

Percolation Threshold and Depression in Properties of Polymer Nanocomposites

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Percolation threshold is an important phenomenon to be addressed when producing nanocomposites, especially because the literature suggests a depression of properties near this region. In this study, epoxy matrix nanocomposites were produced with different volume fractions of multi-walled carbon nanotubes and were characterized according to their electrical, thermal, and mechanical properties. In addition, digital image correlation (DIC) was used to measure the strain of nanocomposites and to show how it behaves in different percolation states. Electrical conductivity indicated a percolation threshold near 0.22% v/v of nanoparticles. Differential scanning calorimetry analysis showed a depression followed by an increase in glass transition temperature near the percolation threshold. Tensile strength tests presented a depression followed by an increasing near percolation threshold. DIC images showed that nanocomposites present a different behavior when near the percolation threshold, with a more distributed strain over the surface of the sample under stress and fracture toughness decreased near the percolation threshold.

Keywords: *Percolation Threshold, Carbon nanotubes, Interphase, Nanocomposites.*

1. Introduction

An important aspect of nanocomposites is the elevated surface area of the nanomaterial per volume unit when compared to microcomposites. This characteristic influences directly on interphase phenomena and, consequently, the final properties of these nanocomposites¹.

One may define the interphase as a zone of transition between the nanoparticle interface and the polymer bulk, which can lead to a change of morphological, chemical, mechanical, and physical properties of the final material, differing from the bulk or the isolated nanoparticle, which, may appear as an unexpected or unwanted characteristic in nanocomposites²⁻⁵.

Therefore, nanocomposites present a considerable volume of interphase, and variations of properties can be observed with few percentages of nanoparticles when compared to their pure polymer matrix⁶. When these regions of interphase connect throughout the whole material occurs the percolation of interphase, which may lead to a different behavior⁷. Thus, nanocomposites may present distinct properties before, after, or near the percolation threshold⁸. Hence, the percolation threshold influences directly the final properties of nanocomposites^{4,5,9}.

The knowledge of the percolation threshold is also important because it may be used as a point of optimization of properties, for example, controlling the dispersed phase

and decreasing the percolation threshold¹⁰ to achieve conductive nanocomposites with an ultra-low percolation threshold^{11,12}, or to predict the approximation of discrete parts of interphases⁷, or even to simulate and measure the percolation in experimental studies^{13,14}.

Despite the different changes in the material during the occurrence and increase of the percolation state, electrical conductivity is one of the most characteristic properties that can be observed and measured when adding conductive nanoparticles to a dielectric matrix. This happens because the incorporation of conductive nanoparticles increases the probabilities of conductive path formation¹⁵ until it reaches a critical value and the nanocomposite changes from dielectric to dissipative or conductive, which is also indicated as the percolation threshold¹⁶⁻²⁴. Moreover, the state of percolation in nanocomposites also presents changes on mechanical properties, which can be enhanced with low volume fractions of nanoparticles²⁵ or present discontinuities, caused by local perturbations on polymer chains, leading to a degradation mechanism of mechanical properties⁸.

The percolation state of nanocomposites may be verified by using different techniques, with electrical percolation the most established technique when considering the addition of conductive nanoparticles in a dielectric matrix.

As the percolation threshold may act directly on other material properties, the glass transition temperature (T_g) of materials may also change, exhibiting both an increase or

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a decrease in T_g , which is related to interactions between polymer chains with the surface of nanoparticles²⁶⁻³⁰.

Digital image correlation (DIC) is an ongoing technique for materials characterization, which uses optical and numerical data to determine the displacement on the surface of samples under mechanical loading and compare this changing of position, providing a more accurate technique for measuring strain³¹⁻³³. Although there is still a lack of comprehensive studies in the area showing that DIC can also be used to locate surface deformations of nanocomposites and their relation with a percolated network on their structure. Thus, this study aims to evaluate the electrical, thermal, and mechanical properties of nanocomposites in stages below, above, and near the percolation threshold, as well as it is employed the use of digital image correlation technique as a tool to visualize how strain is distributed over the nanocomposites in these three main stages.

2. Experimental

2.1. Materials

The polymeric matrix was a low viscosity epoxy resin SQ2004F monomer (500 cPs, 20°C) and a SQ3154 hardener (<200 cPs, 20°C) produced by Silaex Química Ltd, with density of 1.09 g.cm⁻³. The nanoparticles were multi-walled carbon nanotubes (MWCNTs) TNM4, produced by Chengdu Organic Chemicals Co. Ltd, with outer diameter between 10 nm and 30 nm, length between 10 µm and 30 µm, surface area of 140 m².g⁻¹ and density of 2.1 g. cm⁻³.

2.2. Methods

Nanocomposites were produced using different quantities of nanoparticles as presented in Table 1. The monomer/hardener ratio was the same of 100:50 for all samples, as indicated by the supplier, and the amounts of CNTs were chosen based on previous work³⁴⁻³⁷ and the maximum capacity of CNTs addition in epoxy matrix.

The nanocomposites processing followed the steps presented in Figure 1. Initially, nanoparticle amounts were added to the monomer and mixed for 20 minutes in a magnetic stirrer to a previous homogenization and kept under stirring to the application of a high energy sonication process using a Sonics VCX750, in a constant amount of 400 J/g. After sonication, the solution was kept under stirring until reached room temperature. Then, the hardener was added to the mixture and kept under stirring for more 20 minutes. The mixtures were poured into molds according to the dimensions of test specimens of ASTM D638 (Type IV) and

Table 1. Description of groups.

Group	Φ vol. (%)
000	0.00
015	0.15
022	0.22
050	0.50
150	1.50
220	2.20

Note: Φ vol. = volume fraction.

ASTM D5045 standards and the curing process was done at room temperature for 7 days, as indicated by the epoxy resin supplier. The production of samples without nanoparticles was conducted directly in the step of hardener addition and stirring for 20 minutes.

2.3. Characterization

2.3.1. Electrical characterization

Electrical conductivity was measured according to electrical impedance spectroscopy³⁵⁻³⁷ in an Agilent – Precision Impedance Analyzer 4294, measuring 500 points between 40 Hz and 40 MHz, in 5mV AC, at room temperature.

2.3.2. Thermal characterization

Differential scanning calorimetry (DSC) was applied to verify the glass transition of samples, using a NETZSCH STA 449 F3 Jupiter®, in a N₂ atmosphere with a first heating cycle (for stress-relief purposes) of 10°C/min and a second heating cycle of 10°C/min, from 30°C to 250°C. Glass transition temperature was determined in second heating, at the inflection point, using the equipment proper software, NETZSCH Proteus.

2.3.3. Mechanical characterization

Tensile strength tests were conducted in five samples according to ASTM D638 properties of five samples were determined according to ASTM D638 standard, conducted in an AME 5kN – Filizola machine, with a load cell of 5kN, test speed of 5 mm/min, and data acquisition rate of 300 points per minute (5Hz). In these tests, yield strength values of samples were measured considering the first point at which an increase in strain occurs without an increase in stress, and ultimate tensile strength was considered as the value of stress at break.

Fracture toughness (K_{Ic}) tests were conducted according to ASTM D5045, in five samples with a compact tension (CT) shape, speed test of 10 mm/min, and data acquisition of 5 Hz in an opening mode I.

2.3.4. Digital image correlation

Specimens were prepared in two steps: first, samples were painted with a thin layer of matte white spray paint

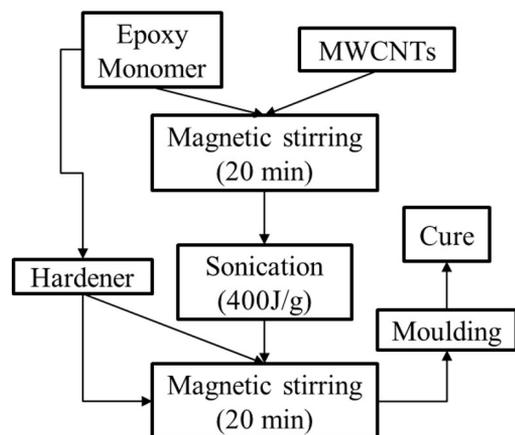


Figure 1. Flow diagram of the experimental procedure.

(Figure 2a), and then matte black spray paint was pulverized over white paint (Figure 2b) to allow contrast calibration of the equipment. The digital image correlation (DIC) technique was applied using a Dantec Dynamics Q-400, with two 4MPix cameras adjusted as shown in Figure 3, and with a frame acquisition rate of 5Hz to allow the pairing between DIC and mechanical stress data.

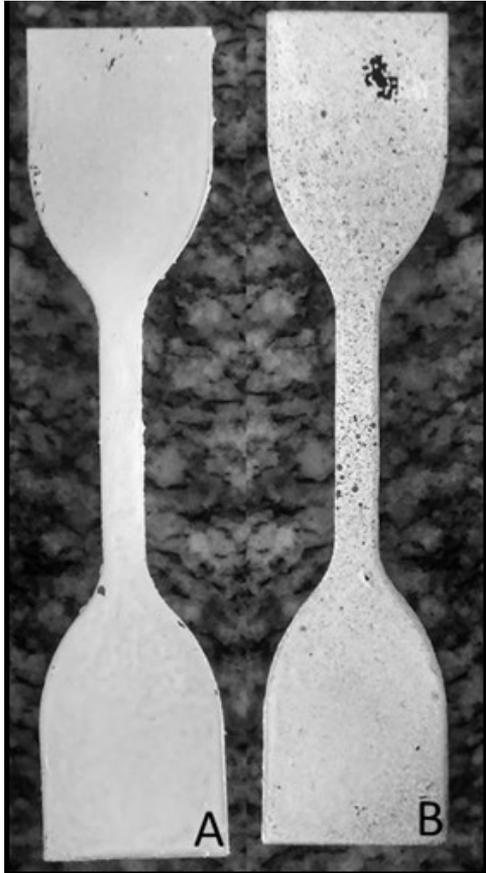


Figure 2. Sample preparation in A, painted with a thin layer of matte white spray paint and in B, after the pulverization with matte black spray paint.

3. Results and Discussion

3.1. Impedance spectroscopy

Results of electrical conductivity are shown in Figure 4 and Figure 5. Figure 4 shows electrical conductivity as a function of frequency, for each group of nanocomposites. In all samples, it is verified an increase in conductivity as the frequency increases. Similar behavior was reported in the literature and it is attributed to dipole and interface polarization processes. In this behavior, charges move from one place to another inside the dielectric material in frequencies up to 10^3 Hz (interfacial polarization), and charges locally bonded to atoms and molecules move in frequencies up to 10^7 Hz (dipolar polarization)³⁸.

As Figure 4 also shows an overlap of initial curves, Figure 5 presents data of electrical conductivity as a function of nanoparticles fraction, in which is possible to verify that there is a jump in conductivity after 0.15% v/v up to 0.50% v/v, where electrical conductivity stabilizes in a linear increasing, indicating an already percolated state. Thus, it was established the sample in 0.22% as the closest one near the percolation threshold, indicated by the gray area in Figure 5. It should be noted that even the electrical conductivity presented a depression in the gray region followed by an increase. Very probably a trap for charges at interphases overlap is created near the percolation threshold as already pointed out in the literature⁵.

3.2. Glass transition temperature

Results of the DSC analysis are presented in Figure 6 and Figure 7, which showed a change of behavior in glass transition temperature for sample in percolation threshold. While Figure 6 presents DSC traces of second heating, Figure 7 summarizes the results of the inflection point, as indicated by equipment software. The epoxy matrix, as detailed in Figure 7, presents a T_g of 71° . There is a decrease in T_g for 0.15% v/v, where T_g is 68°C followed by an increase in T_g for 76°C for sample 0.22% v/v in percolation threshold, followed by a decrease in T_g for all samples above the percolation threshold.

It was noted that a percolated interphase network has a significant effect on T_g , by acting on the properties.

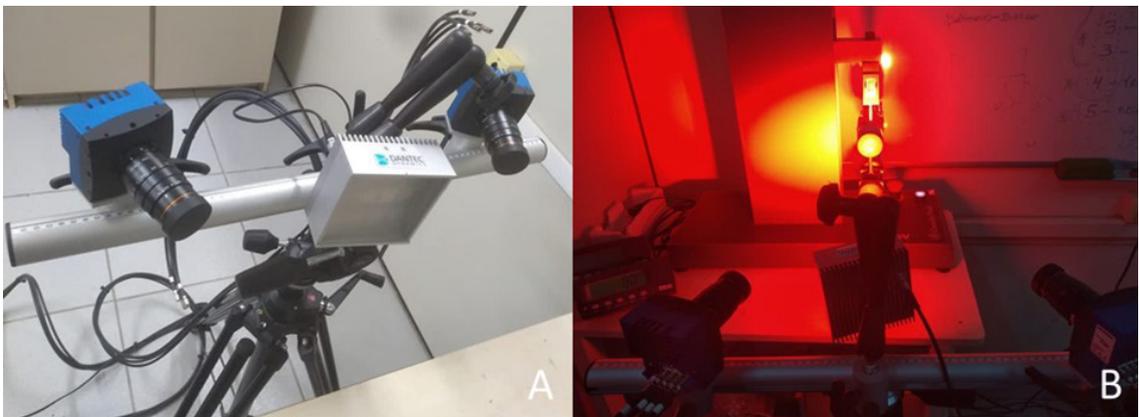


Figure 3. Apparatus of DIC.

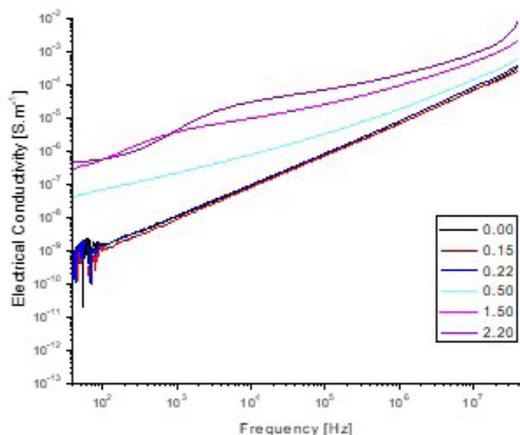


Figure 4. Electrical conductivity of nanocomposites according to frequency.

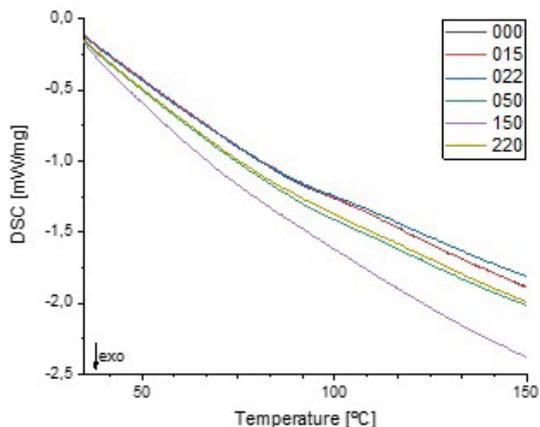


Figure 6. DSC traces of samples.

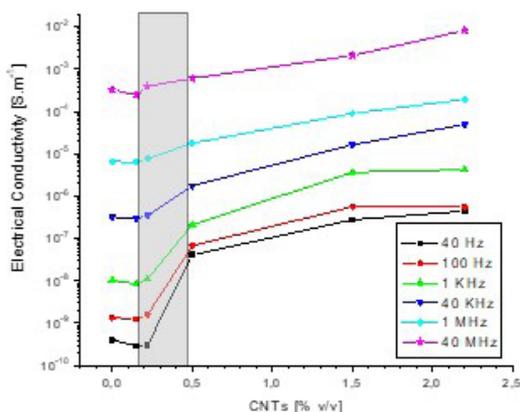


Figure 5. Electrical conductivity of nanocomposites according to nanotubes fractions in different frequencies. The percolation threshold is indicated by the gray area.

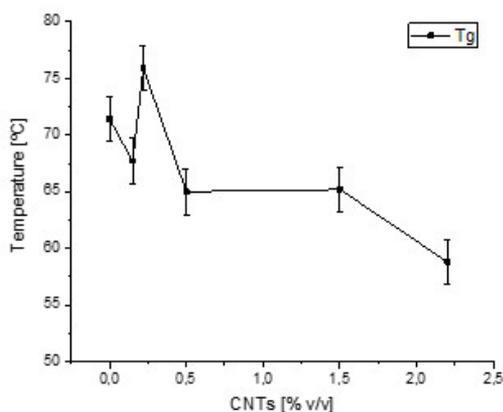


Figure 7. Glass transition temperature of samples.

As nanoparticles may produce agglomeration clusters, it was reported that these clusters lead to a decrease of interphase, not only because the interphase in agglomerated clusters overlaps, but also because a disappearance of the interphase network in the matrix may happen and it may produce effects on properties according to its stage of percolation. Below the percolation threshold, the effect of these clusters did not produce a pronounced change in Tg. Near the percolation threshold, as the paths are being formed, Tg changes significantly while after percolation, as the paths are saturated, Tg improvements decay above the percolation threshold.

An important fact of interphase on increasing Tg is the attractive interaction between nanofillers and polymer chains, which restricts the local mobility of these chains and significantly increases Tg^{2,5,9,27}.

At interphase polymer chains can have steric confinement, reducing their mobility and dipoles mobility⁵, modifying crystallinity and chain network^{12,39,40}. Concerning the effects of interphase on the Tg, it is important to highlight that there are opposing mechanisms acting, which make the

influence on the glass transition temperature not so clear. While the inclusion of rigid nanoparticles may restrain the movements of polymer chains, (increasing Tg), it may also locally disrupt cross-link, which ends up in a slight decrease in the Tg. The last one is particularly important in case there no effective functionalization techniques are employed⁴¹.

Another important aspect to be considered is that interphases have at least two layers, also called double layer interphase model, which present one tightly bonded layer to the nanoparticle and the other is weaker connected. The double layer interphase model also presents a reliable model to explain a gradient of properties toward the matrix material⁴². Hence, it is suggested that when the inner layer is bonded to the nanoparticle, it leads to a formation of a glassy chain, formed by a dynamically frozen polymer layer^{43,44}.

3.3. Mechanical properties and digital image correlation

The typical behavior of each group of nanocomposites under the tensile strength test is presented in Figure 8, represented by average curves of samples and their numerical

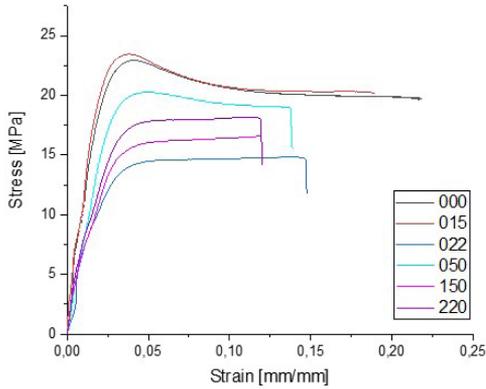


Figure 8. Representative curves of tensile strength tests.

results are presented in Table 2, as well as analysis of variance (ANOVA) and Tukey's test at 5% of representative level.

It is important to highlight that the obtained data for the epoxy matrix is in accordance with the supplier and also the available literature⁴⁵. In comparison to electrical conductivity, it is possible to verify an increase in mechanical properties with the addition of 0.15% v/v of MWCNTs. However, there is a decrease in mechanical properties above this value, reaching the minimum value for the sample with 0.22% v/v in the percolation threshold.

Images taken using DIC cameras were normalized in a range between 0% and 5% of strain, represented by colors from deep blue to red, and greyish red for points above this range. Figure 9 shows the frames taken when samples reached yield strength.

It is possible to visualize in Figure 9 that samples present distinct behaviors according to the percentage of MWCNTs. The epoxy matrix showed typical behavior of tensile test, with the strain concentrated in a narrow region section, as represented by the grayish points. As impedance spectroscopy showed an increase in electrical conductivity after 0.22%, v/v and there is the percolation threshold near this point, the nanocomposite with 0.22% v/v MWCNTs presents a highlighted behavior, in which the main portion of the specimen has grayish areas, showing that the strain is much more distributed along the sample. Although, it should be stressed that the tensile tests indicated that adhesion between matrix and nanoparticles at 0.22% v/v is very weak since the numerical value is the smallest of the studied samples. The ultimate tensile strength data indicated the adhesion is recovered at 0.50% v/v and after this composition is decreasing again.

On the other hand, samples above the percolation threshold recover their behavior of concentrating strain in specific regions and not over the whole surface. In order to evidence this strain distribution, Figure 10 shows images for samples without, near, and after the percolation threshold. As Figure 10 demonstrates this behavior, Figure 11 shows the connection between the images and the tested results of yield strength in tensile tests.

As seen in previous works of our research group^{35,46-48}, failure mechanisms such as crack bridging – pull-out, crack

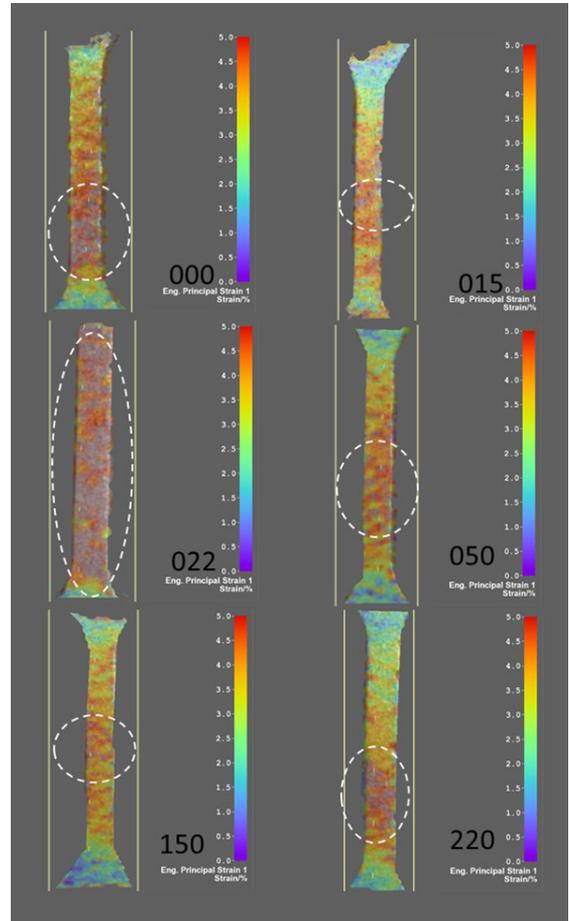


Figure 9. Digital images for tensile tested nanocomposites.

Table 2. Analysis of variance and Tukey's test at 5% of significance level of tensile strength tests.

Group	Yield Strength [MPa]	Ultimate Tensile Strength [MPa]
000	22.94 (1.86) a	22.94 (1.86) a
015	23.47 (2.88) a	23.47 (2.88) a
022	14.38 (1.41) c	16.78 (1.02) c
050	20.43 (1.09) ab	20.92 (1.22) ab
150	15.78 (2.40) c	17.45 (2.41) bc
220	17.76 (1.88) bc	18.97 (1.82) bc

Note: Standard deviation values are in parenthesis. Means followed by the same letter do not significantly differ, by Tukey's test at 5% of significance level.

deflection, and crack pinning tend to occur in the interphase. This is especially true when strong nanoparticle-matrix interactions promote the formation of brittle interphase, through which the crack propagates. In these cases, the percolation threshold may lead to less energy dissipation during crack growth, since these interphases may act as a region of weakness for mechanical properties⁴⁹. As the percolation threshold in nanocomposites indicates the minimum concentration of a nanomaterial necessary to form a kind of continuous path network⁵⁰, this amount may not

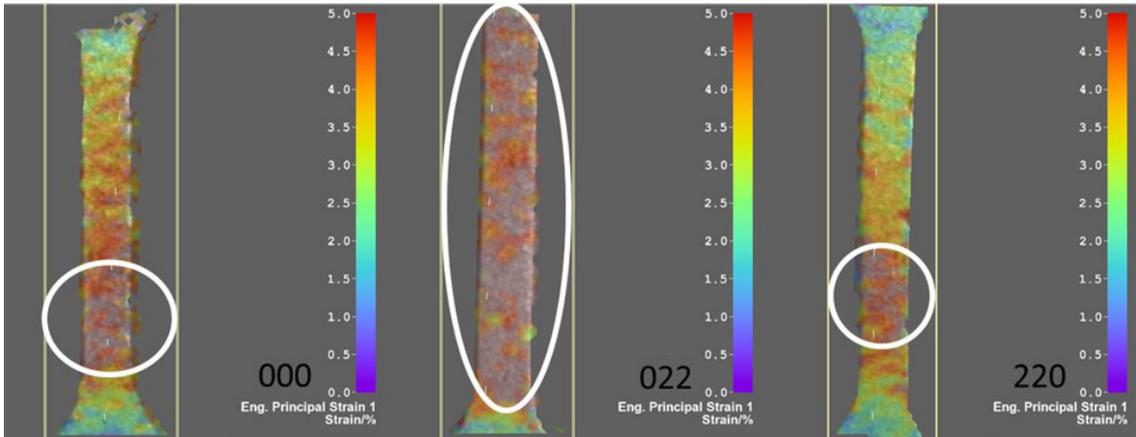


Figure 10. Strain distribution over sample surface in the polymer matrix (000), near percolation threshold (022), and after percolation (220).

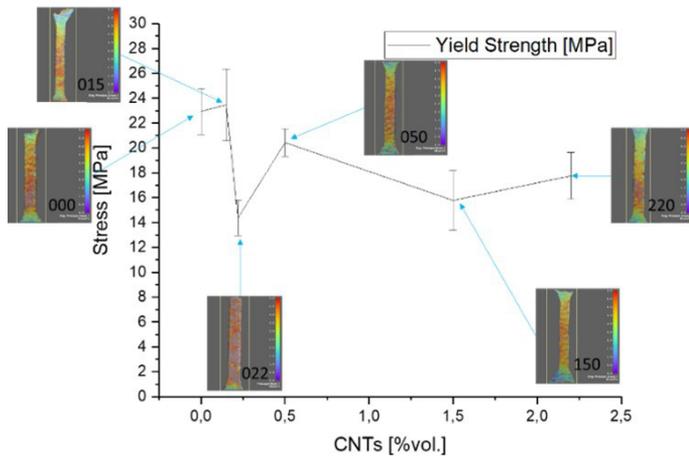


Figure 11. Digital images of nanocomposite samples and their values of yield strength in a tensile strength test.

be enough to guarantee that reinforcement occurs. Instead, stress and strain have this weak region be distributed, as yield strength presents a drop in value, due to a reduction of constraints on the polymer network⁵¹.

The obtained results of mechanical strength, its relation with electrical percolation, and the behavior observed from DIC images are in agreement between them and in accordance with simulation methods⁵¹, which also predict a yield drop and plastic weakening polymer nanocomposites near percolation, followed by a recovery of behavior after percolation.

The fracture toughness of samples is presented in Table 3, where it is also possible to verify a similar behavior of discontinuity of properties near the percolation threshold.

An important aspect observed is the relatively high fracture toughness of polymer matrix, when compared to other studies using epoxy resins^{47,52-54}. However, it is consistent with behavior presented in tensile strength tests, demonstrating that the chosen commercial resin has a considerable strain.

The increase in K_{ic} values is an expected behavior for percolated nanocomposites^{55,56}, although a decrease in K_{ic} was observed for the sample at the percolation threshold,

Table 3. Analysis of variance and Tukey's test at 5% of significance level of fracture toughness tests.

Group	K_{ic} [MPa.m ^{1/2}]
000	2.59 (0.25) ab
015	2.86 (0.12) ab
022	2.49 (0.04) b
050	2.91 (0.12) ab
150	2.98 (0.18) a
220	2.52 (0.19) ab

Note: Standard deviation values are in parenthesis. Means followed by the same letter do not significantly differ, by Tukey's test at 5% of significance level.

as indicated in Table 3 and verified by tukey's test at 5% of significance level.

In terms of digital image correlation, Figure 12 shows the strain distribution over the surface of samples on fracture toughness tests taken in the last frame before crack propagating. It is detailed that the sample with 0.22%v/v, at the percolation threshold, presents a strain more distributed

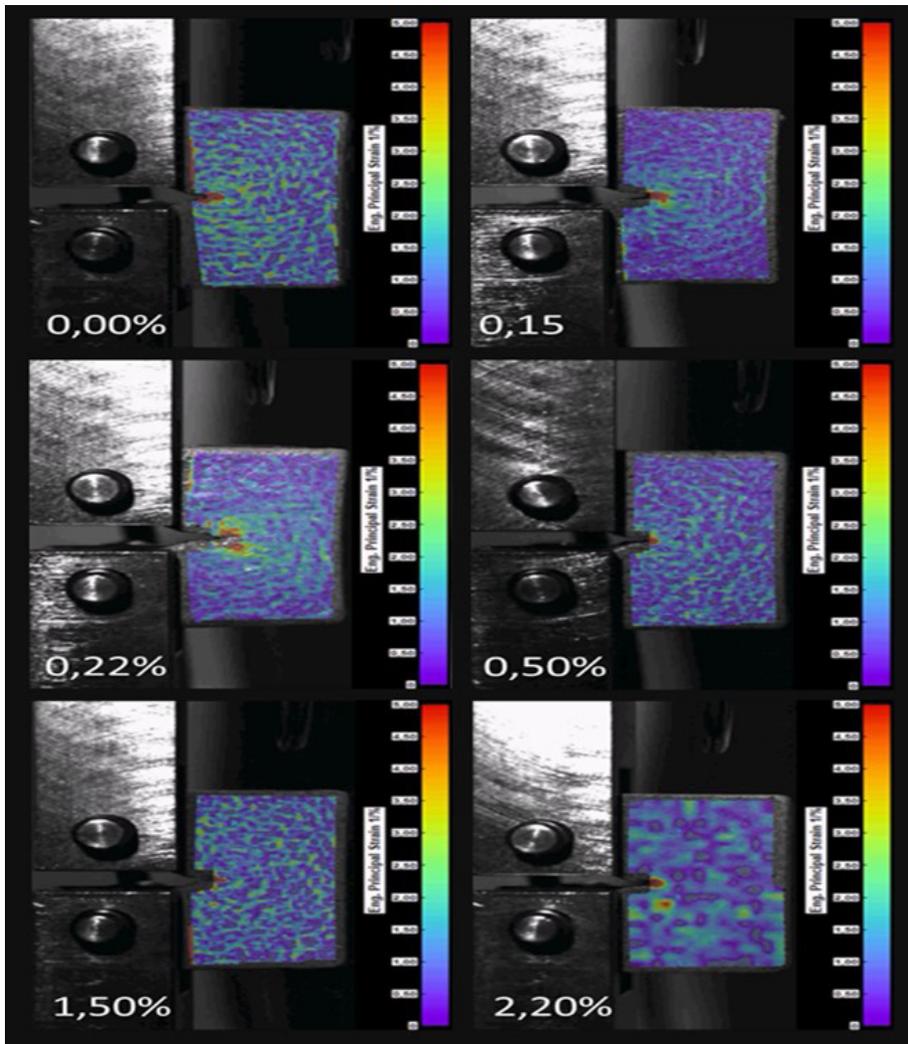


Figure 12. Digital images of fracture toughness tests.

over the surface, which is evidenced not only by the larger red area near the crack opening, but also by the yellow and green areas around the crack tip.

Another important aspect that corroborates this behavior, is that it is reported that carbon nanotubes may also present a weak interfacial bonding, which brings to lower fracture toughness of the specimens, acting as imperfection and reducing mechanical properties^{56,57}.

4. Conclusions

Epoxy matrix nanocomposites were produced with different percentages of MWCNTs and were characterized according to their electrical, thermal, and mechanical properties.

Impedance spectroscopy showed a decrease in the electrical conduction at very low fractions of MWCNTs, an increase in samples after 0.22% v/v of MWCNTs, with a relevant increase on samples with 0.50% v/v of MWCNTs, indicating the range after 0.15% v/v and 0.50% v/v as the lower and upper limits of percolation, and sample with 0.22% v/v as the sample in this threshold.

An interesting behavior of glass transition temperature right on the percolation threshold was detected, with an increase of this temperature for the sample with 0.22% v/v of MWCNTs, followed by a decrease of T_g on samples already percolated. This behavior is attributed to a critical amount of interphase which has bounded polymer chains, forming a glassy layer, with strong interaction between the polymer layer and nanoparticles.

Mechanical characterization also showed a change in mechanical properties near the percolation threshold. The behavior of strain under tensile tests was evidenced by the digital image correlation technique, which also revealed that samples near percolation present a different mechanical behavior than samples before or after this threshold.

Considering the existence of the glassy, strong bounded polymer layer around nanoparticles, the percolation path may also form a glassy and thin layer, which acts like a polymer shell, with fragile behavior. As the inner layer around nanoparticles also acts as a stress distributor, this may explain how strain is distributed over the surface of the sample near the percolation threshold.

Regarding this glassy shell around nanoparticles, it would both explain the decreasing of mechanical properties, with the lower tensile strength at percolation and the behavior observed on fracture toughness tests, which also presented a decrease of K_{IC} . Moreover, although the interphase of nanoparticles and polymer matrix may present a strong interaction, the interfacial bonding between this interphase and the whole matrix is weak bonded, leading to the behavior observed in this study.

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