

Effect of Relative Humidities on Microstructural, Barrier and Mechanical Properties of Yam Starch-Monoglyceride Films

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ABSTRACT

The effect of monoglyceride on microstructural, barrier and mechanical properties of casted yam starch films were investigated in different relative humidities (RH) and compared with glycerol-starch films. A single screw extruder was used to produce the starch – monoglyceride complex before film production and this process was effective to inhibit the phase separation in films. The addition of the hydrophobic compound reduced hydrophobicity, transparency and water vapor permeability of films. This later value for starch-glycerol film ($1.7 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) was higher than starch ($1.2 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) and monoglyceride-starch films ($1.0 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$). Films containing glycerol had higher relative crystallinity (B and V_H) with a slight increase at higher RH values, while for monoglyceride films, the crystallinity was constant. Monoglyceride-starch films presented poor mechanical properties when compared to glycerol- starch ones but they presented a stable behavior under different relative humidities.

Key words: biodegradable films, hydrophilicity and glycerol-monoestearate

INTRODUCTION

Biopolymer films and coatings from polysaccharides, proteins and lipids formulated either with one or more components have potential to control mass transfer and, thus, extend food shelf life, as compared to traditional packaging (Parris et al., 1995; García et al., 1999, 2000). Being totally degradable, biopolymers could contribute to reducing the amount of plastic wastes. In addition, these polymers are obtained

from renewable sources, unlike the synthetic polymers (Souza and Andrade, 2000).

The first studies about the use of starch in biodegradable food packaging were based on substituting part of the synthetic matrix by starch (below 10%). However, the main difficulties found were attributed to chemical incompatibility of starch with synthetic polymers (Griffin, 1977). Recently, many works dealt with the addition of plasticizers to pure starch-based materials to overcome the film brittleness caused by high

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intermolecular forces (Bader and Göritz, 1994; Lourdin et al., 1995; Souza and Andrade, 2000; García et al., 2000; Larotonda et al., 2004; Mali et al., 2002; 2004).

The usefulness of starch films is somewhat limited because their mechanical and barrier properties are dependent on moisture (Krochta and Mulder-Johnston, 1997). They become brittle in a dry atmosphere and lose strength and barrier properties in high humidity. The moisture sensitivity in particular must be reduced if starch is to become an alternative to conventional plastics in industrial applications (Petersson and Stading, 2005).

Although some good solutions have been found until now as blends of starch with natural or synthetic biodegradable polyesters (polylactic acid, polycaprolactone, etc.), multilayer films or addition of nanocomposites, these cannot be used still for wide applications because of their relatively high price (Wilhelm et al., 2003; Campos and Franchetti, 2005; Ray and Bousmina, 2005).

At same time, much work has been done to examine the water vapor barrier properties of films made from other biopolymers, like wheat gluten, zein and methylcellulose with added lipids or waxes (Gontard et al., 1994; Weller et al., 1998) and although a great deal of research has been done on edible films made of renewable and biodegradable substances with respect to their barrier and mechanical properties, there has been little research on starch-lipid films.

Garcia et al. (2000) analyzed the barrier properties of starch-based films and coatings from corn and high amylose corn with addition of sunflower oil as hydrophobic component and with a plasticizer present. Petersson and Stading (2005) studied the mechanical and barrier properties of starch-monoacylglyceride films and observed a decrease in water vapor permeability. Nevertheless, they reported that phase separation occurred in films with high amount of monoacylglyceride (about 10 g/100 g starch).

According to Eliasson and Kim (1995), amylose presented the ability to form complexes with monoacylglycerides, which depended on their physical state and thus, the utilization of extrusion cooking in the mixture of starch and monoacylglycerides could be an alternative to overcome the phase separation. Yam starch, due to its high concentration of amylose (higher than 30%) has been related as raw material with potential good results in the

production of biodegradable films, such as stability during storage and others (Mali et al., 2002; 2004; Wilhelm et al., 2003).

The objectives of this work were to produce the casted films with yam starch, complexed with monoacylglyceride (glycerol-monoestearate) and to evaluate its microstructural, barrier and mechanical properties in different relative humidities.

MATERIALS AND METHODS

Materials

Fresh tubers of yam (*Dioscorea alata*), with uniform size and shape, without any mechanical and pathological injuries, were obtained from a local farm (Londrina - PR, Brazil). Yam starch was extracted according to Alves et al. (1999), which presented the following composition on dry basis: ash = $0.21 \pm 0.01\%$, protein = $0.50 \pm 0.01\%$ and lipids = $0.07 \pm 0.02\%$ and amylose = 33.7%.

The monoacylglyceride employed was the glycerol-monoestearate that was supplied by Ceralit S/A (Campinas - Brazil), and had a melting point of 55-62°C.

Complex starch – monoacylglyceride preparation

Yam starch and the monoacylglyceride were mixed for 15 min in an electric mixer using a monoacylglyceride concentration of 2g/100 g starch, with a moisture content adjusted at 18% with distilled water. A single screw extruder (Cerealtec CT-L15, Campinas, Brazil) was used to produce the complex starch – monoacylglyceride. The extruder was coupled with a barrel of 420 mm in length and 19.4 mm in diameter, 1:2 compression ratio screw and 5 mm die diameter. The extrusion temperature was maintained at 70-80°C for the feeding section, and 145°C for the mixing and metering sections. Screw speed was fixed in 120 rpm. The extruded samples were collected and dried at 55°C in a forced-air convection oven (Tecnal TE 394-3 - Brazil) during 12 h and were finely ground in a Quimis Mill (Q-298 A21- Brazil).

Differential scanning calorimetry

Native and complexed yam starches were tested in a Shimadzu DSC, model 50 (Shimadzu Corporation, Japan) to confirm the formation of the complex starch-monoacylglyceride. Samples of 1 mg, mixed with 3 µL of distilled water, were stored for 12 h in aluminum pans hermetically

sealed; an empty pan was used as reference. Samples were heated from 20 to 160°C with 10°C/min heating rate. All measurements were performed in duplicate.

Films preparation

The films were prepared by mixing the starch-mono-glyceride complex (4 g/100 g solution) with distilled water to make batches with a total weight of 500 g. The film-forming solutions were transferred quantitatively to the viscograph cup of a Brabender Viscograph Pt 100 (OHG, Duisburg, Germany). They were heated from 30 to 95 °C and maintained at 95 °C for 10 min, with regular shaking (75 rpm) and constant (3°C/min) heating rate (this treatment did not disrupt the starch-mono-glyceride complex as proved by DSC tests – data not shown). The films were prepared by casting and gelatinized suspensions were immediately poured on rectangular acrylic plates (10 x 20 cm). The quantity of starch suspension poured onto the acrylic plates was calculated to obtain the films with 0.11 ± 0.01 mm of thickness, measured with a Mitutoyo micrometer (São Paulo - Brazil). The starch suspensions were dried at 45 °C in a ventilated oven model TE-394-3 (Tecnal, Piracicaba, SP, Brazil) to constant weight (about 20 h). Starch films without mono-glyceride (4 g starch/100 g filmogenic solution) and glycerol-starch films (4 g yam starch and 1.3 g glycerol/100 g filmogenic solution) were produced at the same conditions; which were included in the study for comparative purpose. Glycerol and starch concentrations were established in a previous study (Mali et al., 2002).

All the films were stored for seven days before the analysis. They were placed at $25 \pm 2^\circ\text{C}$ in separated desiccators over saturated salt solutions (LiCl, MgCl₂, Mg(NO₃)₂, NaCl, (NH₄)₂SO₄) that respectively establish the desired relative humidity (11, 33, 54, 75 and 81 % RH) conditions.

Films characterization

Adsorption isotherms

Film specimens (30 mm x 30 mm) were pre-dried for 7-days over phosphorous pentoxide (P₂O₇) and then were placed in desiccator at $25 \pm 2^\circ\text{C}$, over saturated salt solutions having different relative humidity (11, 33, 54, 75 and 81 % RH) conditions. Each film specimen was weighed at regular intervals, and when two consecutive weighings were equal, it was assumed that an equilibrium

condition was reached. Under the above conditions, an equilibrium period of 3-days was sufficient to establish the moisture equilibrium. Equilibrium moisture content was calculated from the increase in mass of the dried sample after equilibration at a given RH.

GAB (Guggenheim – Anderson – de Boer) model was used to fit yam starch film sorption isotherm data and monolayer values were calculated from the equations (Bizot, 1984). GAB isotherm model can be expressed as follows: $M = m_0 C K a_w / (1 - K a_w) (1 - K a_w + C K a_w)$, where M is the equilibrium moisture content at a water activity (a_w), m_0 is the monolayer value (g water/ 100 g solids) and C and K are the GAB constants.

Water vapor permeability (WVP)

WVP tests were conducted using ASTM (1995) method E96. Each film sample was sealed over a circular opening of 0.00181 m² in a permeation cell that was stored at 25°C in a desiccator. To maintain a 100 % RH gradient across the film, anhydrous calcium chloride (0% RH) was placed inside the cell and distilled water (100% RH) was used in the desiccator. The RH inside the cell was always lower than the outside, and water vapor transport was determined from the weight gain of the permeation cell. After steady state conditions were reached (about 2 h), eight weight measurements were made over 24 h. Changes in the weight of the cell were recorded to the nearest 0.0001 g and plotted as a function of time. The slope of each line was calculated by linear regression ($r^2 > 0.99$) and the water vapor transmission rate (WVTR) was calculated from the slope of the straight line (g/s) divided by the cell area (m²). After the permeation tests, film thickness was measured and WVP (g Pa⁻¹ s⁻¹ m⁻¹) was calculated as $WVP = [WVTR = S (R_1 - R_2)] d$; where S is the saturation vapor pressure of water (Pa) at the test temperature (25°C), R₁, the RH in the desiccator, R₂, the RH in the permeation cell and d is the film thickness (m).

X-ray diffraction

Samples were analyzed between $2\theta = 2^\circ$ and $2\theta = 60^\circ$ with a step size $2\theta = 0.02^\circ$ in a X-ray diffractometer Philips PW 1710 (The Netherlands) using a Cu Ka radiation ($\lambda = 1.543$), and 40 kV and 30 mA. Relative crystallinity was calculated for B and V_H crystals by dividing the area of the diffraction peaks at $2\theta = 17^\circ$ and 22° (for B-type)

and $2\theta = 19.8^\circ$ (for V_H -type) by the total area of the diffractogram (Hullemann et al., 1999).

Mechanical properties

The tensile properties of starch films were determined using a TA.TX2i Stable Micro Systems texture analyzer (Surrey – England) in accordance with ASTM D-882-91 method (1996). The samples were clamped between the pneumatic grips and force (N) and deformation (mm) were recorded during extension at $50 \text{ mm}\cdot\text{min}^{-1}$ and with an initial distance between the grips of 50 mm. The parameters determined were: stress at break (MPa) and strain at break (%). Five film specimens (100 mm x 25 mm) of each formulation were used in the analysis

RESULTS AND DISCUSSION

The films obtained were translucent and easily removed from the plate.

The DSC thermogram of native yam starch (Fig. 1a) presented an endothermic peak at 63.3°C that could be attributed to the starch gelatinization. The monoglyceride-complexed starch (Fig. 1b) did not present an endothermic peak at this temperature, probably because the extrusion process was effective in gelatinization of starch granules. In addition, another endothermic peak was observed at 95.7°C and this could be attributed to the melting of the starch-monoglyceride complex (Fig. 1b). These data was according to Tufvesson and Eliasson (2000) who reported an endothermic peak between 96 and 120°C in potato starches complexed with monoglycerides and related it to the melting of this complex.

The presence of glycerol or monoglyceride affected the final appearance of the films and only a slight phase separation was observed on monoglyceride starch films, which were more opaque than starch and glycerol-starch films probably because the hydrophobicity conferred by the monoglyceride.

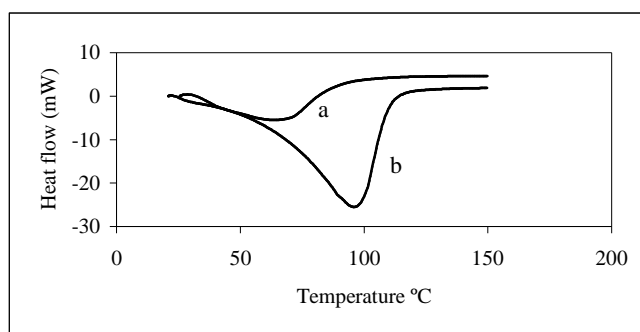


Figure 1 – DSC thermograms of (a) native yam starch (peak temperature= 63.3°C) and (b) monoglyceride-starch complex (peak temperature = 95.7°C).

According to Petersson and Stading (2005), monoglyceride concentration affected the final appearance of casted starch films, which became more opaque and shrunken at higher monoglyceride concentrations (about $10 \text{ g}/100 \text{ g}$ starch). In this study, two factors probably inhibited the phase separation in monoglyceride starch films: the extrusion process employed to form the starch-monoglyceride complex and the lower monoglyceride concentration employed in film formulations ($2 \text{ g}/100 \text{ g}$ starch).

Adsorption isotherms

The sorption isotherms of starch and glycerol-

starch films (control samples) were compared with those of monoglyceride starch films (Fig. 2). The isotherms showed a similar sigmoid shape (isotherm type II) and glycerol films showed higher equilibrium moisture content in all water activities. This could be explained by the difference between the films formulations; while glycerol was a hydrophilic plasticizer, the addition of a hydrophobic compound as a monoglyceride probably reduced the water binding capacity of the films.

To improve the investigation about water sorption behavior, the adsorption data obtained were fitted using GAB model (Bizot, 1984). As shown in

Figure 2, the GAB model adjusted well to experimental points ($r^2 = 0.99$); films with glycerol showed highest monolayer value (0.087 g water/ g solids) and monoglyceride-starch films (0.081 g water/ g solids) the lower. The monolayer value indicated the maximum amount of water that could be adsorbed in a single layer per gram of dry film

and was a measure of number of sorbing sites (Strauss et al., 1991). The addition of an hydrophilic plasticizer provides more active sites by exposing its hydroxyl groups in which the water molecules could be adsorbed (Mali et al., 2005).

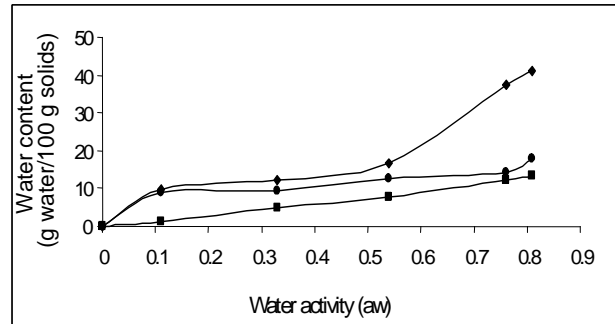


Figure 2 - Sorption isotherms at 25°C for: ● = starch films, ◆ = starch-glycerol films and ■ = starch-monoglyceride films. The lines were derived from GAB model.

Water vapor permeability (WVP)

The WVP of glycerol starch films ($1.7 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) was significantly higher (Tukey test, $p \leq 0.05$) than starch ($1.2 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) and monoglyceride starch films ($1.0 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$). These results were an indicative that monoglyceride addition to starch structure can be effective in reducing moisture transfer. According to Petersson and Stading (2005), the effectiveness of monoglycerides to improve barrier properties in starch films was affected by the phase separation. In the films with phase separation, the WVP increase instead decrease because the films structures have areas without the hydrophobic compound.

X-ray diffraction

The crystallinity pattern of films (similar to that showed in Fig. 3) could be assigned to a B-type (high intensity peaks at $2\theta = 17$ and 22.1), characteristic of biofilms containing starch (van Soest and Vliegenthart, 1997; Mali et al., 2002).

V_H crystals (high intensity peaks at $2\theta = 19.8$) were also observed. The X-ray diffractograms were used for the purpose of calculating the relative crystallinity of starch films at specific angles that corresponded at particular crystal types.

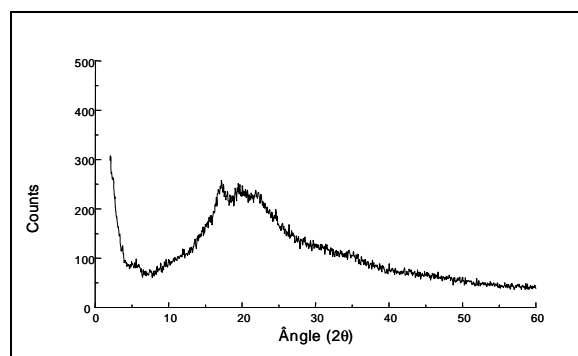


Figure 3 – X-ray diffractogram profile observed in the different films.

In Figure 4, the relative crystallinities for B and V_H crystals were plotted against the different relative humidities tested for films storage. In both cases glycerol films presented higher crystallinity degree, with a slight increase at higher RH values, while monoglyceride starch films showed constant crystallinity degree (Fig. 3). Rindlav-Westling et al. (1998) demonstrated that increasing levels of relative humidities increased the relative

crystallinity of glycerol plasticized amylopectin films. Theoretically, the V_H structure is found in extruded starches (van Soest et al., 1996) and in this work should be appeared more significantly in the monoglyceride starch films, but probably the short storage time and the low water content did not favored the starch crystallization in these films.

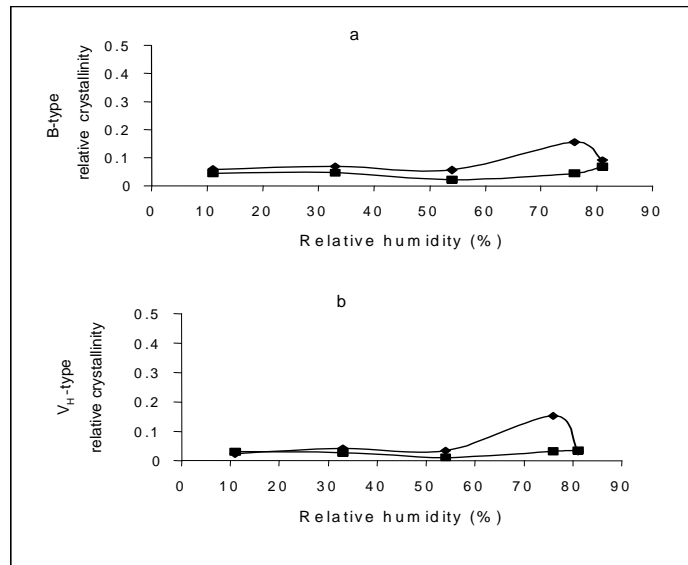


Figure 4 – Type-B (a) and Type V_H (b) relative crystallinity of \blacklozenge = starch- glycerol films and \blacksquare = starch-monoglyceride films.

Mechanical properties

Starch films and glycerol plasticized films showed large variations in stress and strain at break under different RH; a decrease in stress and an increase in strain were evidenced when RH increased (Fig. 5). The decrease of stress and the increase of strain in starch films were related with the variation of water content in these hydrophilic materials and has been reported previously (Cuq et al., 1995; Parris et al., 1995; Monterrey and Sobral, 1999; Mali et al., 2004; 2005). Structural modifications occurred in starch network when these plasticizers were incorporated. Water and glycerol molecules are small and present high capacity to interact with starch chains, enhancing the molecular mobility and increasing free volume in the film matrix, leading more weak and flexible films (Mali et al.,

2004; 2005). Although monoglyceride starch films presented poor mechanical properties when compared to starch and glycerol-starch films, they presented a desirable stable behavior under different relative humidity (Fig. 5).

The low stress at break could be related to the weakening effect of the monoglyceride on the starch network (Petersson and Stading, 2005), probably the monoglyceride groups sterically interfered with the intermolecular alignment of starch chains, decreasing its tendency to form hydrogen bonds (Wurzburg, 1986).

The lower flexibility presented by these films agreed with isotherms data, which showed that monoglyceride starch films had a lower water binding capacity, and this probably conferred lower flexibility to them.

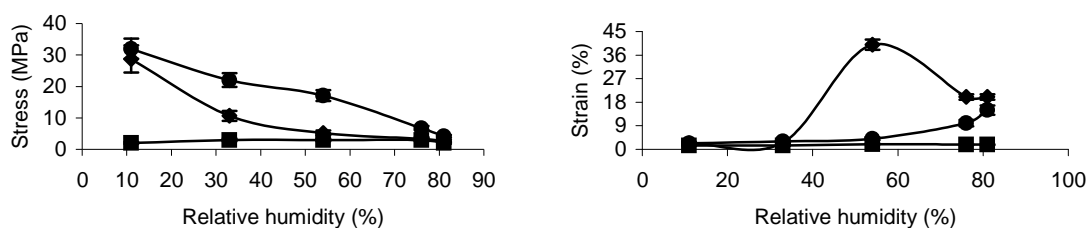


Figure 5 - Stress at break and strain at break for: ● = starch films, ◆ = starch-glycerol films and ■ = starch-monoglyceride films.

CONCLUSIONS

The use of extrusion cooking to complex yam starch and monoglyceride was effective and permitted to produce starch-monoglyceride films with only a slight phase separation. The high stability of mechanical properties of starch-monoglyceride films submitted to different RH conditions was its most desirable characteristic, and at the same time, these films showed lower hydrophilicity and water vapor permeability than starch and glycerol-starch films. The tensile tests showed that the monoglyceride had a weakening effect on the films, suggesting that it was the starch interactions that provided most of the tensile strength. Although starch-monoglyceride films presented poor mechanical properties when compared with glycerol films, they could have application as packing for fast food, for example, that do not require high resistance or elongation.

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RESUMO

Estudou-se o efeito da adição de monoglicerídeo nas propriedades microestruturais, mecânicas e de barreira de filmes de amido de inhame, em diferentes umidades relativas (UR), comparando-as com as de filmes de amido-glicerol. Uma extrusora mono-rosca foi usada para produzir o complexo amido-monoglicerídeo, antes de produzir o filme, e o processo foi efetivo para inibir a separação de fases que geralmente ocorre

nesse tipo de filmes. A adição de monoglicerídeo, que é um composto hidrofóbico, reduziu a hidrofiliçidade, a transparência e a permeabilidade ao vapor de água dos filmes. O valor desta, para os filmes de amido-glicerol ($1,7 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) foi maior que para os de amido ($1,2 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$) e para os de amido-monoglicerídeo ($1,0 \times 10^{-10} \text{ g Pa}^{-1} \text{ s}^{-1} \text{ m}^{-1}$). Os filmes com glicerol tiveram maior cristalinidade relativa (B e V_H), com um ligeiro aumento em altas UR, enquanto que nos filmes com monoglicerídeo a cristalinidade foi constante. Os filmes de amido-monoglicerídeo apresentaram piores propriedades mecânicas que os filmes de amido-glicerol, mas foram mais estáveis sob diferentes umidades relativas.

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