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# Elastic modulus evaluation of Titania nanotubes obtained by anodic oxidation

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#### **ABSTRACT**

The use of titania (TiO<sub>2</sub>) nanotubes is becoming one of the most attractive techniques as surface treatment for implants due its combination of morphology (that accelerates osteoblast adhesion and proliferation), bioactivity and possibility of being use as a drug vehicle. Anodic oxidation is one of the cheapest and simplest approaches to obtain highly ordered nanotubes. Parameters such as applied potential, reaction time and fluoride containing in the electrolyte define the nanotubes morphology. However, the mechanical properties of the nanotubes layer do not have been completely elucidated and they play a crucial role in the implant long term stability. The objective of this research was to obtain TiO<sub>2</sub> nanotubes using anodic oxidation and to determine their elastic modulus and hardness. The TiO<sub>2</sub> nanotubes layer was obtained in a fluoride containing electrolyte for 1 hour, one group at 15 V and another one at 25 V. The TiO2 nanotubes morphology was characterized by scanning electron microscopy (SEM) and atomic force microscopy (AFM). The elastic modulus and hardness were evaluated by nanoindentation experiments using a spherical tip. SEM images showed highly ordered nanotubes on all titanium surfaces and it was observed that the nanotubes diameters are directly related with the applied potential. Nanotubes diameters are  $66 \pm 9$  nm and  $131 \pm 22$  nm for nanotubes obtained at 15 V and 25 V, respectively. Nanoindentation test results showed a decrease in the elastic modulus comparing with titanium reference and these values approach to cortical bone elastic modulus. These results demonstrate that it was possible to obtain a homogeneous TiO2 nanotubes layer that has mechanical properties adequate to improve implant long-term stability.

Keywords: Titania nanotubes, anodic oxidation, indentation, elastic modulus.

# 1. INTRODUCTION

Titanium and titanium alloys are the materials most used as endosseous implants. Their characteristics as mechanical properties, low density, good corrosion resistance, make them more attractive than other used as implants, as stainless steel 316 L and Cr-Co alloy [1], [2]. Elastic modulus (E) is a property that affects directly the implant stability. It is desirable that the metal elastic modulus be as close as possible from that of the bone (around 30 GPa to the cortical bone), because lower differences between the E values result in better transfer of stress, avoiding stress-shielding effect [3]. Being a valve metal, titanium has a self-formed spontaneous oxide layer that prevents the release of ions when implanted, leading to biocompatibility. However this thin oxide layer does not promote chemical bonds with live tissue, so it's necessary a surface treatment to improve their surface properties looking for a optimized osseointegration [4].

Recently,  $TiO_2$  nanotubes are being studied as a surface treatment due to the combination of  $TiO_2$  properties and the nanotubular morphology. Researches demonstrate that the nanotubes accelerate osteoblast adhesion and growth [5], enhance apatite deposition [6], exhibit excellent bioactivity [7], improve bone bonding *in vivo* [8], demonstrate better corrosion resistance [9] and can be a drug delivery vehicle [10].  $TiO_2$  nanotube layer can be produced by many methods, including template-assisted methods, sol–gel techniques, and hydro/solvothermal methods (with or without templates) [11]. Among these different superficial treatment the simplest and cheapest approach is the anodic oxidation using hydrofluoric containing electrolyte [12].

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Elastic modulus of  $TiO_2$  nanotubes layer is not well established until now and it plays an important role on the long term stability of the implant, although few researches have investigate it. Instrumented indentation is the most suitable technique to determine the elastic modulus of thin films, however the initial roughness and the probe geometry can impose some limitations. Crawford [13] has examined the deformation behavior of a nanotube layer using nanoindentation tests with a Berkovich probe, what led to a indentation penetration higher than the thickness of the nanotube layer and wear marks on indentation.

In this study it is reported the nanotube obtainment under two different potentials, to observe their morphological properties and investigate the elastic modulus of  $TiO_2$  nanotubes layers using a spherical probe.

#### 2. MATERIALS AND METHODS

Prior to anodic oxidation, commercially pure titanium samples (~5×18×2) mm, grade 2 were grounded and polished with SiC paper and silical coloidal suspension to mirror image. They were then degreased by sonicating in acetone, isopropyl alcohol and deionized water, for 15 min in each bath . To remove the air-formed oxide layer the samples were chemically etched by immersion in a solution of nitric acid and hydrofluoric acid for 15 sec. A two-electrode electrochemical cell was used with the sample as anode and a platinum wire as counter electrode. The applied potential was computer-controlled using a Agilent DC power supply. Anodization was conducted at constant voltage of 15 V or 25 V for 1 h at room temperature. A 1 mol.L<sup>-1</sup> H<sub>3</sub>PO<sub>4</sub> electrolyte with an addition of 0.3 wt % HF was used. A magnetic stirrer was employed during the anodization to avoid formation of bubbles on the electrode surface. After the anodization the samples were rinsed in deinonized water and dried with a heat gun.

The  $TiO_2$  nanotubes morphology was analyzed by scanning electron microscopy (SEM) and atomic force microscopy (AFM) in contact mode. The average diameter was calculated after the image acquisition using ImageJ software measuring 50 nanotubes in three regions of each sample. Structure was evaluated by Raman spectroscopy, using a 532 nm laser. The elastic modulus was obtained from the Oliver and Pharr method using instrumented indentation tests. A spherical tip (100  $\mu$ m diameter) was used and the applied loads ranged from 0.10 mN to 100 mN in 8 loading/unloading cycles or 20 mN in one cycle. A Ti polished sample was used as reference to the nanoindentation test.

### 3. RESULTS AND DISCUSSIONS

# 3.1. Chronoamperometric curve of obtainment

Current profile of anodic oxidation is show in Figure 1. It's possible to observe that initially the current density decrease (region I), due to thickening of oxide that act as barrier layer, for both applied voltage. Around 150 sec there is an increase in current density (region II) caused by the nanotube formation, more pronounced for 25 V than for 15 V, that increase the reactive area subject to anodization. Finally, the curve enters in a steady-state (region III) originated by the balance between oxide growth and dissolution caused by fluoride ions. The current density behavior is in accordance with literature and it is believed that region III is greater for samples anodized at 25 V due to the higher ions migration through the TiO<sub>2</sub> oxide [12], [14].

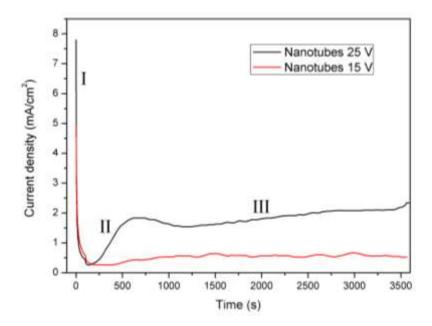


Figure 1: Current densities as function of time during anodization of TiO<sub>2</sub> nanotubes obtained at 15 V and 25 V.

## 3.2. Morphological features

Figure 2 shows an AFM image of the nanotubes anodized at 25 V. It's possible to observe that the nanotubes tops were not on the same level, probably due to the initial roughness. AFM analyses prove to be adequate to observe the topography, but it was not possible to measure diameter and roughness due to the tip convolution, consequence of tip geometry. As a consequence, this image provides just a qualitative view of the nanotopography.

Morphology analysis of  $TiO_2$  nanotubes shows that anodization processes lead to a highly ordered nanotube layer, self-organized and perpendicularly disposed over the substrate. SEM images show the top-view of  $TiO_2$  nanotubes obtained under 25 V (Figure 3) and under 15 V (Figure 4).  $TiO_2$  nanotubes diameter is affected by the applied potential. Samples anodized under 15 V and 25 V showed inner diameters of  $66 \pm 9$  nm and  $131 \pm 22$  nm respectively. Since only the applied potential was changed during the anodization tests, it is possible to conclude, in accordance with literature, that the average diameter depends on the applied potential.

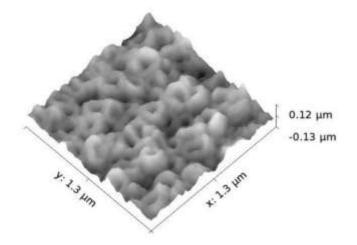


Figure 2: AFM image of TiO<sub>2</sub> nanotubes grown at 25 V obtained by contact mode.

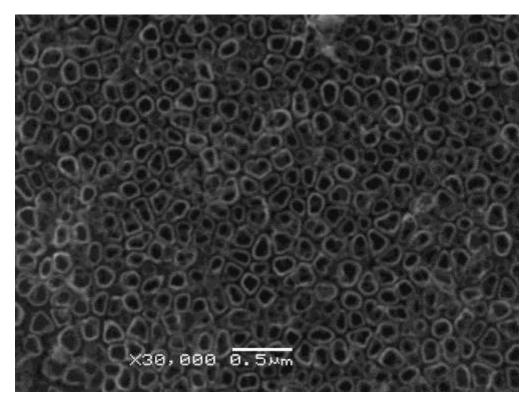


Figure 3: SEM top view images of TiO<sub>2</sub> nanotubes grown at 25 V.

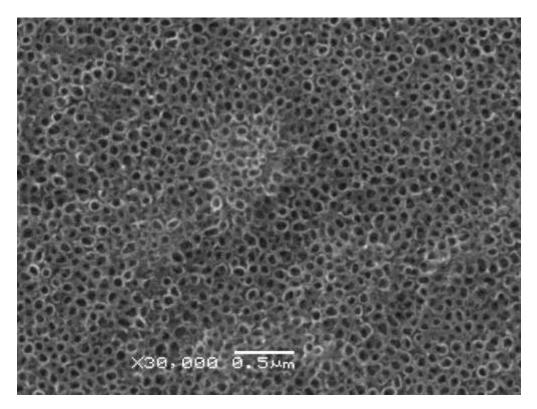


Figure 4: SEM top view images of  $TiO_2$  nanotubes grown at 15 V.

# 3.3. Crystallinity

The Raman spectra of both samples is presented in figure 5. No peaks are observed to the titanium substrate, whereas for the nanotube layer obtained at 25 V it is possible to observe characteristic peaks of anatase phase

according to RRUFF project. Nanotubes obtained at 15 V exhibit a broad band instead of well defined peaks. Previous data in literature reported the absence of Raman peaks in porous titanium layers obtained at 20 V due to the low layer thickness [15].

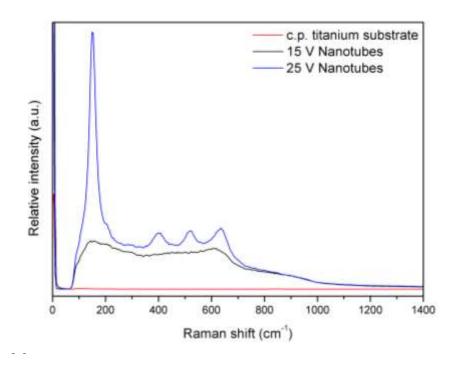


Figura 5: Raman spectra of titanium substrate and nanotube layers obtained at 15 and 25 V.

The dotted blue line on Figure 6a corresponds to the elastic modulus of untreated Ti sample. After the anodization process it was repeated the indentation tests and the results are the black and red dots, to nanotubes obtained under 15 V and 25 V, respectively. On this test it was performed 8 loading/unloading cycles of indentation, where the maximum load applied was 100 mN. As even the small irregularities influence on indentation test, resulting in large deviations, the graphs presented here are useful for comparison but are not quantitative results. Both nanotubes layers show an increase on elastic modulus as the contact depth becomes higher. This behavior is caused by the substrate influence. No difference is observed between the values measured for both nanotubes layers and the amount of anatase phase seems not to be significant to the nanotube elastic modulus.

Literature reports show that the indentation could lead to densification, caused by the collapse of nanotubes under pressure, resulting in results variation [16]. Therefore, other tests were performed using just one loading/unloading cycle and a lower load, 20mN. The results are presented in Figure 6(b), where it is possible to observe that both nanotubes elastic modulus values are lower than that of untreated Ti.

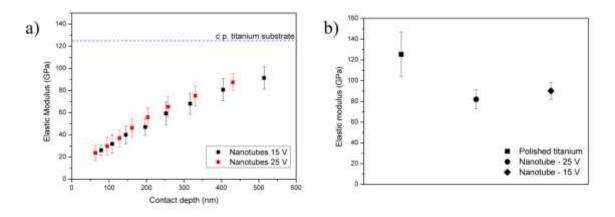


Figure 5: (a) Elastic modulus profile of TiO<sub>2</sub> nanotubes anodized at 15V (black points) and anodized at 25V (red points) in comparison with titanium reference (blue dotted lines), It's was used 8 loading/unloading cycles with maximum load of 100mN (b) Elastic modulus for one loading/unloading cycle with load of 20mN.

#### 4. CONCLUSIONS

It was possible to obtain nanotubes by anodic oxidation using a 1 mol.L<sup>-1</sup>  $H_3PO_4 + 0.3$  wt % HF electrolyte and the nanotube diameter was defined by the applied potential. The nanotubes elastic modulus does not exhibited difference between nanotubes obtained at 15 V and 25 V, but both values are lower than that of untreated Ti. These results demonstrated that it was possible to obtain an improved surface due to a homogeneous  $TiO_2$  nanotubes layer that has elastic modulus values adequate to improve osseointegration.

### 5. ACKNOWLEDGEMENT

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