

MASS TRANSFER INSIDE OBLATE SPHEROIDAL SOLIDS: MODELLING AND SIMULATION

J. E. F. Carmo and A. G. B. Lima

Centro de Ciências e Tecnologia, Departamento de Engenharia Mecânica,
Universidade Federal de Campina Grande (UFCG),
Phone +(55) (83) 3310-1317, Fax + (55) 83 3310-1272,
Cx. P. 10069, CEP 58109-970, Campina Grande-PB, Brazil.
E-mail: gilson@dem.ufcg.edu.br

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Abstract - A numerical solution of the unsteady diffusion equation describing mass transfer inside oblate spheroids, considering a constant diffusion coefficient and the convective boundary condition, is presented. The diffusion equation written in the oblate spheroidal coordinate system was used for a two-dimensional case. The finite-volume method was employed to discretize the basic equation. The linear equation set was solved iteratively using the Gauss-Seidel method. As applications, the effects of the Fourier number, the Biot number and the aspect ratio of the body on the drying rate and moisture content during the process are presented. To validate the methodology, results obtained in this work are compared with analytical results of the moisture content encountered in the literature and good agreement was obtained. The results show that the model is consistent and it may be used to solve cases such as those that include disks and spheres and/or those with variable properties with small modifications.

Keywords: Mass transfer; Ellipsoid; Oblate spheroid; Drying, simulation; Finite volume.

INTRODUCTION

Rates of heat and mass transfer from a particle of arbitrary shape to an infinitely extended fluid are of considerable importance in certain engineering applications such drying, wetting, heating and cooling. A drying process undergoes different periods such as initial transient, constant rate and falling rate periods. It is well known that moisture (liquid and/or vapor phase) migration in the falling rate period is controlled by diffusion. There are various types of diffusion, namely molecular diffusion, liquid diffusion through solid pores, vapor diffusion in air filled pores and effusion (Knudsen type diffusion).

For many years, intense research on diffusion phenomena in porous bodies using the liquid diffusion model has been applied to different materials by several researchers with great success.

The liquid diffusion model assumes that water migrates through the solid in the liquid phase, and consequently water vaporization occurs at the surface of the porous body. The following recent works can be reported: Rastogi et al. (1997), Derdour and Desmorieux (2004), Lim et al. (2004), Porto and Lisboa (2005) and Rodriguez et al. (2005).

Fundamental solutions of the diffusion problems for spheres, cylinders, plates and parallelepipeds have been provided (Crank, 1992; Gebhart, 1993). There are many situations, however, where the particles are not spherical or cylindrical; for example, rice, wheat, banana, silkworm cocoon etc. may be classified as prolate spheroids and lentils as oblate spheroids. Numerical and analytical solutions of the diffusion equation for prolate spheroids have been reported by Payne et al. (1986), Oliveira (2001), Lima et al. (2002), Teruel et al. (2002) and Oliveira and Lima (2002), and for oblate spheroids

Payne et al. (1986), Farias (2002), Carmo (2004), Lima et al. (2004) and Carmo and Lima (2005).

An especially analytical solution for diffusion in spheroidal bodies is given for products of infinite series and complex integrals. Depending on the initial and boundary conditions, the series are, for example, in Bessel functions and Legendre polynomials, both of a high order. Each series consists of coefficients that are very complex to obtain, presenting in a formidable undertaking (Oliveira, 2001; Oliveira and Lima, 2002). In this case, the numerical solution is recommended because of its simplicity and speed in obtaining results.

The objectives of this investigation are as follows: a) to present a two-dimensional mathematical model to describe moisture transport inside oblate spheroidal solids which will depend only of the particle dimensions and b) to solve numerically the mass transport equation written in the oblate spheroidal coordinate system.

MATHEMATICAL MODELLING

Analytical Procedure

In this work, the following assumptions were made: the solid is homogeneous and isotropic; the drying process occurs at a falling drying rate; the heat conduction through the oblate spheroid is negligible; the field of moisture content is symmetric around the z-axis and constant and uniform at the beginning of the process; the thermo-physical properties are constant; the effect of capillarity is negligible; shrinkage is not important; and the process occurs under convective boundary conditions at the surface of the solid.

Fick's second law in Cartesian coordinates can be written as follows:

$$\frac{\partial M}{\partial t} = \frac{\partial}{\partial x} \left(D \frac{\partial M}{\partial x} \right) + \frac{\partial}{\partial y} \left(D \frac{\partial M}{\partial y} \right) + \frac{\partial}{\partial z} \left(D \frac{\partial M}{\partial z} \right) \quad (1)$$

Eq. (1) is an appropriate equation to predict the mass diffusion in bodies with a rectangular shape, such as plates and parallelepipeds. To predict the diffusion phenomenon in oblate spheroids, it is necessary to transform this equation into an appropriate coordinate system, in this case, the oblate spheroidal coordinate system. Fig. 1 shows a body with an oblate spheroidal shape.

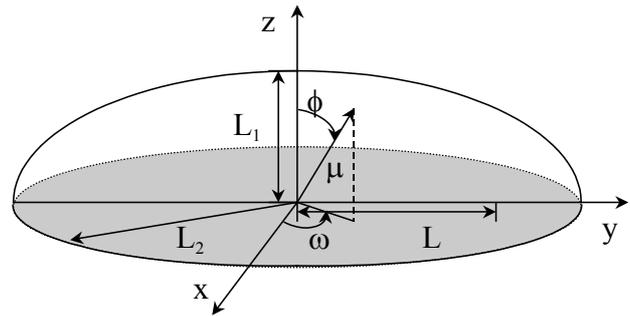


Figure 1: Characteristics of an oblate spheroid

The relationships between the Cartesian (x, y, z) and oblate spheroidal coordinate systems (μ, ϕ, ω) are given by Stratton et al. (1941) and Carmo (2004). By calculating the metric coefficients and Laplacian in the new coordinate system, using the symmetry around the z-axis, and considering the constant diffusion coefficient, Eq. (1) may be written as follows:

$$\frac{\partial M}{\partial t} = \left[\frac{1}{L^2 (\xi^2 + \eta^2)} \frac{\partial}{\partial \xi} \left((\xi^2 + 1) D \frac{\partial M}{\partial \xi} \right) + \frac{1}{L^2 (\xi^2 + \eta^2)} \frac{\partial}{\partial \eta} \left((1 - \eta^2) D \frac{\partial M}{\partial \eta} \right) \right] \quad (2)$$

The following initial, symmetry and boundary conditions are used:

$$M(\xi; \eta; 0) = M_0; \quad \frac{\partial M(\xi, \eta = 1, t)}{\partial \eta} = 0;$$

$$\frac{\partial M(\xi, \eta = 0, t)}{\partial \eta} = 0; \quad \frac{\partial M(\xi = 0, \eta, t)}{\partial \xi} = 0$$

$$\frac{D}{L} \sqrt{\frac{(\xi^2 + 1)}{(\xi^2 + \eta^2)}} \frac{\partial M}{\partial \xi} \Big|_{\xi = \xi_f} + h_m [M(\xi = \xi_f, \eta, t) - M_e] = 0 \quad (3a-c)$$

with $\xi_f = L_1/L$ in the surface.

The average moisture content of the body was calculated as follows:

$$\bar{M} = \frac{1}{V} \int_V M dV \quad (4)$$

where V is the overall volume in the domain under study.

Defining the following dimensionless parameters:

$$\eta^* = \eta \quad \xi^* = \xi \quad t^* = \frac{Dt}{L^2}$$

$$V^* = \frac{V}{L^3} \quad M^* = \frac{M - M_e}{M_o - M_e} \quad (5)$$

$$Bi = \frac{h_m L}{D}$$

we obtain the diffusion model (Eq. (2), Eq. (3a-c) and Eq. (4)) in the dimensionless form.

As a comment, in the models presented in the literature moisture diffusivity is assumed constant over the whole period. However, this consideration is not entirely true. It is valid for certain materials that have a slow drying rate (Lim et al., 2004). So, outside this condition, the model fails to adequately predict the experimental data, and thus a drying model should assume the diffusion coefficient to be a function of moisture content.

On the other hand, it is well known that the mass transfer coefficient depends on the geometry of the solid, velocity and thermo-physical properties of the fluid phase on the surface of the solid. Due to the complexity of the 3D-flow around ellipsoids of revolution (Geissler, 1974; Rosenfeld et al., 1992), it is very difficult to obtain the gradient velocity and concentration at the fluid-particle interface outside

the body, so the mass transfer rate is usually expressed in terms of the overall mass transfer coefficient (Strumillo and Kudra, 1986; Saravacos, 1995). As a result, as an approach the mean convective mass transfer coefficient on the surface of a spheroid can be obtained using either of the following methods: a) agreement between the predicted and experimental data using, for example, the least squares error technique (Queiroz, 1994; Lima et al., 2002; Carmo, 2004; Carmo and Lima, 2005) or b) empirical and theoretical mathematical correlations (Lochiel and Calderbank, 1964; Masliyah and Epstein, 1972; Clift et al., 1978; Coutelieris et al., 1995; Feng and Michaelides, 1997).

Finally, specifically for drying, the proposed mathematical model can be applied to liquid or vapor diffusion inside the solid.

Numerical Procedure

Due to the body symmetry, the computational domain shown in Fig. 2 where the nodal points (P, N, S, W, E) and constant lines of ξ and η are also presented, was adopted. It is possible to verify the existence of the symmetry in the plane that contains the points $(x=0, y=0, z=0)$ and $(x=0, y=0, z=L)$, in particular $y \geq 0$ and $z \geq 0$. The numerical solution of the problem utilizing the finite-volume method is obtained by integrating Eq. (2) (in the dimensionless form) with respect to space and time (Maliska, 2004).

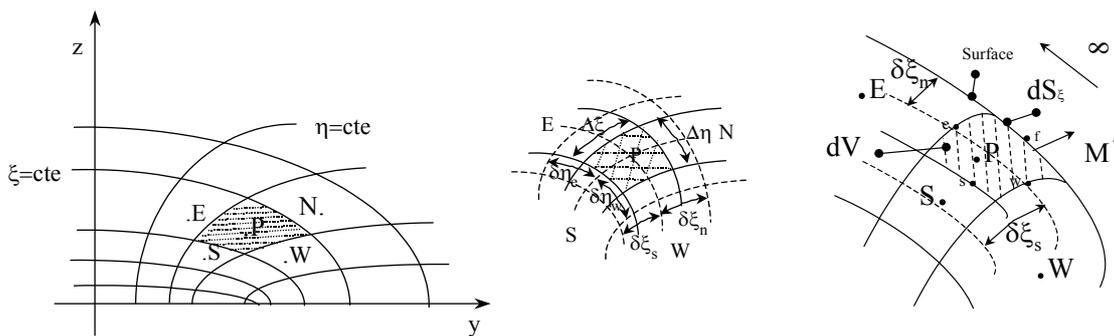


Figure 2: Control volume used in this work

RESULTS AND DISCUSSIONS

The numerical results using the finite-volume method are seriously affected by the $D\Delta t/L^2$ values and the number of grid points. In order to verify grid size and time step independence, results were

obtained with three grid sizes and time steps. In the numerical calculations we use $L_2=1.0 \times 10^{-2}$ m and $D=1.22 \times 10^{-9}$ m²/s in every test. Table 1 contains the deviations in the results on the mean moisture content for the three grids and different time steps for $L_2/L_1=100.00$ and $Bi=10.00$. An analysis of the

table shows that 20x20 nodal points and $D\Delta t/L^2=2.44 \times 10^{-6}$ provide satisfactory results (with an error less than 0.13%). Based on these parameters, numerical solutions of the mass diffusion equation for an oblate spheroid solid were obtained for various values of the input parameters. Details of this procedure can be found in the literature (Carmo, 2004).

To validate the numerical methodology used in the present work, Fig. 3 illustrates a comparison between the numerical results obtained by the authors and the analytical results reported in the literature (Farias, 2002). As shown, good agreement was obtained for all the cases reported in the literature.

Figs. 4 and 5 show the effect of the Fourier number on the drying kinetics of the solid for fixed values of other parameters. The curves correspond to different Biot numbers and body dimensions. An analysis of the curves indicates that the average moisture content decreases with increasing Fourier number for any Biot number and aspect ratio. For fixed values of aspect ratio, increasing the Bi increases the drying rate of the product, decreasing the Fourier number and consequently the overall drying time. It is possible to verify that solids with higher aspect ratios dry first, due to the area/volume relationship.

Table 1: Dimensionless mean moisture content for several grid sizes and dimensionless times. $L_2/L_1=100.0$ and $Bi=10.00$

$D\Delta t/L_2^2$	Dt/L_2^2	$(M - M_e)/(M_0 - M_e)$			Error (%)	
		Grid A: (10 x 10)	Grid B: (20 x 20)	Grid C: (40 x 40)	(B-A)/A	(C-B)/B
0.00000244	0.0000146	0.9786	0.9787	0.9787	0.01	0.00
	0.0000732	0.8993	0.8995	0.8996	0.02	0.01
	0.0003660	0.6004	0.6012	0.6016	0.13	0.06
0.00000366	0.0000146	0.9787	0.9787	0.9787	0.00	0.00
	0.0000732	0.8994	0.8996	0.8997	0.02	0.01
	0.0003660	0.6007	0.6014	0.6018	0.12	0.07
0.00000488	0.0000146	0.9787	0.9787	0.9788	0.00	0.01
	0.0000732	0.8995	0.8997	0.8998	0.02	0.01
	0.0003660	0.6010	0.6017	0.6021	0.12	0.07

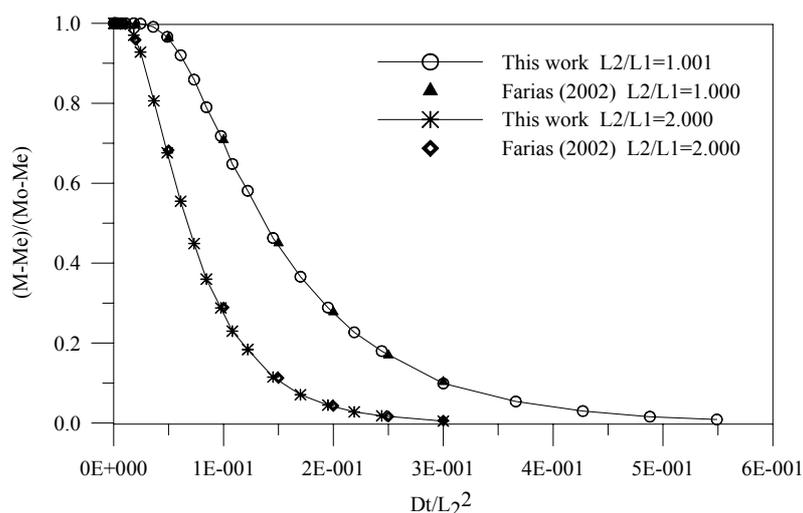


Figure 3: Comparison between numerical (this work) and analytical results on the dimensionless moisture content in the center of two oblate spheroids and $Bi = h_m L / D$ infinity

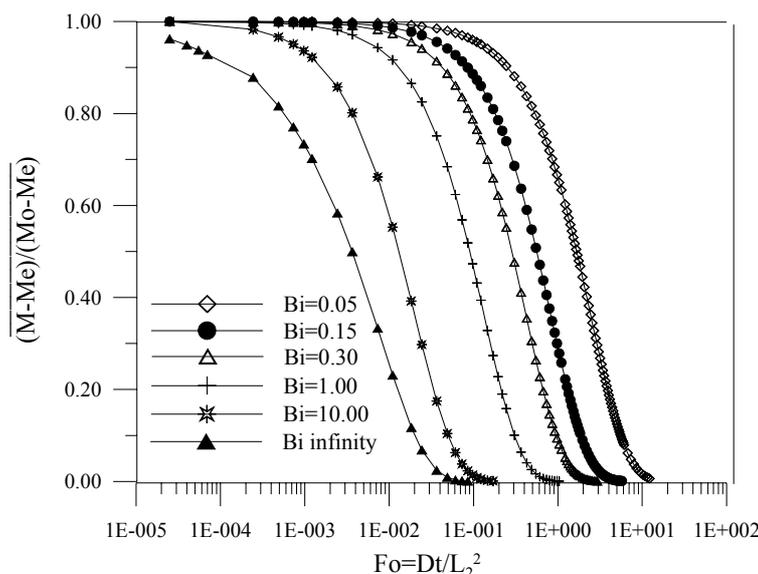


Figure 4: Dimensionless average moisture content of an oblate spheroid solid as a function of the Fourier number for $L_2/L_1=5.00$ and several Biot numbers.

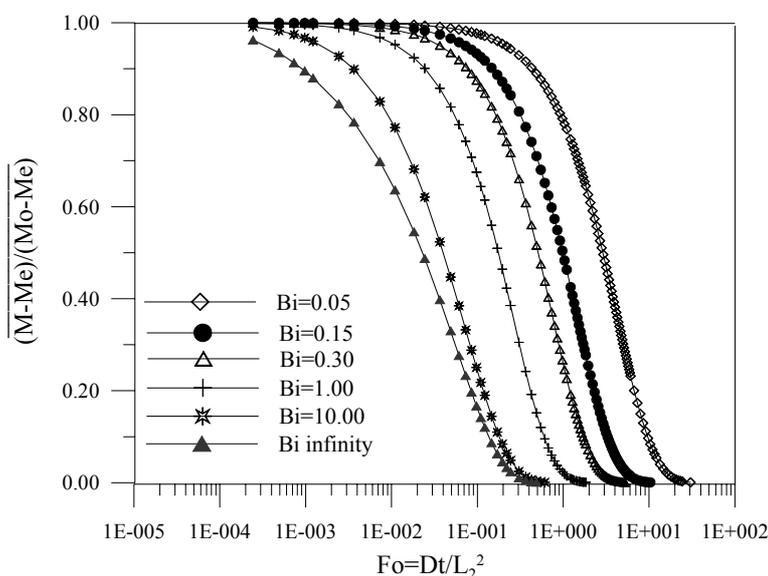


Figure 5: Dimensionless average moisture content of an oblate spheroid solid as a function of the Fourier number for $L_2/L_1=1.43$ and several Biot numbers.

The moisture content distribution inside an oblate spheroidal solid with an aspect ratio of $L_2/L_1=5.00$ and Bi infinity in three Fourier numbers is shown in Figures 6a-b. It can be observed that the moisture content at all the points inside the body decreases with the increase in Fourier number. In these illustrations, the isoconcentration lines are seen along and inside the body. It can be observed that these lines have a confocal elliptic shape. The results indicate that moisture diffusion is initially faster close to the focal point, decreasing with time of drying in the direction of the center of the solid. This behavior is due to the geometrical shape of the body.

High moisture gradients are undesirable because they can result in mechanical stress, cracks and deformations, reducing the quality of the product at the end of the process. As already noted, the bodies

with higher aspect ratios have focal points near the surface. It can be observed that in the vicinity of this point the moisture content decreases more quickly and larger moisture gradients are found. In this study, the effect of shrinkage on the drying rate and quality of the product was not analyzed because experimental tests would be required for verification.

As a final comment, although good fit was obtained in this study, it is necessary to dedicate more attention to the quantitative study of surface area and volume changes during the dehydration processes, especially in complex situations, such as simultaneous multidirectional deformations and changes in temperature. Multidirectional deformations occur for example in grape drying, where in the final process the surface of the product has a totally wrinkled texture.

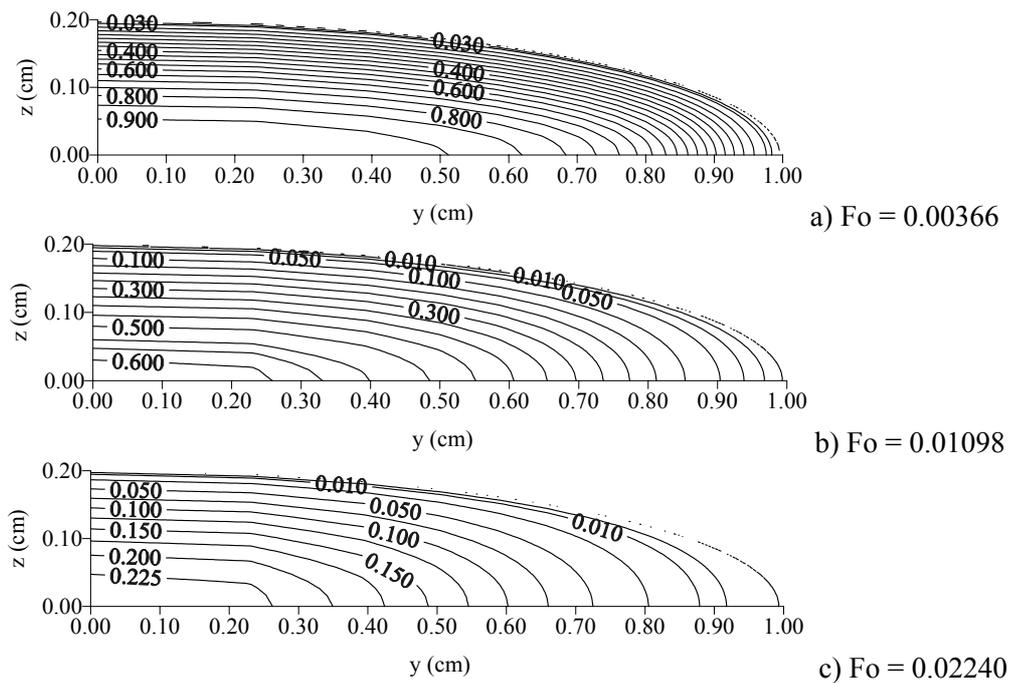


Figure 6: Dimensionless moisture content distribution in an oblate spheroid with an aspect ratio of $L_2/L_1=5.00$ and Bi infinity

CONCLUSIONS

A general fully numerical method for the solution of diffusion equation was developed and applied to the diffusion phenomenon in an oblate spheroid. The method uses a system of oblate spheroidal coordinates. With improved treatment of the diffusion equation, convergence is quickly achieved in each iteration and case studied in the nonsteady numerical simulation. The effect of singularity at the symmetry points of the spheroid was minimized using a regular grid. Satisfactory prediction of moisture content kinetics and distribution inside the solid was obtained.

By analysis of the results obtained, the following conclusions were reached: bodies with higher aspect ratios dry first for any Biot number; higher moisture gradients in the solid are found near the surface and around the focal point; and the model may be used in many physical problems of mass transfer, such as diffusion in circular disks, spheres and oblate spheroids and also in cases which include variable diffusion coefficients and other boundary conditions, with small modifications in the numerical procedure.

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NOMENCLATURE

Bi	Biot number of mass transfer	(-)
D	Diffusion coefficient	m^2/s
Fo	Fourier number of mass transfer	(-)
L	Focal length	m
L_1, L_2	Minor and major axis of the solid	M
M, \bar{M}	Local and average moisture content	kg/kg
t	Time	S
V	Volume	m^3
x, y, z	Cartesian coordinates	M

Greek Letters

ξ, η	Angular (\perp x axis), angular (\perp z axis) and radial coordinates	(-)
Δ, δ	Variation	(-)

Subscripts

e	Equilibrium	(-)
e,w,s,n	Boundary of the nodal points	(-)
o	Initial	(-)

Superscripts

*	Dimensionless	(-)
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