

## Influence of the Electrolyte Composition on the Kinetics of the Oxygen Evolution Reaction and Ozone Production Processes

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A influência da composição do eletrólito (ácido sulfúrico, ácido perclórico e suas misturas) sobre a cinética eletrodica da reação de desprendimento de oxigênio (*RDO*) e a produção eletroquímica de ozônio (*PEO*) em eletrodo de  $\beta$ - $\text{PbO}_2$ , foi investigada empregando-se a espectroscopia de impedância eletroquímica e curvas de polarização quase-estacionárias. A análise dos espectros de impedância revelou uma dependência da capacitância da dupla camada elétrica e da pseudo-capacitância de adsorção dos intermediários da reação com a composição do eletrólito. A pseudo-capacitância é função do potencial do eletrodo e da composição do eletrólito, indicando que a cobertura superficial pelos intermediários da reação depende destes parâmetros. Os valores do coeficiente de Tafel apoiam a descarga primária da água como sendo a etapa determinante da velocidade do mecanismo eletrodico descrevendo a *RDO* e a *PEO*. Os valores da eficiência da corrente para a *PEO* ( $\Phi_{\text{PEO}}$ ) mostram que os eletrólitos puros resultam numa produção máxima de ozônio quando comparados aos eletrólitos mistos. Baseada na análise teórica do mecanismo eletrodico, este comportamento é conseqüente da redução na concentração superficial dos centros ativos responsáveis pela *PEO* ocasionada pela adsorção de ânions.

The influence of electrolyte composition (pure sulphuric or perchloric acid and their mixtures) on the kinetics of the oxygen evolution reaction (*OER*) and the electrochemical ozone production (*EOP*) on  $\beta$ - $\text{PbO}_2$  electrodes was investigated by electrochemical impedance spectroscopy and quasi-stationary polarisation curves. Analysis of the impedance spectra revealed a dependency of the electric double layer capacity and the adsorption pseudocapacitance, due to reaction intermediates, on electrolyte composition. The pseudocapacitance is a function of electrode potential and electrolyte composition, indicating the surface coverage by the reaction intermediates depends on these parameters. Tafel slope data support primary water discharge as rate determining step of the *OER* and *EOP* electrode processes. *EOP* current efficiency data ( $\Phi_{\text{EOP}}$ ) show pure electrolytes lead to maximum  $\text{O}_3$  production when compared to mixed electrolytes. According to the theoretical analysis of the electrode mechanism, this behaviour is a consequence of the reduction in surface concentration of the active centres leading to *EOP* caused by anion adsorption.

**Keywords:** impedance spectroscopy, ozone production, oxygen evolution, kinetics, mixed electrolytes

### Introduction

Lead dioxide is a poor electrocatalyst for the oxygen evolution reaction, *OER*, and for this reason an interesting material for processes taking place at high positive potentials, such as electrochemical ozone production, *EOP*, or the oxidation of organic compounds.<sup>1-4</sup>

It has been shown<sup>1-3,5,6</sup> *EOP* is capable of generating higher ozone concentrations in the gaseous phase ( $\text{O}_2 + \text{O}_3$ ) than the conventional technologies (e.g. corona discharge, UV-process), thus permitting faster degradation of resistant organic pollutants in effluents (e.g. pesticides and dyes from the textile industry).

Fundamental investigations show the main parameters affecting *EOP* are:<sup>1-8</sup> (i) chemical nature of the electrode material; (ii) pre-treatment of the electrode; (iii) electrolyte

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composition; (iv) current density, and (v) electrolyte temperature. However, as discussed earlier,<sup>1-3,6-8</sup> the electrolyte composition is the single most important factor affecting *EOP*. This is due to the fact anion adsorption at the electrode surface strongly influences electrode kinetics and *EOP* current efficiency by affecting the electrochemical activation energy for the *OER* and the degree of coverage by reaction intermediates.<sup>1-3,8</sup> The introduction into the base electrolyte (e.g.  $\text{H}_2\text{SO}_4$ ) of anions having a high electronegativity (e.g.  $\text{BF}_4^-$ ,  $\text{F}^-$ ,  $\text{PF}_6^-$ ) influences *EOP* by changing the nature of the electrode/electrolyte interface, thus promoting an increase in the surface concentration of the active centres leading to *EOP*.<sup>1-3,8</sup>

The influence of the physicochemical properties on elementary processes at the  $\text{PbO}_2$  electrode/electrolyte interface was discussed by Pavlov and Monahov,<sup>9</sup> who proposed the *OER* takes place at active sites located in a hydrated (gel) zone of the oxide layer,  $[\text{PbO}(\text{OH})_2]$ . In this case the activity of the hydrated gel zone for the *OER* process can be affected by anion adsorption.

In the light of the considerations raised by Pavlov and Monahov,<sup>9</sup> Amadelli *et al.*<sup>4</sup> reported adsorption of  $\text{HSO}_4^-/\text{SO}_4^{2-}$  anions at  $\text{PbO}_2$  affects the electrode activity for the *OER* inhibiting both water discharge and desorption of reaction intermediates. These authors<sup>4</sup> established desorption of reaction intermediates is the rate determining step of the electrode process, and proposed elementary reactions leading to *OER* take place at a surface consisting of crystalline ( $\text{PbO}_2$ ) and hydrous  $[\text{PbO}(\text{OH})_2]$  zones. Ho *et al.*<sup>10</sup> also discussed the importance of the electrochemical adsorption behaviour at  $\text{PbO}_2$  electrodes of chemisorbed intermediates that are involved in electrocatalytic multistep electrode mechanisms.

As discussed previously,<sup>1-3</sup> the *OER* governs the current efficiency with the respect to the overall electrode process leading to the *OER/EOP* processes. Considering the particular case of sulphuric acid as electrolyte and lead dioxide as anode, the main side reaction taking place during the *OER* is ozone formation while persulphate formation is a minor side reaction. The theoretical approach, supported by the thermodynamic and kinetic data,<sup>1</sup> indicates partial surface coverage by adsorbed  $\text{O}_2$  molecules and  $\text{O}^\bullet$  radicals, which are both affected by electrode nature and electrolyte composition, are the main parameters governing *EOP* current efficiency.

Although the influence of the electrolyte composition on *OER/EOP* kinetics and *EOP* current efficiency has been extensively investigated,<sup>1-8,11</sup> a systematic investigation of the influence of mixed perchloric and sulphuric acid electrolytes on these processes is not reported in the literature.

We now report the results of an electrochemical impedance spectroscopy, *EIS*, investigation of the

influence of pure and mixed perchloric and sulphuric acid, on the *OER/EOP* kinetics at  $\beta\text{-PbO}_2$ .

## Experimental

### *Electrode preparation*

$\beta\text{-PbO}_2$  electrodes were prepared by electrodeposition at constant current from  $\text{Pb}(\text{NO}_3)_2$  acid solution onto both faces of a steel micro-sphere blasted Ti-support ( $10 \times 5 \times 0.12$  mm), previously etched for 5 min in boiling oxalic acid (10% m/m) and then platinised. The electrodeposition of Pt was carried out from a solution containing  $10 \text{ g dm}^{-3}$   $\text{H}_2\text{PtCl}_6 + 10 \text{ mg dm}^{-3}$   $\text{Pb}(\text{CH}_3\text{CO}_2)_2 \cdot 3\text{H}_2\text{O}$ , at  $24^\circ\text{C}$ , using a constant current density of  $30 \text{ mA cm}^{-2}$  for 5 min.  $\beta\text{-PbO}_2$  was then electrodeposited onto both sides of the platinised Ti-support from a solution containing  $0.2 \text{ mol dm}^{-3}$   $\text{Pb}(\text{NO}_3)_2 + 0.01 \text{ mol dm}^{-3}$   $\text{HNO}_3$ , at  $60^\circ\text{C}$ , using a constant current density of  $20 \text{ mA cm}^{-2}$  for 40 min. The average thickness of the  $\beta\text{-PbO}_2$  layer was estimated by weighing, using a  $\beta\text{-PbO}_2$  density<sup>12</sup> of  $9.375 \text{ g cm}^{-3}$  and the geometric electrode area of  $1 \text{ cm}^2$ . An average thickness of  $30 \mu\text{m}$  was obtained. Electrodes were mounted in a glass tube and sealed with silicon glue. Duplicate samples were prepared to check the reproducibility of the experimental data. Aldrich "purum p.a." products were used throughout.

### *Cell*

A three-compartment all-glass cell ( $0.2 \text{ dm}^3$ ) was used throughout. To avoid contact between the anodic (oxygen and ozone) and cathodic (hydrogen) gaseous products, a coarse glass frit separator was introduced separating the anodic and the cathodic compartments. Ohmic drop was minimised using a Luggin capillary approaching the working electrode from below, while two heavily platinised platinum counter electrodes ensured uniformity of the current on the two opposite faces of the sample. Electrode potentials were read against the reversible hydrogen electrode (RHE). The  $\text{H}_2$ -gas required to complete the RHE was generated *in situ* before its use. The RHE containing the electrolyte investigated was immersed directly in the electrolyte investigated and was separated from the main body of the cell by a coarse glass frit.

### *Procedures and equipment*

*EIS* study.  $\beta\text{-PbO}_2$  is a dynamic system that changes with the experimental conditions preceding the impedance measurements.<sup>9,13</sup> Therefore, to minimise the influence of the electrode history on experimental data,<sup>1,6</sup> prior to

taking measurements the PbO<sub>2</sub> electrode was washed with pure water and then immersed for 24 hours in a vessel containing pure water. Next, before application of the d.c. potential, located in the *OER* domain (1.75 to 2.24 V(*vs.* RHE)) the PbO<sub>2</sub> electrode was pre-conditioned ( $j = 100 \text{ mA cm}^{-2}$ ;  $t = 30 \text{ min}$ ) in the electrolyte under investigation. Impedance spectra were recorded covering the 10 mHz to 100 kHz frequency interval. To ensure linearity of the electrode response a small amplitude sine wave (5 mV(*p/p*)) was used throughout. As required by the linear system theory, validation of the *EIS*-data was performed applying the Kramers-Kronig test<sup>14,15</sup> using the software furnished with the AUTOLAB electrochemical system. Chi-square values,  $\chi^2$ ,  $\leq 10^{-4}$  were obtained in all cases. The equivalent circuit, EC, proposed in the literature<sup>10</sup> for the lead dioxide electrode using a d.c. potential interval where the *OER* evolution takes place in the absence of diffusion control, was applied to fit the impedance data using the EQUIVCRT program elaborated by Boukamp.<sup>16</sup>

*Quasi-stationary polarisation curves.* Prior to taking measurements, we applied the same treatment described above for the PbO<sub>2</sub> electrode. Using the potentiostatic mode, forwards and backwards polarisation curves ( $E$  *vs.*  $j$ ) were recorded twice sweeping cyclically the electrode potential, under quasi-stationary conditions ( $v = 0.1 \text{ mV s}^{-1}$ ),<sup>1-3</sup> covering the potential interval of  $\sim 1.70$  to 2.35 V(*vs.* RHE), which corresponds to a current density interval of  $\sim 0.1$  to 300 mA cm<sup>-2</sup>. Experimental data extracted from the backwards scan of the second consecutive polarisation curve were used in the kinetic study.

*Current efficiency for EOP,  $\Phi_{\text{EOP}}$ .* Ozone concentration in the N<sub>2</sub> stream, used to transport O<sub>3</sub> from the cell (anodic compartment) to the spectrophotometer (HACH model D4800), was measured under stationary conditions at 254 nm.  $\Phi_{\text{EOP}}$ -values were calculated using next equation:<sup>1-3</sup>

$$\Phi_{\text{EOP}}(\%) = [(A \dot{V} z F) / (\epsilon l I_T)] 100 \quad (1)$$

where:  $A$  = Absorbance at 254 nm;  $\dot{V}$  = volumetric gas flow rate (N<sub>2</sub> + O<sub>2</sub> + O<sub>3</sub>) (dm<sup>3</sup> s<sup>-1</sup>);  $z$  = number of electrons (= 6);  $\epsilon$  = ozone absorptivity<sup>17</sup> at 254 nm (3024 cm<sup>-1</sup> mol<sup>-1</sup> dm<sup>3</sup>);  $l$  = cuvette optical path (10 cm);  $I_T$  = total current (*OER* + *EOP*) (A);  $\Phi_{\text{EOP}}$  = ozone current efficiency (%);  $F$  = Faraday's constant (96485 C mol<sup>-1</sup>).

An AUTOLAB (Eco Chemie, The Netherlands) electrochemical system (GPES), model PGSTAT20, was used throughout. Temperature control was done by means of a model FC55A01 FTS cooling system.

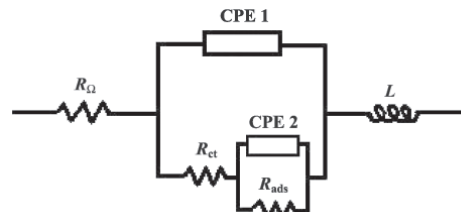
## Solutions

Electrochemical studies were carried out using as electrolyte different mixtures of 3.0 mol dm<sup>-3</sup> H<sub>2</sub>SO<sub>4</sub> (Vetec) and 6.0 mol dm<sup>-3</sup> HClO<sub>4</sub> (Merck), prepared volumetrically using twice distilled water with a final pass through a Millipore Milli-Q<sub>plus</sub> apparatus. Fourteen solutions were prepared changing the [H<sub>2</sub>SO<sub>4</sub>]:[HClO<sub>4</sub>] ratio.

## Results and Discussion

### *Analysis of the electrode behaviour in the frequency domain for the OER*

Electrochemical Impedance Spectroscopy, *EIS*, is a powerful technique for investigation of gas evolution reactions at solid electrodes<sup>10,18-22</sup> (e.g. H<sub>2</sub>, O<sub>2</sub>, Cl<sub>2</sub>). The response in the frequency domain of an electrochemical reaction can be simulated based on an intuitive but rationally chosen equivalent circuit.<sup>10</sup> A circuit model predicting two time constants in the frequency domain can adequately describe the *OER* or *OER/EOP* processes, at the inert  $\beta$ -PbO<sub>2</sub> electrode. Figure 1 presents the EC model proposed by Ho *et al.*<sup>10</sup> for the *OER* at the PbO<sub>2</sub> electrode in the absence of diffusion control.



**Figure 1.** Equivalent circuit for an electrode process presenting adsorption/desorption of an electroactive chemisorbed intermediate.

In the above EC model  $R_{\Omega}$  represents the uncompensated solution resistance; CPE1 the double layer capacitance ( $C_{dl}$ );  $R_{ct}$  the charge transfer resistance; CPE2 the adsorption pseudocapacitance of the reaction intermediates ( $C_{ads}$ );  $R_{ads}$  the resistance imposed by the reaction intermediates adsorbed at the electrode surface. Introduction of a serial inductor,  $L$ , is necessary to represent the inductive behaviour comprising the spurious and the effective inductance observed in the high frequency domain.<sup>18,19,23</sup>

Constant phase elements (CPE), instead of capacitors (C), were used to fit the experimental data.<sup>24</sup> According to the literature,<sup>21,24-26</sup> the use of CPE is a good approach for the study of solid electrodes with different degrees of surface roughness, physical nonuniformity or a nonuniform distribution of surface reaction sites. The impedance of the CPE can be written as:<sup>26-29</sup>

$$Z_{\text{CPE}} = \frac{1}{T(j\omega)^n} \quad (2)$$

where  $T$  is the capacity parameter expressed in  $\text{F cm}^{-2} \text{s}^{(n-1)}$ . The power  $n$  is related to the depression angle ( $\psi$ ) according to the following equation:

$$\psi = (1-n)\pi/2 \quad (3)$$

Experimentally, the CPE behaviour shows up as a clockwise rotation by an angle  $\psi$  of the complex plane plot referred to an ideal smooth electrode surface. Thus,  $T = C$  only when the solid electrode behaves as an ideal flat electrode ( $n = 1$ ).

Brug *et al.*<sup>27</sup> proposed that the double layer capacitance ( $C_{\text{dl}}$ ) is coupled with the uncompensated solution resistance ( $R_{\Omega}$ ) and the charge transfer resistance ( $R_{\text{ct}}$ ) according to the following equation:

$$T = (C_{\text{dl}})^n [(R_{\Omega})^{-1} + (R_{\text{ct}})^{-1}]^{(1-n)} \quad (4)$$

Thus, using the model described by equation 4,  $C_{\text{dl}}$  values were calculated using  $T$ -values obtained from the CNLS fit.<sup>21,24-26</sup>

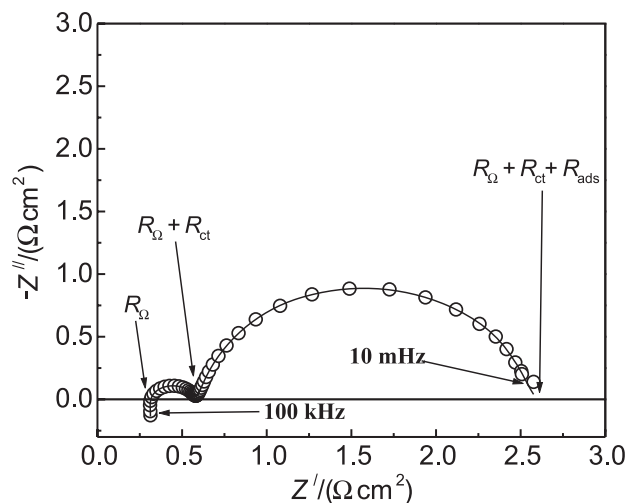
Since equation 4 was indeed proposed for the special case involving the double layer capacitance,<sup>27</sup> in the case of the pseudo-capacitive behaviour caused by adsorption of the reaction intermediates we used the  $T$ -parameter obtained from CPE2 to describe the influence of the electrolyte composition on the adsorption pseudo-capacitance. Such consideration is based in the fact that when  $n$  is close to one (see Table 2) the CPE2 adequately describes the pseudo-capacitance behaviour.<sup>28,29</sup>

The theoretical aspects related with the adsorption pseudo-capacitance and its true significance was discussed previously by Harrington and Conway.<sup>30</sup>

Considering that the main parameter governing  $EOP$  current efficiency is the degree of competition between the  $\text{O}_2$  and  $\text{O}_3$  electrode processes, the investigation of the influence of the electrolyte nature on the  $OER$  constitutes an important fundamental issue for the electrochemical technology oriented towards ozone production. In the light of these considerations, impedance measurements were carried out as function of the d.c. electrode potential ( $E_{\text{dc}}$  interval where  $OER$  and  $OER/EOP$  take place) and the electrolyte composition.

Figure 2 shows a complex-plane plot,  $Z'$  vs.  $Z''$ , representative of the frequency response for the  $OER$  at the  $\beta\text{-PbO}_2$  electrode.

Figure 2 reveals the complex-plane is mainly characterised by two well separated semicircles,



**Figure 2.** Complex plane plot representative of the frequency response at  $\beta\text{-PbO}_2$  during the  $OER$ .  $E_{\text{dc}} = 1.91\text{V}$ (vs. RHE). (o) experimental data; (—) simulation. Electrolyte:  $6.0 \text{ mol dm}^{-3} \text{ HClO}_4$ .  $T = 24 \text{ }^\circ\text{C}$ .

distributed in the low and high frequency domains, thus revealing an excellent agreement with the EC model originally proposed for the  $OER$  at  $\text{PbO}_2$  in the absence of diffusion control<sup>10</sup> (see Figure 1). As discussed in a previous paper,<sup>18</sup> a clear separation of the semicircles in the complex plane depends on the intrinsic physico-chemical properties of the electrode/electrolyte interface and the electrode potential. From a theoretical point of view, complete deconvolution of the complex plane semicircles is only possible if the ratio between the relaxation frequencies is greater than two orders of magnitude<sup>31</sup> ( $w_{01}/w_{02} > 100$ ). This limit reveals the difficulty to observe a perfect deconvolution of the semicircles in real cases.

According to the literature,<sup>4,10</sup> the semicircle observed in the low frequency domain is due to reaction intermediates adsorption formed during the  $OER$  or  $OER/EOP$  processes, while the semicircle in the high frequency domain describes the resistive/capacitive behaviour associated with the electron transfer (faradaic process) coupled with the double layer charging process.

Independently of electrolyte composition,  $R_{\Omega}$ -values in the  $0.30$  to  $0.60 \text{ } \Omega \text{ cm}^2$  range were obtained (see Table 1). These results are in good agreement with  $EIS$  data obtained for conductive metallic oxide electrodes immersed in strong electrolytes.<sup>18,19,21</sup> An inductance in the high frequency domain of about  $10 \text{ } \mu\text{H cm}^2$  was observed in all cases. As previously discussed by Da Silva *et al.*,<sup>18,19</sup> this inductive behaviour, normally presented by conductive metallic oxide films, is caused by different factors: (i) shape and relative position of the electrodes and their electric and electrolytic connections, which result in the spurious inductance ( $L_s$ ) connected in series with

the electrode impedance, and (ii) the disordered movement of the charge carriers at the surface of the complex electrode micro-structure (pores, cracks, grain boundaries, etc.), which can result in the effective inductance ( $L_E$ ). According to these authors,<sup>18,19</sup> the effective inductance in the high frequency domain is influenced by the resistive components associated with the electrode system according to the next equation:

$$L_E = \omega^{-1}[(Z_p)^2 - \gamma(\Sigma R)^2]^{1/2} \quad (5)$$

where  $Z_p$  is the impedance due to the effective inductance ( $L_E$ ) coupled with resistive components (e.g.  $\Sigma R = R_\Omega + R_{ct}$ );  $\omega$  is the angular frequency, and  $\gamma$  is the dimensionless parameter ( $0 \leq \gamma \leq 1$ ) describing the true contribution of the resistive components to  $Z_p$ .

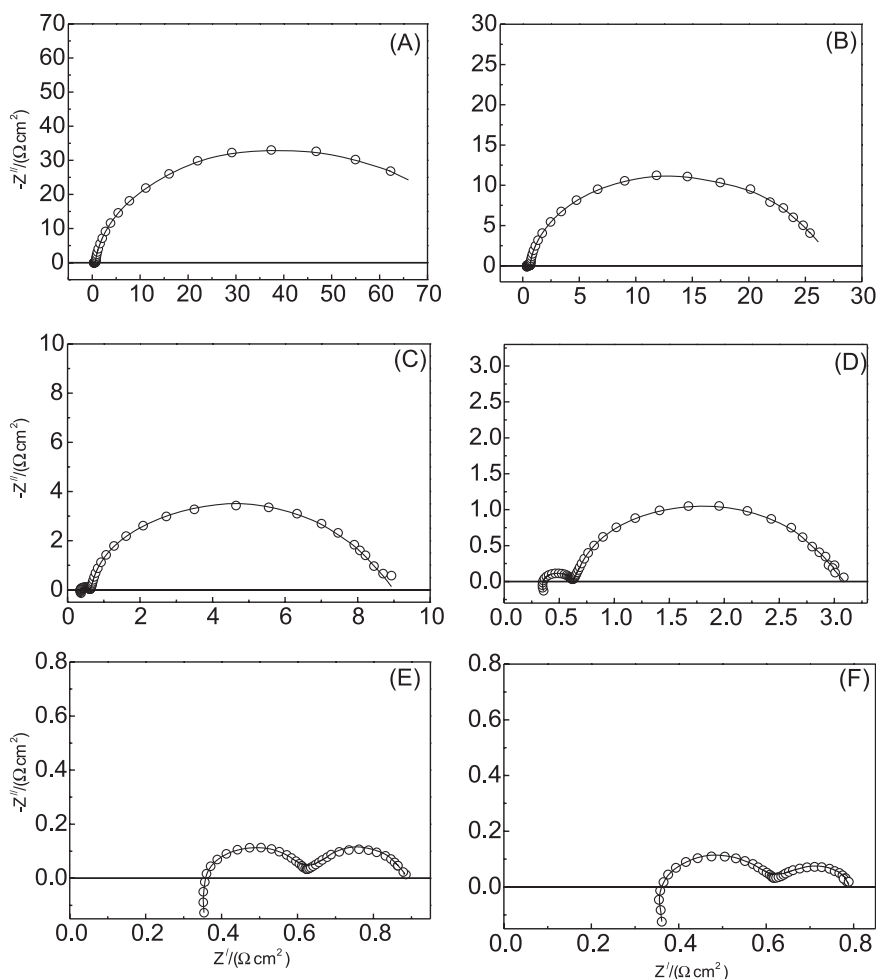
The influence of physico-chemical nature of the electrode/electrolyte interface on the inductive behaviour present in the high frequency domain was recently discussed by Bisquert *et al.*,<sup>23</sup> who proposed a model for

the electrochemical behaviour of electroactive material containing heterogeneity or energy disorder, and proved that charge relaxation can lead to an inductive behaviour in the high frequency domain.

Figure 3 shows complex-plane plots ( $Z'$  vs.  $Z''$ ) as function of the d.c. electrode potential, which are representative of the electrochemical behaviour of the *OER* (low overpotential domain) and *OER/EOP* (high overpotential domain) at the  $\beta$ - $\text{PbO}_2$ .

Figure 3 clearly shows the resistance imposed by adsorption of the reaction intermediates at the electrode surface,  $R_{ads}$ , considerable decreases on increasing the d.c. electrode potential,  $E_{dc}$ . According to the literature,<sup>4,10,30-33</sup> this behaviour can be correlated with the exponential dependency established between  $R_{ads}$  and  $E_{dc}$  (Tafel behaviour). For the case where  $R_{ads}$  is significant when compared to the  $R_{ct}$  ( $R_{ads} \gg R_{ct}$ ), one has that  $R_{ads}$  governs the electrode kinetic.<sup>4,29,32,33</sup>

Table 1 shows the influence of electrolyte composition and the electrode potential on impedance parameters.



**Figure 3.** Representative complex plane plots as function of the d.c. electrode potential.  $E_{dc}/V$  vs. (RHE): (A) 1.75; (B) 1.80; (C) 1.86; (D) 1.91; (E) 2.13; (F) 2.20. (o) experimental data; (—) simulation. Electrolyte:  $[\text{H}_2\text{SO}_4]:[\text{HClO}_4] = 1:6$ .  $T = 24$  °C.



Analysis of Table 1 reveals that  $C_{dl}$  depends on both electrolyte composition and electrode potential. In the low overpotential case (1.75V),  $C_{dl}$  values are almost constant, presenting a maximum for the pure  $H_2SO_4$  solution. Table 1 also shows the influence of electrolyte composition on  $C_{dl}$  is more pronounced in the high overpotential domain (2.19V), where a sudden and strong increase in  $C_{dl}$  values is observed for  $[H_2SO_4]:[HClO_4] > 1:10$ . For  $[H_2SO_4]:[HClO_4] \geq 1:3$  the  $C_{dl}$  value is approximately constant. Again, the maximum  $C_{dl}$  value is obtained in the pure  $H_2SO_4$  solution. These findings are in agreement with the literature,<sup>4</sup> which reports sulphuric acid presents higher  $C_{dl}$  values than other electrolytes due to the strong  $HSO_4^-$  adsorption when compared to the  $ClO_4^-$  anion.

The adsorption of the several different anions ( $NO_3^-$ ,  $Cl^-$ ,  $ClO_4^-$ ,  $HSO_4^-/SO_4^{2-}$ ) on  $PbO_2$  electrodes, in acid medium, was investigated using the radioisotope and potentiometric techniques by Kokarev *et al.*,<sup>34</sup> who found that the sulphate adsorption increases on increasing the electrode potential. In all cases these authors<sup>34</sup> found the anion adsorption increases on increasing the electrolyte concentration according to the Freundlich isotherm. Also, the anion adsorption on lead dioxide was found to obey the following series:  $SO_4^{2-} > HSO_4^- > Cl^- > ClO_4^- > NO_3^-$ , thus confirming the superior adsorptive properties of the  $SO_4^{2-}$  and  $HSO_4^-$  anions observed in the present work.

Analysis of the impedance data obtained for the exploited electrode potential interval (1.75 to 2.24 V (*vs.* RHE)) revealed that  $R_{ct}$  is little affected by  $E_{dc}$ . In fact, analysis of Table 1 clearly shows a maximum change in  $R_{ct}$  less than 100  $m\Omega\ cm^2$ , thus revealing that charge transfer only plays a minor influence to the overall electrode impedance when compared to the  $R_{ct}$ .

### Kinetic study

*Analyses of the adsorption pseudocapacitance.* As already mentioned in this work, the behaviour of the adsorption pseudo-capacitance as function of the electrolyte composition and the electrode potential was investigated via CPE2, using the  $T$  values obtained from the CNLS fit.

Table 2 shows the dependence of the adsorption behaviour via CPE2 ( $T$ -parameter) on the electrolyte composition and the electrode potential.

Analysis of Table 2 reveals the influence of the electrode potential on  $T$  is most pronounced for electrolytes presenting a  $[H_2SO_4]:[HClO_4]$  ratio in the 1:58 to 1:4 interval. These findings also show pure sulphuric acid presents higher  $T$  values when compared to pure perchloric acid, thus indicating the presence of  $SO_4^{2-}/HSO_4^-$  anions at the electrode/electrolyte interface promotes an increase in the surface coverage by the reaction intermediates. Table 2 also shows the  $T$  values are lower for mixed electrolytes in both low and high overpotential domains passing through a minimum around  $[H_2SO_4]:[HClO_4] = 1:2$  indicating the presence in the electrolyte of  $HSO_4^-/ClO_4^-$  anions leads to a considerable reduction in the surface coverage by reaction intermediates.

Analysis of Table 2 also reveals that the resistance imposed by reaction intermediates adsorbed at the electrode surface,  $R_{ads}$ , suffers a considerable decrease on increasing  $E_{dc}$  (it was found in all cases that  $R_{ads}$  presents an exponential decay on increasing the electrode potential). It was also verified that  $R_{ads}$  does not present any systematic dependence on the electrolyte composition.

*Analysis of the Tafel behaviour.* Figure 4 shows the dependence of the charge transfer (Figure 4A),  $R_{ct}$ , and the

**Table 1.** Influence of the electrolyte composition and the electrode potential on impedance parameters ( $R_{\Omega}$ ,  $C_{dl}$  and  $R_{ct}$ )

Electrolyte <sup>a</sup> [H <sub>2</sub> SO <sub>4</sub> ]:[HClO <sub>4</sub> ]	$R_{\Omega} / (\Omega\ cm^2)$	$C_{dl} / (\mu F\ cm^2)$		$R_{ct} / (m\Omega\ cm^2)$		$n$
		$E / 1.75V$	$E / 2.19V$	$E / 1.75V$	$E / 2.19V$	
0:6	0.33	105	11	378	310	0.98
1:58	0.38	110	11	245	232	0.97
1:22	0.45	112	11	287	224	0.93
1:10	0.40	113	17	326	257	0.98
1:6	0.35	114	50	331	270	0.95
1:4	0.55	115	90	271	229	0.97
1:3	0.44	120	100	390	327	0.94
1:2	0.51	123	99	387	319	0.97
1:1.4	0.60	114	99	321	260	0.99
1:1	0.38	110	98	337	269	0.91
1.5:1	0.30	112	97	383	304	0.93
2.5:1	0.44	116	97	325	306	0.98
5.5:1	0.42	122	102	286	229	0.92
3:0	0.55	128	107	287	225	0.98

<sup>a</sup>[H<sub>2</sub>SO<sub>4</sub>] = 3.0 mol dm<sup>-3</sup>; [HClO<sub>4</sub>] = 6.0 mol dm<sup>-3</sup>.

**Table 2.** Dependence of the adsorption behaviour via CPE2 and the adsorption resistance on electrolyte composition and electrode potential

Electrolyte <sup>a</sup> [H <sub>2</sub> SO <sub>4</sub> ]:[HClO <sub>4</sub> ]	T / (mF cm <sup>-2</sup> s <sup>(n-1)</sup> )		R <sub>ads</sub> / (Ω cm <sup>2</sup> )		n
	E / 1.75V	E / 2.19V	E / 1.75V	E / 2.19V	
0:6	90	78	64	0.27	0.93
1:58	87	81	70	0.25	0.91
1:22	85	107	75	0.24	0.89
1:10	83	189	74	0.25	0.95
1:6	84	107	78	0.18	0.91
1:4	85	75	53	0.22	0.88
1:3	80	70	73	0.23	0.91
1:2	72	62	70	0.20	0.90
1:1.4	78	70	76	0.21	0.93
1:1	82	79	71	0.23	0.91
1.5:1	85	85	74	0.22	0.89
2.5:1	90	90	68	0.22	0.91
5.5:1	95	100	60	0.19	0.90
3:0	108	137	53	0.20	0.89

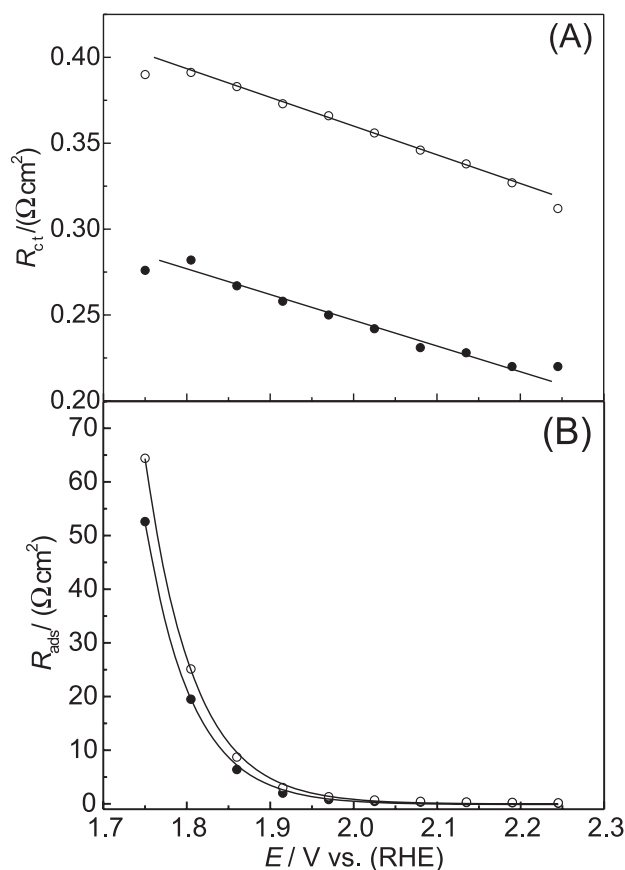
<sup>a</sup>[H<sub>2</sub>SO<sub>4</sub>] = 3.0 mol dm<sup>-3</sup>; [HClO<sub>4</sub>] = 6.0 mol dm<sup>-3</sup>.

adsorption (Figure 4B),  $R_{ads}$ , resistances on electrode potential. Analysis of the results shows a well-defined exponential decrease of the resistance with increasing electrode potential (Tafel's law) is only attained in the case of  $R_{ads}$ . Such behaviour is in agreement with the literature,<sup>10</sup> and reveals the *OER* or *OER/EOP* electrode processes is governed by the resistance related to the adsorption impedance due to reaction intermediate formation.<sup>10,30,32</sup>

The Tafel behaviour, under conditions of the high field approximation, is described by the experimental profile<sup>10,30,32</sup>  $E$  vs.  $\log(R_{ads}^{-1})$ , and the Tafel coefficient,  $b$ , can be obtained from the slope of the linear segment according to the definition  $b \equiv (\partial E / \partial \log R_{ads}^{-1})_T$ . In order to provide a comparison of the Tafel slopes obtained from the *EIS*, polarisation curves ( $E$  vs.  $\log(j)$ ) under quasi-stationary conditions ( $n = 0.1$  mV s<sup>-1</sup>)<sup>1-3</sup> were recorded for the several different electrolytes, using approximately the same electrode potential interval.

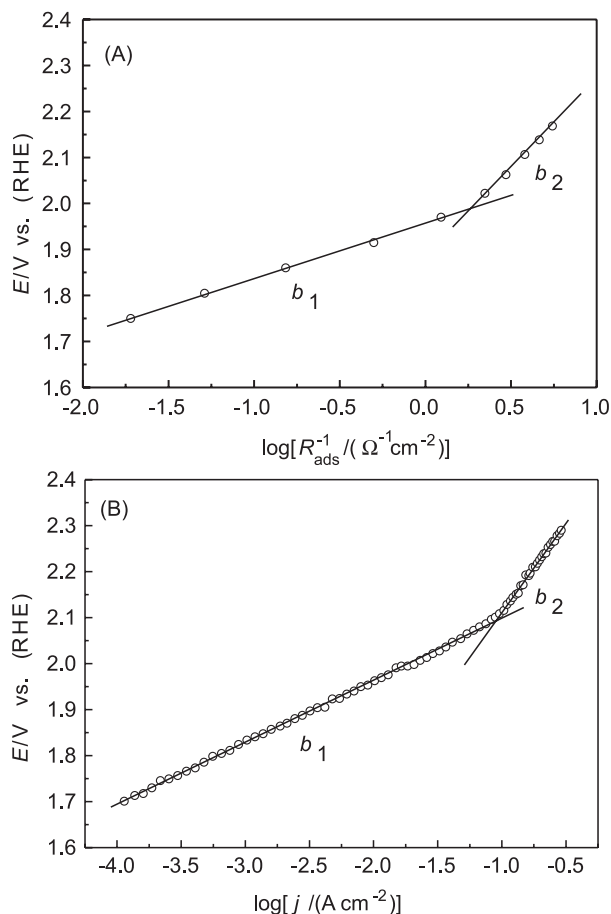
As discussed previously,<sup>1-3</sup> in the case of acid medium the current density in the high overpotential domain describes the *OER/EOP* processes at the  $\beta$ -PbO<sub>2</sub>, since persulphate formation at high overpotentials, in the case of electrolytes containing the sulphuric acid, can be considered negligible.<sup>1-3</sup> Besides, considering a low current efficiency for the ozone production ( $\Phi_{EOP} < 10\%$ , see Table 4), it can be assumed that the electrode process leading to *EOP* comprises a minor process from a kinetic point of view when compared to the *OER*. As discussed previously,<sup>1,7</sup> the main contribution for the electrochemical activation energy in the high overpotential domain comes from the *OER* processes.

Figure 5 shows Tafel plots already corrected for ohmic drop and obtained using different experimental techniques.



**Figure 4.** Dependence of the charge transfer,  $R_{ct}$ , and the adsorption,  $R_{ads}$ , resistances on electrode potential. Electrolyte: (●) [H<sub>2</sub>SO<sub>4</sub>]:[HClO<sub>4</sub>] = 1:4; (○) [H<sub>2</sub>SO<sub>4</sub>]:[HClO<sub>4</sub>] 0:6.  $T = 24$  °C.

Figure 5 clearly shows two linear segments distributed in the low,  $b_1$ , and high,  $b_2$ , overpotential domains. In all cases we found that  $b_1 < b_2$ . A comparison of Figure 5A and 5B clearly reveals an excellent correspondence of the Tafel profiles obtained using different experimental



**Figure 5.** Tafel plots for the OER at  $\beta\text{-PbO}_2$ . Experimental technique: (A) EIS; (B) Quasi-stationary polarisation.  $[\text{H}_2\text{SO}_4]:[\text{HClO}_4] = 1:3$ .  $T = 24^\circ\text{C}$ .

techniques. In the light of discussion presented above, we assumed that  $b_1$  mainly represents the OER, while  $b_2$  describes the OER/EOP processes.<sup>1-3</sup>

As previously discussed by Kötzt and Stucki,<sup>7</sup> the polarisation curve representing the OER process on  $\text{PbO}_2$  at low current densities is characterised by a Tafel slope of  $\cong 120 \text{ mV}$  (see Table 3). However, at higher current densities where the  $\text{O}_3$  evolution takes place the  $E$  vs.  $\log j$  profile considerable depends on the procedure used for ohmic drop correction (*positive feedback* or *current interruption*). These authors<sup>7</sup> found that the  $IR_{\Omega}$  compensation via positive feedback leads to a second linear segment characterised by a higher Tafel slope ( $b_1 < b_2$ ), while in the special case of the current interruption technique an opposite behaviour was verified ( $b_1 > b_2$ ). The latter was also verified by Amadelli *et al.*<sup>4,32</sup> for the OER/EOP processes on  $\text{PbO}_2$ .

Kötzt and Stucki<sup>7</sup> argued that  $IR_{\Omega}$  is not constant on overpotential, and therefore the dynamic compensation for ohmic drop based on the current interruption is more appropriate than the positive feedback. Considering that a standard procedure for  $IR_{\Omega}$  correction is not available in

the literature, in our opinion the choice of a specific procedure in this case is merely arbitrary. In fact, recent reports<sup>1,3,8</sup> clearly reveal the use of a different procedure for  $IR_{\Omega}$  correction also provides a good linearisation of the Tafel curve in the high current density domain.

From the above considerations, we decided to present in the present work a comparative kinetic study based on application of the treatment proposed by Shub and Reznik<sup>35</sup> and the impedance method for ohmic drop correction of the polarisation curves obtained using different experimental approaches.

In the case of quasi-stationary polarisation curves the correction for the ohmic drop was carried out using the procedure proposed by Shub and Reznik,<sup>35</sup> where the influence of ohmic drop,  $IR_{\Omega}$ , on the polarisation curve can be written as:

$$E_c = E_{\text{app}} - IR_{\Omega} = a + b \log j \quad (6)$$

where  $E_c$  is the corrected electrode potential,  $E_{\text{app}}$  is the applied electrode potential,  $R_{\Omega}$  is the uncompensated ohmic resistance,  $a$  is a constant and  $b$  is the Tafel slope. According to the literature,<sup>36,37</sup> the optimum  $R_{\Omega}$ -value is obtained using as criterion a correlation coefficient,  $r$ , for the experimental data in the high overpotential domain higher than 0.9998. Depending on the quality of the experimental data, a very good linearisation of the corrected Tafel curve can be obtained. All Tafel curves, after ohmic drop correction, presented  $r \geq 0.9998$ .

For the several electrolyte compositions investigated,  $R_{\Omega}$  values in the 0.3 to 0.8  $\Omega \text{ cm}^2$  range were obtained. These values are in excellent agreement with the corresponding ones obtained from EIS (see Table 1), and those reported in the literature<sup>1,8,21</sup> for conductive metallic oxide electrodes immersed in strong electrolytes.

In the special case of the polarisation curves obtained from EIS the ohmic drop correction was carried out using next equation:

$$E_c = E_{\text{app}} - IR_{\Omega} \quad (7)$$

where  $R_{\Omega}$  is the uncompensated ohmic resistance obtained from the CNLS fit and  $I$  is the d.c. current available from the EIS data. The other symbols have their usual meaning already described.

The dependence of the Tafel slope on electrolyte composition and the overpotential interval is presented in Table 3.

A comparison of the Tafel slope values obtained from EIS ( $E$  vs.  $\log(R_{\text{ads}}^{-1})$ ) and quasi-stationary polarisation curves ( $E$  vs.  $\log(j)$ ), revealed a good agreement between



**Table 3.** Dependence of the Tafel slope on electrolyte composition and overpotential interval

Electrolyte <sup>a</sup> [H <sub>2</sub> SO <sub>4</sub> ]:[HClO <sub>4</sub> ]	<i>b</i> <sub>1</sub> <sup>b</sup> /mV low η		<i>b</i> <sub>2</sub> <sup>b</sup> /mV high η	
	(EIS)	( <i>E</i> vs. log <i>j</i> )	(EIS)	( <i>E</i> vs. log <i>j</i> )
0:6	130	138	390	410
1:58	120	125	420	440
1:22	120	128	410	440
1:10	120	132	430	490
1:6	120	120	390	385
1:4	120	130	400	420
1:3	120	125	375	390
1:2	120	118	365	370
1:1.4	120	127	363	373
1:1	120	131	363	375
1.5:1	120	120	365	370
2.5:1	120	128	365	371
5.5:1	120	120	330	335
3:0	120	125	300	310

<sup>a</sup>[H<sub>2</sub>SO<sub>4</sub>] = 3.0 mol dm<sup>-3</sup>; [HClO<sub>4</sub>] = 6.0 mol dm<sup>-3</sup>; <sup>b</sup> obtained from Tafel curves corrected for ohmic drop.

these techniques. This internal consistency considerable supports the application of the procedure proposed by Shub and Reznik<sup>35</sup> for  $IR_{\Omega}$  correction and the significance of the Tafel slope data obtained at higher current densities.

Table 3 also shows that, with the exception for the pure HClO<sub>4</sub> solution ([H<sub>2</sub>SO<sub>4</sub>]:[HClO<sub>4</sub>] = 0:6), *b*<sub>1</sub> values do not depend on electrolyte composition. On the contrary, *b*<sub>2</sub> values depend on electrolyte composition, indicating electrode kinetics in the high overpotential domain are affected by the nature of the anions at the electrode/solution interface. Table 3 reveals the maximum *b*<sub>2</sub> value is presented by the electrolyte composition having a [H<sub>2</sub>SO<sub>4</sub>]:[HClO<sub>4</sub>] = 1:10 ratio, while for the composition interval between 1:2 and 2.5:1 a *b*<sub>2</sub> value of ~ 370 mV is observed. The minimum Tafel slope is displayed by pure sulphuric acid. Similar results were reported by Chernik *et al.*,<sup>11</sup> who reported *b*<sub>2</sub> values higher than 300 mV for the *OER/EOP* processes taking place on PbO<sub>2</sub> and Pt in concentrated H<sub>2</sub>SO<sub>4</sub> solution.

Interpretation of these abnormal Tafel slope values observed in the high overpotential domain is rather difficult from a theoretical point of view. A careful theoretical analysis of the complex behaviour presented by the Tafel slope for electrode processes taking place at solid electrodes was presented by several authors.<sup>38-41</sup>

As previously discussed for the PbO<sub>2</sub> electrode,<sup>1-3,8,33</sup> abnormal Tafel slopes can be attributed to anion adsorption and bubble adherence on the electrode surface. A revision of the literature reports<sup>1-4,7,11,26,33</sup> reveals abnormal Tafel slope values in the high overpotential domain for the *OER/EOP* processes at the β-PbO<sub>2</sub> electrode present values covering the 70 to 634 mV interval. Rationalisation of these data

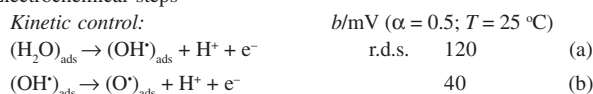
supports changes in the Tafel slope, especially in the high overpotential domain, are associated with factors such as: (i) electrodeposition conditions, which control the fraction of α and β-forms of the oxide and the electrode morphology; (ii) chemical composition and concentration of the electrolyte, and (iii) experimental procedure used to record polarisation curves.

However, considering the experimental conditions used in this work, and the experimental findings reported previously,<sup>1,3</sup> one can in principle exclude contributions due to factors (i) and (iii). Therefore, one can assume the anomalous Tafel behaviour observed in the high overpotential domain (where the *OER/EOP* takes place) is mainly caused by the anion adsorption at the lead dioxide electrode.

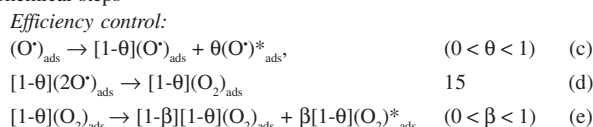
As discussed previously the comparison of findings obtained in different laboratories is rather difficult in the most of cases due to the influence of the procedure used to perform the ohmic drop correction on the Tafel slope.<sup>7</sup> In order to circumvent this inconvenient we used different procedures for ohmic drop correction, which furnished a very good internal consistency for the Tafel slopes obtained via d.c. (conventional polarisation) and a.c. (*EIS*) techniques.

*Electrode mechanism for the OER/EOP processes.* Simultaneous O<sub>2</sub> and O<sub>3</sub> formation at the β-PbO<sub>2</sub> electrode can be represented by next electrode mechanism:<sup>1,3</sup>

Electrochemical steps



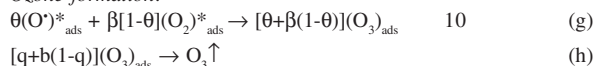
Chemical steps



*Oxygen evolution:*



*Ozone formation:*



where “θ” and “β” are the partial surface coverage describing the competition between *OER* and *EOP* processes while “\*” represents the surface coverage by oxygenated species leading to O<sub>3</sub>-formation.

Experimental *b*-values higher than 120 mV support step (a), known as *primary water discharge*, as rate determining step, r.d.s., of the electrode process, and indicates the effective (apparent) electronic transfer coefficient ( $\alpha_{ap}$ )<sup>1-3,8</sup> is lower than 0.5. Taking into account literature reports,<sup>38,40,41</sup> the concept of the “effective” electronic transfer coefficient can be used to represent the non-ideal behaviour caused,

mainly, by anion adsorption and the non-uniform distribution of the surface electric field on rugged electrodes.

Considering step (a) as r.d., according to Böckris,<sup>42</sup> the reaction rate,  $j$ , is given by next equation:

$$j = k_f[\text{H}_2\text{O}](1-\theta_{\text{OH}\cdot})\exp(\alpha F\eta/RT) - k_b\theta_{\text{OH}\cdot}\exp[-(1-\alpha)F\eta/RT] \quad (8)$$

where  $k_f$  and  $k_b$  are the forward and the backward rate constants,  $\eta(\equiv E - E^0)$  is the overpotential,  $\theta_{\text{OH}\cdot}$  is the surface coverage by the hydroxyl radical, and  $\alpha$  is the electronic transfer coefficient describing the symmetry of the energy barrier for the electron transfer ( $0 < \alpha < 1$ ).<sup>43</sup> In this ideal case  $\alpha$  is an absolute constant. According to Erdey-Gruz and Wick,<sup>44</sup> the special theoretical case where  $\alpha = 0.5$  represents the situation where the energy barrier for the electron transfer lies in the middle of the electric field of the double layer.

Considering negligible the  $\text{OH}^-$ -surface concentration ( $\theta_{\text{OH}\cdot} \rightarrow 0$ ), for conditions of the high field approximation (for  $\eta \geq 0.1\text{V}$ ), equation 8 reduces to next relation:

$$j \cong k_f[\text{H}_2\text{O}]\exp(\alpha F\eta/RT) \quad (9)$$

Taking into account the considerations presented above, equation 9 represents the ideal current-overpotential relation describing the *OER/EOP* processes taking place at inert electrodes. In this ideal case the electron transfer is characterised by a constant  $\alpha$ -value, which represents a constant symmetry of the energy barrier for the whole overpotential domain.<sup>43</sup>

Alternatively, the admittance,  $Y = (\partial j/\partial \eta)_{\eta}$ , related to step (a) can be obtained from equation 9 furnishing next expression:

$$Y = \{k_f[\text{H}_2\text{O}]\alpha F/RT\}\exp(\alpha F\eta/RT) \quad (10)$$

So, considering  $Y = R^{-1}$ , the theoretical expression for the dependence of the resistance due to primary water discharge step,  $R_{\text{pwd}}$ , on overpotential is given by next equation:

$$R_{\text{pwd}} = R_0 \exp\{-\alpha F\eta/RT\} \quad (11)$$

where  $R_0$  ( $\Omega \text{ cm}^2$ ) =  $RT/k_f[\text{H}_2\text{O}]\alpha F$ . Equation 11 is an equivalent form of equation 9 which represents the theoretical resistance ( $R_{\text{pwd}}$ )-overpotential relation describing the electron transfer.

A comparison of equation 11 obtained from the electrode mechanism presented above with the resistive elements present in the EC model (see Figure 1), reveals  $R_{\text{pwd}}$  has the significance of  $R_{\text{ads}}$  (see Figure 4B), thus indicating the adsorption resistance associated with the

hydroxyl radical production (see electrode mechanism, step (a)) governs the *OER* and *OER/EOP* kinetics at the lead dioxide electrode in acid medium.

According to equation 9 (d.c. case) and equation 11 (a.c. case) the theoretically predicted Tafel slope is  $2.302RT/\alpha F$ . So, considering  $T = 24\text{ }^\circ\text{C}$  and  $\alpha = 0.5$ , one has  $b = 120\text{ mV}$ . Confronting experimental  $b$ -values (see Table 3) with the theoretically predicted value of 120 mV, a discrepancy between the theoretical and the experimental Tafel slopes obtained in the high overpotential domain is observed. The ideal case represented by equations 9 and 11, which predicts the electronic transfer coefficient as an absolute constant, is indeed not sustained by several different experimental findings.<sup>1-3,11,33</sup> As already mentioned above, this non-ideal behaviour can be theoretically treated using the concept of the “effective” (apparent) electronic transfer coefficient ( $\alpha_{\text{ap}}$ ).

Considering the high quality of the experimental data (see Figure 5), this behaviour clearly supports the electron transfer process in the high overpotential domain is characterised by  $\alpha_{\text{ap}} < 0.5$ , thus indicating a considerable deviation from the ideal behaviour. These findings indicate the influence of the anion adsorption on the *OER/EOP* kinetics is more pronounced in the high overpotential domain where a stronger interaction between the electrode surface and the anions takes place. In fact, Kokarev *et al.*<sup>34</sup> found that the anion adsorption increases on increasing the electrode potential. This non-ideal behaviour presented by  $b_2$ -values was reported for different electrode processes (e.g. *OER* and *OER/EOP*).<sup>1-3,9,33,45-47</sup>

In the light of the discussion presented above, the deviation from the ideal behaviour presented by the Tafel slope in the high overpotential domain can be mainly attributed to modifications in the double layer properties caused by the anion adsorption. According to Parsons and Böckris,<sup>48</sup> the adsorption of non-active species such as anions at the electrode surface affects the electronic transfer coefficient due to changes suffered by the double layer structure, thus resulting in a non-ideal behaviour for the electron transfer process. A complementary study carried out by different authors<sup>49,50</sup> showed the main factor affecting the electronic transfer coefficient is associated with the effect of the ion penetration in the inner region of the double layer ( $\psi^i$ -effect), which leads to a considerable modification in location of the plane of discharging ions.

#### *Influence of electrolyte composition on EOP current efficiency, $\Phi_{\text{EOP}}$*

Table 4 presents the dependence of *EOP* current efficiency on electrolyte composition at  $0\text{ }^\circ\text{C}$  and  $j = 0.9\text{ A cm}^{-2}$ .

**Table 4.** Dependence of the *EOP* current efficiency on electrolyte composition.  $T = 0\text{ }^{\circ}\text{C}$  and  $j = 0.90\text{ A cm}^{-2}$

Electrolyte <sup>a</sup> [H <sub>2</sub> SO <sub>4</sub> ]:[HClO <sub>4</sub> ]	$\Phi_{\text{EOP}} / (\%)$
0:6	3.5
1:58	2.0
1:22	1.5
1:10	1.3
1:6	1.5
1:4	2.0
1:3	2.2
1:2	2.4
1:1.4	2.4
1:1	2.6
1.5:1	2.6
2.5:1	2.7
5.5:1	2.7
3:0	2.9

<sup>a</sup>[H<sub>2</sub>SO<sub>4</sub>] = 3.0 mol dm<sup>-3</sup>; [HClO<sub>4</sub>] = 6.0 mol dm<sup>-3</sup>.

The  $\Phi_{\text{EOP}}$ -values clearly reveal a dependency of the ozone production on electrolyte composition.  $\Phi_{\text{EOP}}$ -values obtained for pure electrolytes are in good agreement with the literature reports.<sup>1-3,6</sup> From a theoretical point of view,<sup>1-3,8</sup> the minimum observed in the  $\Phi_{\text{EOP}}$ -values for mixed electrolytes indicates the presence of different anions (HSO<sub>4</sub><sup>-</sup>/ClO<sub>4</sub><sup>-</sup>) at the  $\beta$ -PbO<sub>2</sub>/solution interface changes the stability of the adsorbed O<sup>•</sup> intermediate (surface coverage by this intermediate) and/or the degree of hydrophobicity of the electrode/electrolyte interface, resulting in a reduction of the surface concentration of the active centres leading to *EOP*, necessary for the surface process  $\text{O}_{(\text{ads})}^{\bullet} + \text{O}_{2(\text{ads})} \rightarrow (\text{O}_3)_{\text{ads}}$  to take place. This behaviour, contrary to the considerable improvement gained in ozone production by introduction of fluoro-compounds into the base electrolyte<sup>1-3</sup> (e.g. H<sub>2</sub>SO<sub>4</sub>), reveals these mixed electrolytes containing mainly HSO<sub>4</sub><sup>-</sup> and ClO<sub>4</sub><sup>-</sup> anions are not adequate for electrochemical ozone generation at the  $\beta$ -PbO<sub>2</sub> electrode.

## Conclusions

The behaviour of the  $\beta$ -PbO<sub>2</sub>/solution interface and kinetics of the *OER*, in the low and high overpotential domains, was investigated as function of electrolyte composition by means of electrochemical impedance spectroscopy and quasi-stationary polarisation curves. The kinetic study revealed the influence of the electrolyte composition on the *OER* kinetics depends on overpotential domain. The dependence of the adsorption pseudo-capacitance on the electrolyte composition, denounces the presence of the HSO<sub>4</sub><sup>-</sup>/ClO<sub>4</sub><sup>-</sup> anions at the electrode/electrolyte interface reduces the surface coverage by the intermediates leading to the oxygen and oxygen/ozone production.

A comparison of the Tafel slope data obtained for the *OER/EOP* processes in the high overpotential domain from impedance data and quasi-stationary polarisation curves, after ohmic drop correction carried out using different procedures, revealed a very good agreement, thus supporting the experimental findings obtained in these experimental approaches are reliable from the kinetic point of view.

Tafel slope data supported primary water discharge as rate determining step of the overall electrode process leading to *OER/EOP* processes. Tafel slope higher than 120 mV indicates a reduction in the apparent (effective) electronic transfer coefficient in the high overpotential domain. This non-ideal behaviour was attributed mainly to the influence of the anion adsorption on the double layer properties, which is more pronounced at higher overpotentials, where a stronger interaction between the electrode surface and the anions takes place, thus leading to a considerable change in the apparent electronic transfer coefficient.

Current efficiency data for *EOP* is minimum for mixed electrolytes indicating the presence of HSO<sub>4</sub><sup>-</sup>/ClO<sub>4</sub><sup>-</sup> anions at the  $\beta$ -PbO<sub>2</sub>/solution interface leads to a reduction in the surface concentration of the active centres leading to *EOP*. As a result the performance of the electrolyte for this process when compared to pure acid solutions is reduced. These findings support mixtures of sulphuric and perchloric acid are not good as electrolytes for electrochemical ozone production.

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