilization. Calcium carbonate and barium carbonate, the latter used for doping, were transferred to the beaker containing cobalt nitrate and citric acid solution under vigorous agitation. In this process, high effervescence and rapid color change from red to purple were observed. The purple solution was dried in an oven at 343 K until a foamy deep purple material was formed, which was manually ground to break the agglomerates. The calcination of the foam was carried out at 1073 K for 3.5 h in a furnace in an air atmosphere, as determined by differential thermal analysis (DTA, STA-449 F3, Netzsch). DTA was carried out in air up to 1273 K using an Al₂O₃ crucible, with a heating rate of 10 K/min and natural furnace cooling. Identical heating and cooling conditions were adopted for calcination. The calcined foams were manually ground aided by a porcelain mortar and uniaxially pressed at 100 MPa into discs of 12 mm in diameter, producing samples approximately 1 mm thick. Undoped (P) and doped (B) samples were sintered in air at 1173 K for 12 h (P-1173/12; B-1173/12) and 24 h (P-1173/24; B-1173/24), and at 1193 K for 12 h (P-1193/12; B-1193/12) with a heating rate of 10 K/min and natural furnace cooling. Sintering time and temperature were chosen based on previous works that evaluated the influence of these parameters on both doped and undoped ceramics [10, 17, 19].

The structural analysis of the calcined powders and sintered samples was done through X-ray diffraction (XRD) analysis (D8 Advance, Bruker) at room temperature (CuK α radiation) with 2 θ ranging between 10° and 50°, step of 0.02°, and exposure time of 1 s. Microstructural observations were performed by scanning electron microscopy (SEM, Phenom Pro-X, Thermo Fisher Sci.) coupled with energy dispersive spectrometry (EDS). Average particle and grain size were obtained through image analysis using SEM images aided by ImageJ software. Apparent density (0) of the samples was calculated by Archimedes method, based on ASTM B962-17 standard, which states that sintered parts cannot have their volumes accurately measured using micrometers or calipers [20]. Electrical conductivity (σ) measurements were conducted by the standard 4-probe DC method (SB-01, WT Ind.), using the sintered samples shaped in the form of a rectangular prism of about 10x2x1 mm in the air from room temperature up to 873 K, with a heating rate of 1 K/min and temperature gradient lower than 1 K. Seebeck coefficient (S) was measured after 5 min of steady-state using the same sample setup conditions for σ measurement, with a temperature gradient of 5 K and step of 25 K. The thermal diffusivity (α) and specific heat (C₂) of disk-shaped samples coated with graphite were obtained using the pulsed laser flash method (LFA-457, Netzsch) with 3 laser shots average, from room temperature up to 873 K, a step of 25 K, and performed after 2 min of steady-state, under N₂ atmosphere. The thermal conductivity (κ) of the samples was calculated from the measured α , C_p, and ϱ using Eq. A, as follows:

$$\kappa = \alpha . C_{p} . Q \tag{A}$$

RESULTS AND DISCUSSION

The DTA curves relative to precursors mixture of undoped and doped $Ca_3Co_4O_9$ are presented in Fig. 1. The curves show an exothermic peak close to 440 K, which was assigned to the evaporation of adsorbed water. The strong exothermic reaction observed between 590 and 750 K was due to the combustion of the organic compounds from citric acid [21]. Above 790 K, oxidation reactions and crystal formation occurred. According to DTA analysis, the formation process of $Ca_3Co_4O_9$ can be described as the removal of organic phase by calcination to form CaO and CoO, then the oxidation of CoO to Co_3O_4 by heating in the air, and finally, the reaction of inorganic oxides [16]. From



Figure 1: DTA curves of undoped and 0.05 Ba-doped CCO powders obtained by simplified chemical route.



Figure 2: X-ray diffraction patterns of undoped and 0.05 Ba-doped Ca₃Co₄O₉ powders and ceramics. Peaks of Ca₃Co₄O₉ phase are marked with \bullet ; Ca₃Co₂O₆ peaks are marked with \bullet .

the curves, it was possible to observe that the chemical reactions were completely finished at 1073 K, which was the temperature adopted as a reference for calcination. Furthermore, it should be noted that the $Ca_3Co_4O_9$ ceramic sintering temperature should not be higher than 1208 K. Above this temperature, $Ca_3Co_4O_9$ partially decomposes into $Ca_3Co_2O_6$, whose electrical resistivity is higher than that for $Ca_3Co_4O_9$ [22].

Fig. 2 displays similar XRD patterns for undoped and doped Ca₂Co₄O₀ powders. This analysis showed that only the $Ca_2Co_4O_6$ phase was present after calcination, according to JCPDS file 23-110, even with Ba addition into CCO composition. Constantinescu et al. [10] attributed this effect to the fact that Ba2+ ions have mainly entered into the Ca₂Co₂O₂ structure, substituting calcium ions in the b₂-axis $([Ca_2CoO_3]$ type layers), once it is considerably larger than the b₁-axis (corresponding to the [CoO₂] layer). On the other hand, Carvillo et al. [11] observed the segregation of Ba ion at the grain boundary, not being incorporated in the CCO structure. Regarding the sintered samples, Fig. 2 shows that the major peaks in XRD patterns are associated with the Ca₂Co₄O₆ phase, in agreement with previously reported data [10]. Some peaks of the Ca₃Co₂O₆ phase (JCPDS file 21-0139, shown as \blacklozenge in Fig. 2) could be observed on XRD patterns for both undoped and doped ceramics, being more evident in the last. It suggested that Ba2+ addition caused a slight increase in Ca₃Co₂O₆ phase content. However, in the Ba-doped samples, there is no noticeable effect on peak displacement related to the distortion of the structure, neither in Ca₃Co₄O₉ nor in Ca₃Co₂O₆ phases, probably due to the small amount of doping with Ba ion [10], or, more likely, due to the segregation of barium ions in the grain boundary [11]. Furthermore, Ba segregation at grain boundaries could be attributed to the mismatch size effect of the ionic radius in the lattice. The ionic radius of Ba2+ is 149 pm, significantly

larger than those for Ca^{2+} (114 pm) or Co^{3+} (68.5 pm) ions [23], preventing Ba^{2+} ions to fit in the sites occupied by those ions. Based on the Ca-Co-O phase diagram [22], the $Ca_3Co_2O_6$ phase formation started at ~1070 K, close to calcination temperature. Moreover, a rich oxygen atmosphere during calcination and sintering can stabilize the $Ca_3Co_4O_9$ phase [24], avoiding CCO decomposition into $Ca_3Co_2O_6$ and CoO, according to Eq. B. As the second phase could be observed on XRD only for ceramics, it follows that the decomposition of the $Ca_3Co_4O_9$ phase mainly occurred during the sintering process for both compositions, due to higher temperature and air atmosphere.

$$CCO \rightarrow Ca_3Co_2O_6 + 2CoO + \frac{1}{2}O_2(g)$$
(B)

Table I shows the apparent densities for all ceramics. Density values for undoped ceramics were between 3.10 and 3.60 g/cm³, while for doped ceramics, the values were between 3.52 and 3.73 g/cm³. The sintering condition at 1193 K for 12 h produced ceramics with the highest densification values for both compositions, that is, undoped and doped ceramics. Compared to the theoretical density value of 4.677 g/cm³ for Ca₂Co₄O₆ ceramic [25], the highest relative densities were about 77% and 80% for undoped (P-1193/12) and doped (B-1193/12) ceramics, respectively. Constantinescu et al. [10] produced undoped and Ba-doped CCO ceramics through solid-state reaction and the apparent densities for ceramics sintered at 1173 K for 24 h ranged from 72%, for the undoped ceramics, to 77%, for the 0.05 Badoped ones. This indicated that raising sintering temperature by only 20 K, from 1173 to 1193 K, could improve the densification process and shorten sintering time.

Table I - Apparent and relative densities, mean particle/grain sizes, and standard deviations of powders and ceramics.

Sample	Apparent density (g/cm ³)	Relative density (%)	Particle/ grain size (nm)
Undoped CCO powder	-	-	525±116
P-1173/12	3.10	66	1213±293
P-1173/24	3.25	69	1391±245
P-1193/12	3.60	77	1734±402
Doped CCO powder	-	-	521±97
B-1173/12	3.52	75	909±312
B-1173/24	3.57	76	1262±262
B-1193/12	3.73	80	1452±287

Fig. 3 shows SEM micrographs of CCO particles. Particles seemed to be strongly agglomerated in both undoped (Fig. 3a) and doped (Fig. 3e) CCO powders. Typical features of the chemical synthesis route can also be distinguished in the micrographs, composed of randomly oriented plate-like particles of different sizes, even with Ba-doping. Fig. 3 also presents SEM micrographs of the surfaces of P-1173/12 (Fig. 3b), P-1173/24 (Fig. 3c), P-1193/12 (Fig. 3d), B-1173/12 (Fig. 3f), B-1173/24 (Fig. 3g), and B-1193/12 (Fig. 3h) ceramics. The apparent thickness along the c-axis was given by the stacking of very thin plate-like grains of Ca₂Co₄O₆ [26], which confirmed that the preferential crystal-growth is produced along the a-b crystallographic plane. Also, it can be seen that the porosity decreased when barium was present. Table I presents mean particle size values, which were around 520 nm for both powders, and also shows grain size for undoped and doped ceramics. It has been found that grain sizes measured in the planar dimensions were in the range of 1213 to 1734 nm for undoped ceramics. The grain sizes for Ba-doped ceramics were between 909 and 1452 nm, being in agreement with other works in the literature [10, 26]. However, a slight decrease in the grain size of Ba-doped ceramics can be detected as a consequence of a small amount of liquid phase that could have enhanced the densification during the sintering process. The mechanism of the liquid phase sintering process originated from the solution-reprecipitation processing could suppress the coarsening of grain growth, producing a finer microstructure for Ba-doped ceramics [27]. As also confirmed by EDS analysis, undoped ceramics were mainly composed by the Ca₂Co₄O₆ phase, and Ba ion was not identified due to its very low concentration in the samples.

Fig. 4 shows the temperature dependence of the electrical conductivity (σ) for the ceramics. In comparison with P-1193/12 ceramic, some increase of σ was obtained by B-1193/12 ceramic from 6200 to around 7000 S/m at 873 K. Electrical conductivity values between 6500 and 8500 S/m at 873 K were found for undoped CCO produced by sol-gel route

[28] and coprecipitation method [17] for ceramics sintered at 1173 K for 24 h. This work shows that Ba-doping associated with a simplified methodology can lead to values of electrical conductivity close to those obtained from complex synthesis methods. Higher sintering temperature favors grain growth for both undoped and doped ceramics, as can be noted in Table I. Although Ba-doped ceramics exhibit a finer microstructure, P-1193/12 and B-1193/12 ceramics were denser than the others, which favored the electrical conductivity due to reduced porosity [29]. Also, as discussed before, barium doping reduced the porosity of the ceramics, which enhanced σ values. The P-1173/12 ceramic body had a relative density of 66% and the lowest σ , whereas B-1173/12 reached 5500 S/m at 873 K due to a 9% increase in relative density.



Figure 4: Electrical conductivity (σ) as a function of temperature for undoped and 0.05 Ba-doped CCO ceramics up to 873 K.



Figure 3: SEM micrographs of $Ca_3Co_4O_9$ particles (a), and undoped bodies sintered at 1173 K/12 h (b), 1173 K/24 h (c), and 1193 K/12 h (d); $Ca_{2.95}Ba_{0.05}Co_4O_9$ particles (e), and doped bodies sintered at 1173 K/12 h (f), 1173 K/24 h (g), and 1193 K/12 h (h).

At 600 K the CCO ceramics show small polaron conducting behavior, where the charge transport process in this system is a hole hopping from Co^{4+} to Co^{3+} [17]. At higher temperatures, there is a change to a semiconducting mechanism. According to the polaron theory, the electrical conductivity of a small polaron hopping conduction mechanism can be written as:

$$\sigma = n.e.a^2 \frac{A}{T} \exp \frac{-E_p}{K_B T}$$
(C)

where n, e, a, E_p , K_B , and A are the carrier concentration, the electron charge of the carrier, the intersite distance of hopping, the polaron activation energy, the Boltzmann constant, and a pre-exponential term related to the scattering mechanism, respectively [9]. For materials with semiconducting behavior, the electrical conductivity can be described by the Arrhenius equation as:

$$\sigma = \sigma_0 \exp \frac{-E_a}{K_B T}$$
(D)

where σ_0 is the pre-exponential term and E₀ is the Arrhenius activation energy. Linear relationships can be obtained at two temperature ranges: below 600 K, representing the small polaron-hopping conduction mechanism [15]; and above 600 K, indicating the semiconducting mechanism. As shown in Fig. 5, the E_p and E_a activation energies were obtained from a plot of $\ln(\sigma T)$ or $\ln(\sigma)$ versus 1000/T, respectively. Table II presents the E_p and E_a values for every ceramic, related to each carrier conducting behavior. E_p values were lower than previously reported values for the CCO system ranging from 0.066 to 0.085 eV for K [9] and Bi [27] doped ceramics. It was noted that the E₂ values were lower than the E_n values, which can be associated with higher carrier transport efficiency by semiconducting mechanism than polaron mechanism. It is known that polaron mobility is reduced since the binding energy of the carrier to the polarized lattice must be overcome, becoming highly



Figure 5: Activation energy plots of electrical conductivity for undoped and 0.05 Ba-doped CCO ceramics. The lines are linearly fitted using a least-squares method.

temperature-dependent. In this case, the polaron presents higher activation energy than a semiconductor material, where the electrons in the conduction band and holes in the valence band may be considered as quasi-free particles [30]. Moreover, both undoped and doped ceramics presents almost the same range of activation energy values, which can indicate that Ba-doping does not alter the electronic structure of the ceramics, once it may be segregated in the grain boundary [11].

Table II - Arrhenius (E_a) and polaron (E_p) activation energy for undoped and doped ceramics.

Ceramic	$E_{p}(eV)$	E _a (eV)
P-1173/12	0.046	0.039
P-1173/24	0.037	0.033
P-1193/12	0.050	0.021
B-1173/12	0.049	0.032
B-1173/24	0.043	0.028
B-1193/12	0.040	0.034

Fig. 6a shows the thermal conductivity (κ) of the ceramics and its temperature dependence. There was a reduction in thermal conductivity with increasing temperature due to increased vibrations, which reduced phonon mean free path. As mentioned, Ba-ion doping enhanced electrical conductivity by increasing the density of the ceramics. Although grain growth promoted by high sintering temperature at 1193 K favored electrical conductivity, denser bulks also favored the enhancement of thermal conductivities, which had a negative impact on the thermoelectric performance of the ceramic. Thus, the plots on Fig. 6a are in agreement with density values presented in Table I. Carvillo et al. [11] produced doped ceramics with κ values between 1.7 and 1.8 W.m⁻¹.K⁻¹ at ~870 K. They observed that Ba-doping reduced the thermal conductivity of Ca₃Co₄O₉ ceramics mainly due to phonon scattering enhanced by Ba ion segregation in the grain boundary, but the effect of doping on density and grain size was not evaluated. For undoped ceramics produced by conventional [11], microwave [31], or cold sintering process [18], the thermal conductivity is about 2.38, 1.38, and 0.98 W.m⁻¹.K⁻¹, respectively, which are in agreement with the values obtained in this work.

As shown in Fig. 6b, the Seebeck coefficient values for P-1173/24, P-1193/12, B-1173/12, and B-1173/24 ceramics presented almost the same values (from 111 to 116 μ V/K) and near typical to the ones reported in the literature (~125 μ V/K) at room temperature [4]. On the other hand, P-1173/12 ceramic showed a slightly different behavior, which had a higher Seebeck value (130 μ V/K) at room temperature. The B-1193/12 ceramic, which presented the highest density and electrical conductivity, also presented the lowest Seebeck value at room temperature. At 873 K, higher Seebeck values in the range of 130 to 140 μ V/K were observed for undoped samples, while Ba-doping



Figure 6: Thermal conductivity, κ (a), and Seebeck coefficient, S (b), as a function of temperature for undoped and 0.05 Ba-doped CCO ceramics up to 873 K.

reduced its value. In literature, Seebeck coefficient values for CCO ceramics can vary between 100 and 200 μ V/K [24, 27, 31, 32], but also, values lower than 100 μ V/K [18, 29] are observed. The reduction in Seebeck coefficient can be attributed to high charge carrier concentration in materials, which leads to an increase in electrical conductivity [33]. Another issue that can affect Seebeck coefficient values is the grain size [34]; when the grain size decreases, S values can also be reduced. However, the concentration of charge carriers can decrease with increasing porosity, and cause a moderate increase in S values [24]. In the present study, doped ceramics presented higher density, lower grain size, and higher electrical conductivity values in comparison to undoped ceramics. The association of these factors contributed to reducing the Seebeck coefficient values in doped ceramics.

Fig. 7a shows that benefiting from both the increased S and σ , P-1193/12 ceramic reached the highest power factor (PF=S² σ) of 0.10 mW.m⁻¹.K⁻² at 873 K, immediately followed by B-1193/12 ceramic (0.09 mW.m⁻¹.K⁻² at 873 K) due to

the higher σ value. This behavior is explained by the fact that Ba-doping reduces S, which has a quadratic relation with PF. Gunes and Ozenbas [29] produced undoped CCO ceramics by a more complex sol-gel method with reflux adding 0, 3%, 5%, and 7% of polyethylene glycol (PEG). In this study, the authors found PF values ranging from 0.10 to 0.16 mW.m⁻¹.K⁻² at 873 K, increasing with the percentage of PEG. In the study of CCO ceramics obtained by solid-state reaction [10], the PF value for the 0.05 Ba-doped sample was 0.21 mW.m⁻¹.K⁻² at 873 K. On the other hand, through non-stoichiometric addition of Ba, Ca₃Ba_{0.05}Co₄O₉ ceramics prepared by a sol-gel chemical solution route exhibited a PF higher than 0.80 mW.m⁻¹.K⁻² at 873 K [11]. In these studies, the grain size of the ceramics was not evaluated by the authors [10, 11], but was estimated based on published SEM images, being bigger than 2 µm, higher than those obtained in this study. Smaller grain size can reduce the electrical conductivity of the CCO ceramics [18], and in this case, can be related between Table I and Fig. 4, decreasing the PF values of the ceramics as noted in Fig. 7a.



Figure 7: Power factor, $S^2\sigma$ (a), and figure of merit, ZT (b), as a function of temperature for undoped and 0.05 Ba-doped CCO ceramics up to 873 K.

The plots of the dimensionless figure of merit (ZT) as a function of temperature are shown in Fig. 7b. ZT is related to efficiency conversion and can be calculated using Eq. E. It can be seen that undoped ceramics presented higher ZT values than doped ones. Despite the electrical conductivity improvement, Ba-doping also produced ceramics with higher thermal conductivity, due to the increase in density. It can be seen that the increase in thermal conductivity and Seebeck coefficient reduction were more significant than the electrical conductivity improvement, which is harmful to increase ZT values, based on Eq. E. As a result, the maximum ZT value for a doped ceramic was 0.05 at 873 K (B-1173/12). At last, the highest overall ZT value was 0.07 for the P-1173/24 ceramic at 873 K. Highest ZT achieved for pure calcium cobaltite samples was around 0.16 at 773 K produced by sol-gel and spark plasma sintering [35]. In the study performed by Carvillo et al. [11], they obtained ZT values of 0.21 and 0.52 at 1023 K for undoped and doped ceramics, respectively. Besides the additionally doping methodology, the ceramics were produced in an oxygen atmosphere, which substantially increased the electrical conductivity, and consequently, increased the ZT values of the ceramics.

$$ZT = \frac{S^2 \cdot \sigma}{\kappa} T$$
 (E)

CONCLUSIONS

The effects of the simplified chemical route, barium doping, and sintering conditions on the thermoelectric properties of the calcium cobaltite system were investigated by means of relative density, grain size, electrical and thermal conductivity, Seebeck coefficient, power factor, and ZT. The Ba-doped CCO ceramics showed higher densities and higher electrical conductivity when sintered at 1193 K for 12 h. Undoped and doped ceramics presented almost the same range of activation energy values, which can indicate that Ba-doping does not alter the electronic structure of the ceramics, once it may be segregated in the grain boundary. As the densification and grain size had a more significant impact on electrical conductivity, ceramics with higher density and grain size showed a higher power factor, e.g., 0.10 mW.m⁻¹.K⁻² at 873 K for P-1193/12 (undoped sample sintered at 1193 K for 12 h). Since the preparation methods can drastically influence the final bulk properties of CCO ceramics, the simplified method developed in this work was suitable to produce undoped CCO ceramics with ZT up to 0.07 at 873 K, unlike substitutional Ba-doped ones, mainly due to non-effective substitution reflected on lower Seebeck coefficient values.

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REFERENCES

[1] S. Jantrasee, P. Moontragoon, S. Pinitsoontorn, J. Semicond. **37**, 9 (2016) 92002.

[2] M.A. Mohammed, S. Izman, A.M. Noor, S. Rajoo, M.B. Uday, N.H. Obayers, M.F. Omar, Int. J. Eng. Technol. 7, 2.29 (2018) 31.

[3] I. Terasaki, Y. Sasago, K. Uchinokura, Phys. Rev. B 56, 20 (1997) 685.

[4] S. Lemal, J. Varignon, D.I. Bilc, P. Ghosez, Phys. Rev. B **95**, 7 (2017) 75205.

[5] M. Molinari, D.A. Tompsett, S.C. Parker, F. Azough, R. Freer, J. Mater. Chem. A **2** (2014) 14109.

[6] D. Srivastava, C. Norman, F. Azough, M.C. Schäfer, E. Guilmeau, R. Freer, J. Alloys Compd. **731** (2018) 723.

[7] M.A. Mohammed, S. Izman, A.M. Noor, S. Rajoo, M.B. Uday, N.H. Obayers, M.F. Omar, Int. J. Eng. Technol. 7, 2.29 (2018) 27.

[8] G. Constantinescu, S. Rasekh, M.A. Torres, P. Bosque, J.C. Diez, M.A. Madre, A. Sotelo, Ceram. Int. 41, 9 (2015) 10897.

[9] S.-M. Choi, C.-H. Lim, W.-S. Seo, J. Korean Phys. Soc. 57, 4 (2010) 1054.

[10] G. Constantinescu, S. Rasekh, M.A. Torres, M.A. Madre, A. Sotelo, J.C. Diez, J. Mater. Sci. Mater. Electron. **26**, 6 (2015) 3466.

[11] P. Carvillo, Y. Chen, C. Boyle, P.N. Barnes, X. Song, Inorg. Chem. **54**, 18 (2015) 9027.

[12] C. Boyle, L. Liang, Y. Chen, J. Prucz, E. Cakmak, T.R. Watkins, E. Lara-Curzio, X. Song, Ceram. Int. 43, 14 (2017) 11523.

[13] Q.M. Lu, J.X. Zhang, Q.Y. Zhang, Y.Q. Liu, D.M. Liu, 25th Int. Conf. Thermoelectr. **9** (2006) 66.

[14] F. Kahraman, M.A. Madre, S. Rasekh, C. Salvador, P. Bosque, M.A. Torres, J.C. Diez, A. Sotelo, J. Eur. Ceram. Soc. **35**, 14 (2015) 3835.

[15] Y. Zheng, H. Zhou, T. Ma, G. Zuo, H. Li, T. Su, C. Wu,H. Huang, D. Wang, L. Yin, Bull. Mater. Sci. 37, 5 (2014)963.

[16] J. Xu, C. Wei, K. Jia, J. Alloys Compd. **500**, 2 (2010) 227.

[17] A. Sotelo, S. Rasekh, M.A. Torres, P. Bosque, M.A. Madre, J.C. Diez, J. Solid State Chem. **221** (2015) 247.

[18] A.M. dos Santos, D. Thomazini, M.V. Gelfuso, Ceram. Int. **46**, 9 (2020) 14064.

[19] S. Katsuyama, Y. Takiguchi, M. Ito, Mater. Trans. **48**, 8 (2007) 2073.

[20] ASTM B962, "Standard test methods for density of compacted or sintered powder metallurgy (PM) products using Archimedes' principle", ASTM Int. (2017).

[21] C. Masingboon, P. Thongbai, S. Maensiri, T. Yamwong,S. Seraphin, Mater. Chem. Phys. 109, 2-3 (2008) 262.

- [22] D. Sedmidubský, V. Jakeš, O. Jankovský, J. Leitner, Z. Sofer, J. Heitmánek, J. Solid State Chem. **194** (2012) 199.
- [23] R.D. Shannon, Acta. Crystallogr. A32 (1976) 751.
- [24] N. Kanas, S.P. Singh, M. Rotan, M. Saleemi, M.
- Bittner, A. Feldhoff, T.E. Norby, K. Wiik, T. Grande, M.-A. Einarsrud, J. Eur. Ceram. Soc. **38**, 4 (2018) 1592.
- [25] Y.C. Liou, W.C. Tsai, W.Y. Lin, U.R. Lee, J. Aust. Ceram. Soc. 44 (2008) 17.
- [26] X. Song, Y. Chen, S. Chen, E. Barbero, E.L. Thomas, P. Barnes, Solid State Commun. **152**, 16 (2012) 1509.
- [27] Z. Shi, F. Gao, J. Zhu, J. Xu, Y. Zhang, T. Gao, M. Qin, J. Mater. **5**, 4 (2019) 711.
- [28] A. Sotelo, G. Constantinescu, S. Rasekh, M.A. Torres, J.C. Diez, M.A. Madre, J. Eur. Ceram. Soc. **32**, 10 (2012) 2415.

[29] M. Gunes, M. Ozenbas, J. Alloys Compd. 626 (2015) 360.
[30] W.D. Kingery, H.K. Bowen, D.R. Uhlmann, *Introduction to ceramics*, Wiley Intersci., New York (1976) 1032.

[31] K. Miyazawa, F. Amaral, A.V. Kovalevsky, M.P.F. Graça, Ceram. Int. **42**, 8 (2016) 9482.

[32] F. Delorme, P. Diaz-Chao, E. Guilmeau, F. Giovannelli, Ceram. Int. **41**, 8 (2015) 10038.

[33] J.P. Heremans, V. Jovovic, E.S Toberer, A. Saramat, K. Kurosaki, A. Charoenphakdee, S. Yamanaka, G.J. Snyder, Science **321**, 5888 (2008) 554.

[34] R.Z. Zhang, K. Koumoto, J. Electron. Mater. **42** (2013) 1568.

[35] T. Yin, D. Liu, Y. Ou, F. Ma, S. Xie, J. Li, J. Li, J. Phys. Chem. C **114**, 21 (2010) 10061.

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