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# Recent developments of some asymptotic methods and their applications for nonlinear vibration equations in engineering problems: A review

#### Abstract

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This review features a survey of some recent developments in asymptotic techniques and new developments, which are valid not only for weakly nonlinear equations, but also for strongly ones. Further, the achieved approximate analytical solutions are valid for the whole solution domain. The limitations of traditional perturbation methods are illustrated, various modified perturbation techniques are proposed, and some mathematical tools such as variational theory, homotopy technology, and iteration technique are introduced to over-come the shortcomings. In this review we have applied different powerful analytical methods to solve high nonlinear problems in engineering vibrations. Some patterns are given to illustrate the effectiveness and convenience of the methodologies.

#### Keywords

Nonlinear Vibration; Nonlinear Response; Analytical Methods ;Parameter Perturbation Method (PPM) ; Variational Iteration Method(VIM);Homotopy Perturbation Method (HPM); Iteration Perturbation Method (IPM); Energy Balance Method (EBM); Parameter-Expansion Method (PEM) ; Variational Approach (VA);Improved Amplitude Frequency Formulation (IAFF);Max-Min Approach (MMA); Hamiltonian Approach (HA); Homotopy Analysis Method (HAM); Review

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# 38 1 INTRODUCTION

Most of engineering problems, especially some oscillation equations are nonlinear, and in most 39 cases it is difficult to solve such equations, especially analytically. Recently, nonlinear oscillator 40 models have been widely considered in physics and engineering. It is obvious that there are 41 many nonlinear equations in the study of different branches of science which do not have 42 analytical solutions. Due to the limitation of existing exact solutions, many analytical and 43 numerical approaches have been investigated. Therefore, these nonlinear equations must be 44 solved using other methods. Many researchers have been working on various analytical methods 45 for solving nonlinear oscillation systems in the last decades. Perturbation technique is one the 46 well- known methods [3, 11, 34, 37, 39, 85], the traditional perturbation method contains 47 many shortcomings. They are not useful for strongly nonlinear equations, so for overcoming 48 the shortcomings, many new techniques have been appeared in open literatures. 49

It should be mentioned that several books appeared on the subject of mathematical methods in engineering problem during the past decade [10, 48, 54, 77, 113, 125, 133, 137, 144– 146, 180, 186, 187].

The aim of this article is to review the recent research on the approximate analytical 53 methods for nonlinear vibrations. The applications of these methods have been appeared in 54 open literatures in the last three years. There are hundreds of published papers too numerous to 55 refer to all of them, but for the purpose of filling the gaps in the present summary, Refs[14, 15, 56 28, 30, 36, 40, 47, 55, 66, 75, 76, 83, 88, 89, 94, 142, 166, 170, 173, 178, 192, 193, 210, 217]may 57 offer good help in overcoming the inevitable shortcomings in a condensed presentation. To 58 show the efficiency and accuracy of the methods some comparisons have done with the results 59 obtained by those methods and numerical methods and they are valid for whole domain. Some 60 of the ideas first appeared in this review article, and most cited references were published in 61 the last three years, revealing the most emerging research fronts. In this review, the basic 62 idea of each method is presented then some examples are illustrated and discussed to show the 63 application of these methods. 64

# 65 2 PARAMETERIZED PERTURBATION METHOD (PPM)

Recently, nonlinear oscillator models have been widely considered in physics and engineering. 66 Study of nonlinear problems which are arisen in many areas of physics and also engineering 67 is very significant for scientists. Surveys of the literature with numerous references have been 68 given by many authors utilizing various analytical methods for solving nonlinear oscillation 69 systems. Non-linear problems continue to be as a challenge, and heed has mainly concentrated 70 on qualitative changes of systems bifurcations and instability. Parameterized Perturbation 71 Method (PPM) is one of the well-known methods for solving nonlinear vibration equations. 72 The method was proposed in by He in 1999 [80]. It was rarely used recently, but this method is 73 a kind of powerful tool for treating weakly nonlinear problems, but they are less effective for 74 analyzing strongly nonlinear problems [37, 50, 86, 92, 115, 160]. 75

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#### 76 2.1 Basic idea of Parameterized Perturbation Method

For the nonlinear equation L(u) + N(u) = 0, where L and N are general linear and nonlinear differential operators respectively, a linear transformation can be introduced as:

$$u = \varepsilon \nu \tag{2.1}$$

We can assume that  $\nu$  can be written as a power series in  $\varepsilon$ , as following

$$\nu = \nu_0 + \varepsilon \nu_1 + \varepsilon^2 \nu_2 + \dots, \tag{2.2}$$

80 And

$$\nu = \lim_{\varepsilon \to 1} \nu = \nu_0 + \nu_1 + \nu_2 + \nu_3 + \dots$$
(2.3)

# 81 2.2 Application of Parameterized Perturbation Method

<sup>82</sup> Two examples have considered showing the applicability of this method.

84 Example 1

83

<sup>85</sup> Consider the following Duffing equation:

$$\ddot{u} + \alpha u + \beta u^3 = 0, \qquad u(0) = A, \ \dot{u}(0) = 0$$
 (2.4)

We let  $u = \varepsilon \nu$  in Eq. (2.4) and obtain

$$\ddot{\nu} + \alpha \nu + \varepsilon^2 \beta \nu^3 = 0, \quad \nu(0) = A/\varepsilon, \ \dot{\nu}(0) = 0 \tag{2.5}$$

Supposing that the solution of Eq. (2.5) and  $\omega^2$  can be expressed in the form

$$\nu = \nu_0 + \varepsilon^2 \nu_1 + \varepsilon^4 \nu_2 + \varepsilon^6 \nu_3 \tag{2.6}$$

$$\alpha = \omega^2 + \varepsilon^2 \omega_1 + \varepsilon^4 \omega_2 + \varepsilon^6 \omega_3 \tag{2.7}$$

Substituting Eqs. (2.6) and (2.7) into Eq. (2.5) and equating coefficients of like powers of  $\varepsilon$  yields the following equations

$$\ddot{\nu}_0 + \omega^2 \nu_0 = 0,$$
  $\nu_0(0) = A/\varepsilon$ ,  $\dot{\nu}_0(0) = 0,$  (2.8)

 $\ddot{\nu}_1 + \omega^2 \nu_1 + \omega_1 \nu_0 + \beta \nu_0^3 = 0 , \qquad \nu_1(0) = 0 , \, \dot{\nu}_1(0) = 0$ (2.9)

Solving Eq. (2.8) results in

$$\nu_0 = \frac{A}{\varepsilon} \cos \omega t \tag{2.10}$$

Equation (2.9), therefore, can be re-written down as

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$$\ddot{\nu}_1 + \omega^2 \nu_1 + \left(\omega_1 + \frac{3\beta A^2}{4\varepsilon^2}\right) \frac{A}{\varepsilon} \cos\left(\omega t\right) + \frac{\beta A^3}{4\varepsilon^3} \cos\left(3\omega t\right) = 0.$$
(2.11)

Avoiding the presence of a secular terms needs:

$$\omega_1 = -\frac{3\beta A^2}{4\varepsilon^2} \tag{2.12}$$

Substituting Eq. (2.12) into Eq. (2.7)

$$\omega_{PPM} = \sqrt{\alpha + \frac{3}{4}\beta A^2} \tag{2.13}$$

Solving Eq. (2.11), gives:

$$\nu_1 = -\frac{A^3\beta}{32\omega^2\varepsilon^3} \left(\cos\left(\omega t\right) - \cos\left(3\omega t\right)\right) \tag{2.14}$$

<sup>96</sup> Its first-order approximation is sufficient, and then we have:

$$u = \varepsilon \nu = \varepsilon (\nu_0 + \varepsilon^2 \nu_1) = A \cos(\omega t) - \frac{A^3 \beta}{32\omega^2 \varepsilon^3} \left[ \cos(\omega t) - \cos(3\omega t) \right]$$
(2.15)

<sup>97</sup> The exact frequency of this problem is:

$$\omega_{Exact} = 2\pi \left/ 4\sqrt{2} \int_0^{\pi/2} \frac{dt}{\sqrt{\beta A^2 \cos^2(t) + \beta A^2 + 2\alpha}} \right.$$
(2.16)

Table 2.1 Comparison of the approximate frequencies with the exact period.

Α	$\alpha$	β	Present Study	Exact	Error %
			(PPM)	Solution	$\left(\omega_{PPM}-\omega_{ex} ight)/\omega_{ex}$
0.1	0.5	0.1	0.7076	0.7076	0.0000
0.5	0.1	2	0.6892	0.6800	1.3501
1	2	0.5	1.5411	1.5403	0.0520
2	5	2	3.3166	3.2958	0.6313
5	2	5	9.7852	9.5818	2.1228
10	1	0.5	6.2048	6.0772	2.0994
15	0.5	2	18.3848	17.9866	2.2135
20	5	1	17.4642	17.0977	2.1436

The maximum relative error is less than 2.2135% for this example.

#### 98

# 99 Example 2

100 We consider the following nonlinear oscillator [89];

$$(1+u^2)\ddot{u}+u=0, \ u(0)=A, \dot{u}(0)=0.$$
 (2.17)

We let  $u = \varepsilon \nu$  in Eq. (2.17) and obtain

$$\ddot{\nu} + 1.\nu + \varepsilon^2 \nu^2 \ddot{\nu} = 0, \quad \nu(0) = \frac{A}{\varepsilon}, \ \dot{\nu}(0) = 0.$$
 (2.18)

Supposing that the solution of Eq. (2.18) and  $\omega^2$  can be expressed in the form

$$\nu = \nu_0 + \varepsilon^2 \nu_1 + \varepsilon^4 \nu_2 + \dots$$
 (2.19)

$$1 = \omega^2 + \varepsilon^2 \omega_1 + \varepsilon^4 \omega_2 + \dots \tag{2.20}$$

<sup>103</sup> Substituting Eqs. (2.19) and (2.20) into Eq. (2.18) and equating coefficients of like powers <sup>104</sup> of  $\varepsilon$  yields the following equations

$$\ddot{\nu}_0 + \omega^2 \nu_0 = 0,$$
  $\nu_0(0) = \frac{A}{\varepsilon}, \ \dot{\nu}_0(0) = 0,$  (2.21)

105

$$\ddot{\nu}_1 + \omega^2 \nu_1 + \omega_1 \nu_0 + \nu_0^2 \ddot{\nu}_0 = 0 , \quad \nu_1(0) = 0 , \\ \dot{\nu}_1(0) = 0.$$
(2.22)

Solving Eq. (2.21) results in

$$\nu_0 = \frac{A}{\varepsilon} \cos \omega t \tag{2.23}$$

Equation (2.22), therefore, can be re-written down as

$$\nu_1'' + \omega^2 \nu_1 + \frac{\omega_1 A}{\varepsilon} \cos \omega t - \frac{\omega^2 A^3}{\varepsilon^3} \cos^3 \omega t = 0$$
(2.24)

108 Or

$$\nu_1'' + \omega^2 \nu_1 + \left(\frac{\omega_1 A}{\varepsilon} - \frac{3\omega^2 A^3}{4\varepsilon^3}\right) \cos 3\omega t = 0.$$
(2.25)

109 We let

$$\omega_1 = \frac{3\omega^2 A^2}{4\varepsilon^2} \tag{2.26}$$

In Eq. (2.25) so that the secular term can be eliminated. Solving Eq. (2.25) yields;

$$\nu_1 = \frac{A^3}{32\varepsilon^3} (\cos\omega t - \cos 3\omega t) \tag{2.27}$$

<sup>111</sup> Thus we obtain the first-order approximate solution of the original Eq. (2.17), which reads

$$u = \varepsilon (\nu_0 + \varepsilon^2 \nu_1) = A \cos \omega t - \frac{A^3}{32} (\cos \omega t - \cos 3\omega t)$$
(2.28)

Substituting Eq. (2.26) into Eq. (2.20) results in

$$1 = \omega^2 + \varepsilon^2 \omega_1 = \omega^2 + \frac{3\omega^2 A^2}{4}$$
(2.29)

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<sup>113</sup> Then we have;

$$\omega_{PPM} = \frac{1}{\sqrt{1 + \frac{3}{4}A^2}}$$
(2.30)

Eq. (2.30) gives the same frequency as that resulting from the artificial parameter Linstedt– Poincare method [89].

# 116 3 VARIATIONAL ITERATION METHOD (VIM)

Nonlinear phenomena play a crucial role in applied mechanics and physics. By solving nonlin-117 ear equations we can guide authors to know the described process deeply. But it is difficult for 118 us to obtain the exact solution for these problems. In recent decades, there has been great devel-119 opment in the numerical analysis and exact solution for nonlinear partial equations. There are 120 many standard methods for solving nonlinear partial differential equations. The variational it-121 eration method was first proposed by He [82] used to obtain an approximate analytical solutions 122 for nonlinear problems. In VIM in most cases only one iteration leads to high accuracy of the 123 solution and it doesn't need any linearization or discretization, and large computational work. 124 The VIM is useful to obtain exact and approximate solutions of linear and nonlinear differen-125 tial equations [35, 57, 62, 99, 104, 117, 122, 136, 139, 153, 167, 177, 179, 184, 191, 202, 206]. We 126 have considered three examples to show the implement of the VIM. 127

# 128 3.1 Basic idea of Variational Iteration Method

To illustrate its basic concepts of the new technique, we consider following general differentialequation[82]:

$$Lu + Nu = g(x) \tag{3.1}$$

Where, L is a linear operator, and N a nonlinear operator, g(x) an inhomogeneous or forcing term. According to the variational iteration method, we can construct a correct functional as follows:

$$u_{(n+1)}(t) = u_n(t) + \int_0^t \lambda \{ L u_n(\tau) + N \tilde{u}_n(\tau) - g(\tau) \} d\tau$$
(3.2)

<sup>134</sup> Where  $\lambda$  is a general Lagrange multiplier, which can be identified optimally via the varia-<sup>135</sup> tional theory, the subscript *n* denotes the nth approximation,  $\tilde{u}_n$  is considered as a restricted <sup>136</sup> variation, i.e.  $\tilde{} = 0 n \delta u$ .

For linear problems, its exact solution can be obtained by only one iteration step due to the fact that the Lagrange multiplier can be exactly identified.

#### 139 3.2 Application of Variational Iteration Method

#### 140 Example 1

The equation of motion of a mass attached to the center of a stretched elastic wire in dimensionless is[181]:

$$\ddot{u} + u - \frac{\eta u}{\sqrt{1+u^2}} = 0$$
,  $0 < \lambda \le 1$  (3.3)

143 With initial conditions

$$u(0) = A , \dot{u}(0) = 0$$
 (3.4)

Assume that the angular frequency of the system (3.3) is  $\omega$ , we have the following linearized equation:

$$\ddot{u} + \omega^2 u = 0 \tag{3.5}$$

146 So we can rewrite Eq. (3.3) in the form

$$\ddot{u} + \omega^2 u + g(u) = 0 \tag{3.6}$$

147 Where 
$$g(u) = (1 - \omega^2)u - \frac{\eta u}{\sqrt{1 + u^2}}$$

Applying the variational iteration method, we can construct the following functional equation:

$$u_{n+1}(t) = u_n(t) + \int_0^t \lambda(\ddot{u}(\tau) + \omega^2 u_n(\tau) - g(\tau)) d\tau$$
(3.7)

150 Where  $\tilde{g}$  is considered as a restricted variation, i.e.,  $\delta \tilde{g} = 0$ .

<sup>151</sup> Calculating variation with the respect to  $u_n$  and nothing that  $\delta \tilde{g}(u_n) = 0$ . We have the <sup>152</sup> following stationary conditions:

$$\lambda'' + \omega^2 \lambda(\tau) = 0,$$
  

$$\lambda(\tau)|_{\tau=t} = 0,$$
  

$$1 - \lambda'(\tau)|_{\tau=t} = 0.$$
  
(3.8)

<sup>153</sup> The Lagrange multiplier, therefore, can be identified as;

$$\lambda = \frac{1}{\omega} \sin \omega (\tau - t) \tag{3.9}$$

Substituting the identified multiplier into Eq.(3.7) results in the following iteration formula:

$$u_{n+1}(t) = u_n(t) + \frac{1}{\omega} \int_0^t \sin \omega(\tau - t) \times \left( \ddot{u}(\tau) + u(\tau) - \frac{\eta u(\tau)}{\sqrt{1 + u^2(\tau)}} \right) d\tau$$
(3.10)

Assuming its initial approximate solution has the form

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$$u_0 = A\cos(\omega t) \tag{3.11}$$

And substituting Eq. (3.11) into Eq. (3.3) leads to the following residual:

$$R_0(t) = -A\omega^2 \cos(\omega t) + A\cos(\omega t) - \left(\frac{A\eta}{\sqrt{1+A^2}} + \frac{1}{2}\frac{A^3\eta\omega^2 t^2}{(1+A^2)} + O(t^3)\right)\cos(\omega t).$$
(3.12)

By the formulation (3.10), we can obtain

$$u_1(t) = A\cos(\omega t) + \int_0^t \frac{1}{\omega} \sin \omega (\tau - t) R_0(\tau) d\tau., \qquad (3.13)$$

In order to ensure that no secular terms appear in  $u_1$ , resonance must be avoided. To do so, the coefficient of  $\cos(\omega t)$  in Eq. (3.12) requires being zero, i.e.,

$$\omega_{VIM} = \frac{\sqrt{1 + A^2 - \sqrt{1 + A^2}\eta}}{\sqrt{1 + A^2}} \tag{3.14}$$

160 And period of oscillation for this system by variational iteration method is;

$$T_{VIM} = \frac{2\pi\sqrt{1+A^2}}{\sqrt{1+A^2}-\sqrt{1+A^2}\eta}$$
(3.15)

Table 3.1 Comparison of the approximate periods with the exact period[1].

Α	$\eta$	T $_{VIM}$	$T_{exact}[181]$	Error %
0.1	0.1	6.621237	6.62168	0.00669
1	0.1	6.517854	6.537508	0.300634
10	0.1	6.314678	6.322938	0.130635
0.1	0.5	8.863794	8.869257	0.061595
1	0.5	7.814722	7.992133	2.21982
10	0.5	6.445572	6.490208	0.687744
0.1	0.75	12.47385	12.49673	0.183088
1	0.75	9.168186	9.625404	4.750118
10	0.75	6.531632	6.602092	1.067237

Table 3.1 shows an excellent agreement of the VIM with the exact one.

161

162 Example 2

<sup>163</sup> For the second example, we consider Duffing equation:

$$\ddot{u} + u + \varepsilon u^3 = 0 \tag{3.16}$$

164 With initial conditions

$$u(0) = A , \dot{u}(0) = 0$$
 (3.17)

Assume that the angular frequency of the Eq.(3.16) is  $\omega$ , we have the following linearized equation:

$$\ddot{u} + \omega^2 u = 0 \tag{3.18}$$

167 So we can rewrite Eq. (3.16) in the form

$$\ddot{u} + \omega^2 u + g(u) = 0 \tag{3.19}$$

168 Where  $g(u) = u + \varepsilon u^3 - \omega^2 u$ .

Applying the variational iteration method, we can construct the following functional equation:

$$u_{n+1}(t) = u_n(t) + \int_0^t \lambda(\ddot{u}(\tau) + \omega^2 u_n(\tau) - g(\tau)) d\tau$$
 (3.20)

Where  $\tilde{g}$  is considered as a restricted variation, i.e.,  $\delta \tilde{g} = 0$ .

Calculating variation with the respect to  $u_n$  and nothing that  $\delta \tilde{g}(u_n) = 0$ . We have the following stationary conditions:

$$\lambda'' + \omega^2 \lambda(\tau) = 0, \lambda(\tau)|_{\tau=t} = 0, 1 - \lambda'(\tau)|_{\tau=t} = 0.$$
(3.21)

<sup>174</sup> The Lagrange multiplier, therefore, can be identified as;

$$\lambda = \frac{1}{\omega} \sin \omega (\tau - t) \tag{3.22}$$

Substituting the identified multiplier into Eq.(3.20) results in the following iteration formula:

$$u_{n+1}(t) = u_n(t) + \frac{1}{\omega} \int_0^t \sin \omega(\tau - t) \times \left( \ddot{u}_n(\tau) + u_n(\tau) + \varepsilon u_n^3(\tau) \right) d\tau$$
(3.23)

Assuming its initial approximate solution has the form

$$u_0 = A\cos(\omega t) \tag{3.24}$$

And substituting Eq. (3.24) into Eq. (3.16) leads to the following residual:

$$R_0(t) = \left(1 - \omega^2 + \frac{3}{4}\varepsilon A^2\right)A\cos\left(\omega t\right) + \frac{1}{4}\varepsilon A^3\cos\left(3\omega t\right).$$
(3.25)

By the formulation (3.23), we can obtain

$$u_1(t) = A\cos(\omega t) + \int_0^t \frac{1}{\omega} \sin \omega(\tau - t) R_0(\tau) d\tau., \qquad (3.26)$$

To avoid secular terms appear in  $u_{1,t}$  the coefficient of  $\cos(\omega t)$  in Eq. (3.25) requires being zero, i.e.

$$\omega_{VIM} = \sqrt{1 + \frac{3}{4}\varepsilon A^2} \tag{3.27}$$

182 And period of this system is ;

$$T_{VIM} = \frac{2\pi}{\sqrt{1 + (3/4)\,\varepsilon A^2}} \tag{3.28}$$

<sup>183</sup> The exact solution is[89]:

$$T_{Exact} = \frac{4}{\sqrt{1 + \varepsilon A^2}} \int_0^{\pi/2} \frac{dt}{\sqrt{1 - k \sin^2 t}}$$
(3.29)

184 Where  $k = 0.5\varepsilon A^2 / (1 + \varepsilon A^2)$ .

# 186 Example 3

185

The governing equation of Mathieu-Duffing system which is considered in this study is described by the following high-order nonlinear differential equation[45];

$$\ddot{u} + \left[\delta + 2\varepsilon \cos(2t)\right]u - \phi u^3 = 0 \tag{3.30}$$

Where dots indicate differentiation with respect to the time (t),  $\varepsilon <<1$  is a small parameter,  $\phi$ is the Parameter of nonlinearity and  $\delta$  is the transient curve and can be defined as [45];

$$\delta = \phi u_0^2 (1 - \frac{2\varepsilon}{2 + \phi u_0^2}). \tag{3.31}$$

<sup>191</sup> The initial condition considered in this study is defined by [45];

$$u(0) = 0.1, \dot{u}(0) = 0 \tag{3.32}$$

According to the VIM, we can construct the correction functional of Eq. (3.30) as follows

$$u_{(n+1)}(t) = u_n(t) + \int_0^\tau \lambda \{ \ddot{u}_n + [\delta + 2\varepsilon \cos(2\tau)] u_n - \phi u_n^3 \} d\tau$$
(3.33)

<sup>193</sup> Where  $\lambda$  is General Lagrange multiplier.

Making the above correction functional stationary, we can obtain following stationary con ditions

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$$\lambda''(\tau) = 0,$$
  

$$\lambda(\tau)_{\tau=t} = 0,$$
(3.34)  

$$1 - \lambda'(\tau) \mid_{\tau=t} = 0,$$

<sup>196</sup> The Lagrange multiplier, can be identified as:

$$\lambda = \tau - t \tag{3.35}$$

<sup>197</sup> Leading to the following iteration formula

$$u_{(n+1)}(t) = u_n(t) + \int_0^t (\tau - t) \{ \ddot{u}_n + [\delta + 2\varepsilon \cos(2t)] u_n - \phi u_n^3 \} d\tau$$
(3.36)

If, for example, the initial conditions are u(0) = 0.1 and  $\dot{u}(0) = 0$ , we began with  $u_0(t) = 0.1$ , by the above iteration formula (3.33) we have the following approximate solutions

$$u_1(t) = 0.1 - 0.05\varepsilon - 0.05\delta t^2 + 0.05\varepsilon cos(2t) + 0.0005\phi t^2$$
(3.37)

In the same way, we obtain as  $u_2$  (t)follows:

$$\begin{split} u_{2}(t) &= 0.1 - 0.05\varepsilon - 0.05\delta t^{2} + 0.05\varepsilon cos(2t) + 0.0005\phi t^{2} + 0.1875\varepsilon^{2} - 0.328125 \times 10^{-3}\phi\varepsilon^{2} \\ &+ 0.2724609375 \times 10^{-5}\phi^{2}\varepsilon^{2} - 0.5625 \times 10^{-5}\varepsilon\phi^{2} + 0.9461805556 \times 10^{-4}\varepsilon\phi^{3} \\ &+ 6.696428 \times 10^{-8}\delta^{2}\phi^{2}t^{8} + 1.171875 \times 10^{-7}\varepsilon^{2}\phi^{2}t^{2} + 0.125 \times 10^{-5}\phi^{2}t^{4} + 3.75 \times 10^{-8}t^{3}\varepsilon\phi^{3}sin(2t) \\ &+ 0.140625 \times 10^{-4}\varepsilon\delta\phi^{2}cos(2t) + 8.4375 \times 10^{-8}t^{2}\varepsilon\phi^{3}cos(2t) + 0.1875 \times 10^{-5}t^{2}\varepsilon^{2}\phi^{2}cos(2t) \\ &- 0.375 \times 10^{-5}t\varepsilon^{2}\phi^{2}sin(2t) + 0.00025t^{2}\phi\varepsilon cos(2t) - 0.375 \times 10^{-5}\varepsilon\phi^{2}cos(2t)t^{2} \\ &- 2.34375 \times 10^{-7}\varepsilon^{2}\phi^{2}cos^{2}(2t)t^{2} - 0.87890625 \times 10^{-5}\phi\varepsilon^{2}\delta cos(2t)^{2} - 0.025t^{2}\delta\varepsilon cos(2t) \\ &+ 0.00028125\phi\varepsilon^{2}\delta cos(2t) - 0.000703125\phi\varepsilon\delta^{2}cos(2t) - 0.0005625\phi\varepsilon\delta cos(2t) \\ &- 0.140625 \times 10^{-4}\varepsilon\delta\phi^{2} + 0.05t\delta\varepsilon sin(2t) - 0.5 \times 10^{-3}t\phi\varepsilon sin(2t) + 0.75 \times 10^{-5}\varepsilon\phi^{2}sin(2t)t \\ &- 1.125 \times 10^{-7}t\varepsilon\phi^{3}sin(2t) - 9.375 \times 10^{-9}t^{4}\varepsilon\phi^{3}cos(2t) + 0.5625 \times 10^{-3}\phi\varepsilon\delta + 0.70312 \times 10^{-3}\phi\varepsilon\delta^{2} \\ &- 0.2724609375 \times 10^{-3}\phi\varepsilon^{2}\delta - 0.05\delta\varepsilon + 0.00075\phi\varepsilon + 7.03125 \times 10^{-8}\varepsilon\phi^{3} + 4.6875 \times 10^{-7}\varepsilon^{2}\phi^{2}t^{4} \\ &+ 0.9461805556 \times 10^{-4}\phi\varepsilon^{3} - 0.5625 \times 10^{-5}\varepsilon\phi^{2} - 0.46875 \times 10^{-4}\phi\varepsilon^{2}\delta t^{4} + 0.000125\phi\varepsilon\delta t^{4} \\ &- 0.125 \times 10^{-4}t^{6}\phi\delta^{2}\varepsilon + 2.5 \times 10^{-9}\phi^{3}t^{6} + 0.2724609375 \times 10^{-5}\varepsilon^{2}\phi^{2} - 0.328125 \times 10^{-3}\phi\varepsilon^{2} \\ &+ 0.1875 \times 10^{-5}t^{4}\delta\varepsilon\phi^{2}cos(2t) + 2.23214285710^{-12}\phi^{4}t^{8} - 7.03125 \times 10^{-8}\varepsilon\phi^{3}cos(2t) \\ &- 0.28125 \times 10^{-5}\varepsilon^{2}\phi^{2}cos(2t) - 0.75 \times 10^{-3}\phi\varepsilon cos(2t) + 0.375 \times 10^{-3}\phi\varepsilon^{2}cos(2t) \\ &- 0.46875 \times 10^{-4}\phi\varepsilon^{2}cos^{2}(2t) - 0.34722222 \times 10^{-5}\phi\varepsilon^{3}cos^{3}(2t) + 0.5625 \times 10^{-5}\varepsilon\phi^{2}cos(2t) + ... \\ &(3.38) \end{aligned}$$

And so on. In the same manner, the rest of the components of the iteration formula can be obtained.

Figures 3.1 to 3.3 indicate that the VIM experiences a high accuracy. The figures illustrate the time history diagram of the displacement, velocity and phase plan, respectively.

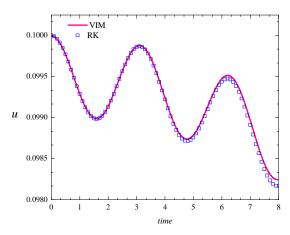


Figure 3.1 Comparison of time history diagram of displacements between VIM and RK solutions at  $\varphi = 2, \varepsilon = 0.01, u(0) = 0.1, \dot{u}(0) = 0.$ 

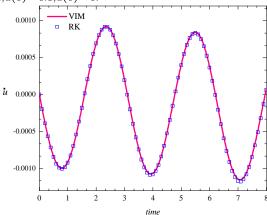


Figure 3.2 Comparison of time history diagram of velocity between VIM and RK solutions at  $\varphi = 2, \varepsilon = 0.01, u(0) = 0.1, \dot{u}(0) = 0.$ 

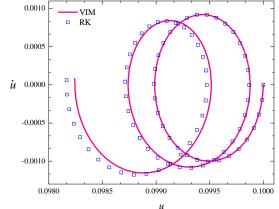


Figure 3.3 Comparison of VIM with RK ,  $\dot{u} {\rm versus}~u {\rm at} \phi {\rm =}$  2,  $\varepsilon$  =  $0.01,~\delta$  = 0.02

#### 205 4 HOMOTOPY PERTURBATION METHOD (HPM)

Until recently, the application of the homotopy perturbation method in nonlinear problems 206 has been devoted by scientists and engineers, because this method is to continuously deform a 207 simple problem easy to solve into the difficult problem under study. The homotopy perturba-208 tion method proposed by He in 1999[81]. Elementary introduction and interpretation of the 209 method are given in the following publications [5, 9, 24, 27–33, 59, 63, 64, 68, 84, 91, 93, 95, 210 96, 98, 101, 102, 123, 148, 168, 174, 176, 208, 218]. HPM can solve a large class of nonlinear 211 problems with approximations converging rapidly to accurate solutions. This method is the 212 most effective and convenient one for both weakly and strongly nonlinear equations. 213

#### 214 4.1 Basic idea of Homotopy Perturbation Method

To explain the basic idea of the HPM for solving nonlinear differential equations, one may consider the following nonlinear differential equation[81]:

$$A(u) - f(r) = 0 \ r \in \Omega \tag{4.1}$$

<sup>217</sup> That is subjected to the following boundary condition:

$$B\left(u,\frac{\partial u}{\partial t}\right) = 0 \ r \in \Gamma \tag{4.2}$$

<sup>218</sup> Where A is a general differential operator, B a boundary operator, f(r) is a known analyt-<sup>219</sup> ical function,  $\Gamma$  is the boundary of the solution domain( $\Omega$ ), and  $\partial u/\partial t$  denotes differentiation <sup>220</sup> along the outwards normal to  $\Gamma$ . Generally, the operator A may be divided into two parts: a <sup>221</sup> linear part L and a nonlinear part N. Therefore, Eq. (4.1) may be rewritten as follows:

$$L(x) + N(x) - f(r) = 0 \ r \in \Omega$$

$$(4.3)$$

In cases where the nonlinear Eq. (4.1) includes no small parameter, one may construct the following homotopy equation

$$H(\nu, p) = (1 - p) [L(\nu) - L(u_0)] + p[A(\nu) - f(r)] = 0$$
(4.4)

224 Where

$$\nu(r,p): \ \Omega \times [0,1] \to R \tag{4.5}$$

In Eq. (4.4),  $p \in [0, 1]$  is an embedding parameter and  $u_0$  is the first approximation that satisfies the boundary condition. One may assume that solution of Eq. (4.4) may be written as a power series in p, as the following:

$$\nu = \nu_0 + p\nu_1 + p^2\nu_2 + \cdots \tag{4.6}$$

The homotopy parameter p is also used to expand the square of the unknown angular frequency u as follows:

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$$\omega_0 = \omega^2 - p\omega_1 - p^2\omega_2 - \dots \tag{4.7}$$

230 Or

$$\omega^2 = \omega_0 + p\omega_1 + p^2\omega_2 + \dots \tag{4.8}$$

<sup>231</sup> Where  $\omega_0$  is the coefficient of u(r) in Eq. (4.1) and should be substituted by the right hand <sup>232</sup> side of Eq. (4.8). Besides,  $\omega_i$  (i = 1, 2, ...) are arbitrary parameters that have to be determined. <sup>233</sup> The best approximations for the solution and the angular frequency  $\omega$  are

$$u = \lim_{p \to 1} \nu = \nu_0 + \nu_1 + \nu_2 + \dots \tag{4.9}$$

$$\omega^2 = \omega_0 + \omega_1 + \omega_2 + \dots \tag{4.10}$$

When Eq. (4.4) corresponds to Eq. (4.1) and Eq. (4.9) becomes the approximate solution of Eq. (4.1)

#### 236 4.2 Application of Homotopy Perturbation Method

#### 237 Example 1.

We consider the mathematical pendulum. When friction is neglected; the differential equation governing the free oscillation of the mathematical pendulum is given by [82];

$$\theta + \Omega^2 \sin \theta = 0, \quad \theta(0) = A, \quad \theta(0) = 0$$

$$(4.11)$$

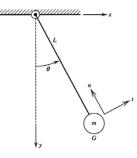


When  $\theta$  designates the deviation angle from the vertical equilibrium position,  $\Omega^2 = \frac{g}{l}$  where g is the gravitational acceleration, l the length of the pendulum[82].

In order to apply the homotopy perturbation method to solve the above problem, the approximation  $\sin \theta \approx \theta - (1/6) \theta^3 + (1/120) \theta^5$  is used

Now we apply homotopy perturbation to Eq. (4.11). We construct a homotopy in the following form:

$$H(\theta, p) = (1 - p) \left[ \ddot{\theta} + \Omega^2 \theta \right] + p \left[ \ddot{\theta} + \Omega^2 \left( \theta - (1/6) \theta^3 + (1/120) \theta^5 \right) \right] = 0$$
(4.12)



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According to HPM, we assume that the solution of Eq. (4.12) can be expressed in a series 247 of p;

$$\theta(t) = \theta_0(t) + p\theta_1(t) + p^2\theta_2(t) + \dots$$
(4.13)

Just the coefficient of  $\theta_{1}(\Omega^{2})$  expanded into a series in p in a similar way:

$$\Omega^2 = \omega^2 - p\omega_1 - p^2\omega_2 + \dots \tag{4.14}$$

Substituting Eq.(4.13) and Eq. (4.14) into Eq. (4.12) after some simplification and substitution and rearranging based on powers of *p*-terms, we have:

$$p^{0}: \ddot{\theta}_{0} + \omega^{2}\theta_{0} = 0, \qquad \theta_{0}(0) = A, \quad \dot{\theta}_{0}(0) = 0$$
 (4.15)

$$p^{1}: \quad \ddot{\theta}_{1} + \omega^{2}\theta_{1} = \omega_{1}\theta + (\frac{\Omega^{2}}{6})\omega^{2}\theta^{3} - (\frac{\Omega^{2}}{120})\omega^{2}\theta^{5}, \qquad \theta_{1}(0) = 0, \quad \dot{\theta}_{1}(0) = 0$$
(4.16)

<sup>251</sup> Considering the initial conditions  $\theta_0(0) = A$  and  $\dot{\theta}_0(0) = 0$  the solution of Eq. (4.15) is <sup>252</sup>  $\theta_0 = A \cos \omega t$  Substituting the result into Eq. (4.16), we have:

.

$$p^{1}: \quad \ddot{\theta}_{1} + \omega^{2}\theta_{1} = \omega_{1}A\cos(\omega t) + \frac{1}{6}\omega^{2}A^{3}\cos^{3}(\omega t) - \frac{1}{120}\omega^{2}A^{5}\cos^{5}(\omega t)$$
(4.17)

<sup>253</sup> For achieving the secular term, we use Fourier expansion series as follows:

$$\Phi(\omega, t) = \left(-\frac{1}{8}\omega^2 A^3 + \frac{1}{192}\omega^2 A^5 - \omega_1 A\right)\cos(\omega t) - \frac{1}{24}\omega^2 A^3\cos(3\omega t) + \frac{1}{1920}\omega^2 A^5\cos(5\omega t) + \frac{1}{384}\omega^2 A^5\cos(3\omega t) = \sum_{n=0}^{\infty} b_{2n+1}\cos\left[(2n+1)\omega t\right] = b_1\cos(\omega t) + b_3\cos(3\omega t) + \dots$$
(4.18)

Substituting Eq. (4.18) into right hand of Eq. (4.17) yields:

$$p^{1}: \quad \ddot{\theta}_{1} + \omega^{2} \theta_{1} = \left[ -(1/8)\omega^{2}A^{3} + (1/192)\omega^{2}A^{5} - \omega_{1}A \right] \cos(\omega t) + \sum_{n=0}^{\infty} b_{2n+1} \cos\left[ (2n+1)\omega t \right] \quad (4.19)$$

Avoiding secular term, gives:

$$\omega_1 = -\frac{1}{192}\omega^2 A^2 (-24 + A^2) \tag{4.20}$$

From Eq. (4.14) and setting p = 1, we have:

$$\Omega^2 = \omega^2 - \omega_1 \tag{4.21}$$

 $_{257}$  Comparing Eqs. (4.20) and (4.21), we can obtain:

$$\omega = \Omega \sqrt{1 - \frac{1}{8}A^2 + \frac{1}{192}A^4} \tag{4.22}$$

#### <sup>258</sup> The exact frequency of this problem is:

$$\omega_{Exact} = 2\pi \bigg/ 2\sqrt{2} \int_0^{\pi/2} \frac{A\sin^2(t) dt}{\Omega\sqrt{\cos\left(A\cos(t)\right) - \cos(A)}}$$
(4.23)

Table 4.1 Comparison of the approximate frequencies with the exact period.

			<b>D</b>	E Ø
Α	52	Present Study	Exact	Error $\%$
		$(\mathrm{HPM})$	Solution	$\left(\omega_{HPM}-\omega_{ex} ight)/\omega_{ex}$
0.1	2	1.99875	1.99875	0.0000
0.2	3	2.992503	2.992502	0.0001
0.5	4	3.937665	3.937579	0.0022
0.8	2	1.920555	1.92025	0.0159
1	1	0.938194	0.937792	0.0429
1.2	2	1.822965	1.821145	0.0999
1.5	1	0.863202	0.860608	0.3013
1.8	0.5	0.403012	0.399787	0.8066
2	1	0.763763	0.7525	1.4968

259

#### 260 Example 2

The motion of a particle on a rotating parabola is considered for second example. The governing equation of motion and can be expressed as;

$$\ddot{u} + a\,u\dot{u}^2 + a\,u\ddot{u} + \alpha_1 u + \alpha_2 u^3 + \alpha_3 u^5 = 0, \qquad u(0) = A, \qquad \dot{u}(0) = 0 \qquad (4.24)$$

Now we apply homotopy-perturbation to Eq(4.24). We construct a homotopy in the following form:

$$H(u,p) = (1-p) \left[ \ddot{u} + \alpha_1 u \right] + p \left[ \ddot{u} + a \, u \dot{u}^2 + a u \ddot{u} + \alpha_1 u + \alpha_2 u^3 + \alpha_3 u^5 \right] = 0 \tag{4.25}$$

265

According to HPM, we assume that the solution of (4.25) can be expressed in a series of p

$$u(t) = u_0(t) + pu_1(t) + p^2 u_2(t) + \dots$$
(4.26)

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The coefficient  $\alpha_1$  expanded into a series in p in a similar way.

$$\alpha_1 = \omega^2 - p\omega_1 - p^2\omega_2 + \dots \tag{4.27}$$

Substituting (4.26) and (4.27) into (4.25) after some simplification and substitution and rearranging based on powers of *p*-terms, we have:

$$p^{0} = \ddot{u}_{0} + \omega^{2} u_{0} = 0,$$
  $u_{0}(0) = A,$   $\dot{u}_{0}(0) = 0$  (4.28)

269 And,

$$p^{1} = \ddot{u}_{1} + \omega^{2} u_{1} = \omega_{1} u_{0} - a u_{0} \dot{u}_{0}^{2} - a u_{0} \ddot{u}_{0} - \alpha_{2} u_{0}^{3} - \alpha_{3} u_{0}^{5}, \qquad u_{1}(0) = 0, \qquad \dot{u}(0) = 0$$
(4.29)

Considering the initial conditions  $u_0(0) = A$  and  $\dot{u}_0(0) = 0$  the solution of Eq. (4.28) is  $u_0 = A \cos(\omega t)$  Substituting the result into Eq. (4.29), we have:

$$p^{1} = \ddot{u}_{1} + \omega^{2} u_{1} = \omega_{1} A \cos(\omega t) - a \omega^{2} A^{3} \cos(\omega t) \sin^{2}(\omega t) - a \omega^{2} A^{3} \cos^{3}(\omega t) - \alpha_{2} A^{3} \cos^{3}(\omega t) - \alpha_{3} A^{5} \cos^{5}(\omega t)$$
(4.30)

No secular term in  $p^1$  requires that

$$\omega_1 = -\frac{1}{8}A^2 \left(-4a\omega^2 + 6\alpha_2 + 5\alpha_3 A^2\right)$$
(4.31)

Substituting (4.31) in to Eq (4.27) and setting p = 1, we can obtain the frequency of the nonlinear oscillator as follows:

$$\omega_{HPM} = \frac{1}{2} \frac{\sqrt{(2+A^2a)(8\alpha_1 + 5A^4\alpha_3 + 6\alpha_2A^2)}}{(2+A^2a)}$$
(4.32)

Table 4.2 shows the high accuracy of the Homotopy Perturbation Method with the Runge-Kutta Method.

277

#### 278 Example 3

In this section, we will consider the system with linear and nonlinear springs in series as it is shown in Fig. 4.2.

In this figure,  $k_1$  is the stiffness coefficient of the first linear spring, the coefficients associated with the linear and nonlinear portions of spring force in the second spring with cubic nonlinear characteristic are described by  $k_2$  and  $k_3$ , respectively. Let  $\varepsilon$  be defined as:

$$\varepsilon = k_2/k_3 \tag{4.33}$$

The case of  $k_3 > 0$  corresponds to a hardening spring while  $k_3 < 0$  indicates a softening one.

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	Case1: $A = 0.5$	5, a = 0.2,	Case2: $A = 1, a = 0.5, \alpha_1 = 1,$			
	$\alpha_1 = 2, \alpha_3$	$_{3} = 0.5$		$\alpha_2 = 0.5, c$	$\alpha_3 = 0.2$	
t	HPM	Runge -Kutta	t	HPM	Runge -Kutta	
	u(t)	u(t)		u(t)	u(t)	
0	0.4	0.4	0	1	1	
0.5	0.299437	0.299766	0.5	0.860691	0.853713	
1	0.049196	0.049299	1	0.469752	0.457651	
1.5	-0.225475	-0.225875	1.5	-0.080103	-0.072308	
2	-0.387780	-0.387848	2	-0.600724	-0.581112	
2.5	-0.355266	-0.355443	2.5	-0.927124	-0.919896	
3	-0.144634	-0.144902	3	-0.988938	-0.989543	
3.5	0.137916	0.138260	3.5	-0.774269	-0.769674	
4	0.351899	0.352131	4	-0.325557	-0.324619	
4.5	0.389486	0.389524	4.5	0.237755	0.215412	
5	0.231375	0.231700	5	0.715872	0.692419	
5.5	-0.042066	-0.042245	5.5	0.972568	0.966842	
6	-0.295018	-0.294619	6	0.955930	0.958391	

 Table 4.2
 Comparison of HPM solution and Runge-Kutta algorithm.

Let x and y denote the absolute displacements of the connection point of two springs, and the mass m, respectively. By introducing two new variables

$$u = y - x, r = x.$$
 (4.34)

Telli and Kopmaz [185] obtained the following governing equation for v and r:

$$(1+3\varepsilon\eta u^2)\ddot{u}+6\varepsilon\eta u\dot{u}^2+\omega_e^2u+\varepsilon\omega_e^2u^3=0, \qquad (4.35)$$

$$r = x = \xi (1 + \varepsilon u^2) u, y = (1 + \xi + \xi \varepsilon u^2) u,$$
(4.36)

289 Where a prime denotes differentiation with respect to time and

$$\xi = k_2/k_1, \quad \eta = \frac{\xi}{1+\xi}, \quad \omega_0^2 = \frac{k_2}{m(1+\xi)}.$$
 (4.37)

Eq. (4.35) is an ordinary differential equation in u. For Eq. (4.35), we consider the following initial conditions:

$$u(0) = A, \quad \dot{u}(0) = 0 \tag{4.38}$$

Eq. (4.35) can be rewritten as the following form:

$$\ddot{u} + 1.u = p. \left[ -3 \ddot{u} \varepsilon \eta u^2 - 6 \varepsilon \eta u \dot{u}^2 - \omega_0^2 \varepsilon u^3 - \omega_0^2 u + u \right] = 0, \quad p \in [0, 1].$$
(4.39)

Substituting Eqs. (4.6) and (4.7) into Eq. (4.39) and expanding, we can write the first two linear equations as follows:

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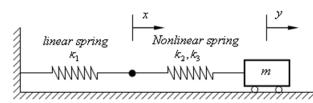


Figure 4.2 Nonlinear free vibration of a system of mass with serial linear and Nonlinear stiffness on a frictionless contact surface[185]

$$p^0: \quad \ddot{u}_0 + \omega^2 u_0 = 0, \qquad u_0(0) = A, \quad \dot{u}_0(0) = 0$$

$$(4.40)$$

$$p^{1}: \ddot{u}_{1} + \omega^{2} u_{1} = -3u_{0}^{"}\eta\varepsilon u_{0}^{2} - 6\eta\varepsilon u_{0}u_{0}^{'2}\omega_{0}^{2}\varepsilon u_{0}^{3} + (1 + \gamma_{1} - \omega_{0}^{2})u_{0}; \qquad (4.41)$$

Solving Eq. (4.40) gives:  $u_0 = A \cos \omega t$ . Substituting  $u_0$  into Eq. (4.41), yield:

$$p^{1} u_{1} + \omega^{2} u_{1} = 9A^{3} \eta \varepsilon \omega^{2} \cos^{3} \omega t - 6\eta \varepsilon \omega^{2} A^{3} \cos \omega t + \left(1 + \gamma_{1} - \omega_{0}^{2}\right) A \cos \omega t - \omega_{0}^{2} \varepsilon A^{3} \cos^{3} \omega t; \qquad (4.42)$$

# <sup>296</sup> For achieving the secular term, we use Fourier expansion series as follows:

$$9A^{3}\eta \varepsilon \omega^{2} \cos^{3} \omega t - 6\eta \varepsilon \omega^{2} A^{3} \cos \omega t - \omega_{0}^{2} \varepsilon A^{3} \cos^{3} \omega t$$

$$= \sum_{n=0}^{\infty} b_{2n+1} \cos \left[ (2n+1) \omega t \right]$$

$$= b_{1} \cos \left( \omega t \right) + b_{3} \cos(3 \omega t) + \dots$$

$$\approx \frac{3A^{3} \varepsilon}{4} \left( \eta \omega^{2} - \omega_{0}^{2} \right) \cos \left( \omega t \right) + \dots$$
(4.43)

Substituting Eq. (4.43) into Eq. (4.42) yields:

$$p^{1}: \quad \ddot{u}_{1} + \omega^{2} u_{1} = \left[\frac{3A^{2}\varepsilon}{4} \left(\eta\omega^{2} - \omega_{0}^{2}\right) + \left(1 + \gamma_{1} - \omega_{0}^{2}\right)\right] \times A\cos(\omega t)$$
(4.44)

Avoiding secular term, gives:

$$\gamma_1 = \frac{3A^2\varepsilon}{4} \left(\omega_0^2 - \eta\omega^2\right) + \left(\omega_0^2 - 1\right) \tag{4.45}$$

From Eq. (4.7) and setting p = 1, we have:

$$\gamma_1 = \omega - 1 \tag{4.46}$$

Comparing Eqs. (4.45) and (4.46), we can obtain:

$$\omega_{HPM} = \frac{3A^2\varepsilon}{4} \left(\omega_0^2 - \eta\omega^2\right) + \omega_0^2 \tag{4.47}$$

Solving Eq. (4.47), gives:

$$\omega_{HPM} = \frac{\omega_0 \sqrt{(4+3A^2 \varepsilon \eta) (4+3A^2 \varepsilon)}}{4+3A^2 \varepsilon \eta}, \qquad (4.48)$$

Table 4.3 Comparison of error percentages corresponding to various parameters of system

		Relative error %					
m	A	ε	$k_1$	$k_2$	$\omega_{HPM}$	numerical	$\frac{\omega_{HPM} - \omega_{num}}{\omega_{num}}$
1	0.5	0.5	50	5	2.220265	2.220231	0.00153
1	0.5	0.5	50	5	3.162277	3.175501	0.41644
1	2	0.5	5	5	1.889822	1.903569	0.72170
1	2	0.5	5	50	2.192645	2.195284	0.12021
3	5	1	8	16	1.612706	1.615107	0.14866
3	5	1	10	5	1.739775	1.749115	0.53398
5	10	2	12	16	1.545360	1.545853	0.03189
2	2	-0.1	10	10	1.434860	1.446389	0.00520
3	4	-0.02	30	10	1.313064	1.318370	0.40247
4	10	-0.008	6	3	0.703731	0.705412	0.23830

Table 4.3 represents the comparisons of angular frequencies for different parameters via numerical is presented in Table 1. The maximum relative error between the HPM results and numerical results is 0.72170 %.

# 305 5 ITERATION PERTURBATION METHOD (IPM)

The study of nonlinear oscillators is of interest to many researchers and various methods of solution have been proposed. The iteration perturbation method (IPM) is considered to be one of the powerful methods which is capable for nonlinear problems, it can converge to an accurate solution for smooth nonlinear systems. The iteration perturbation method was first proposed by He [87] in 2001 and used to give approximate solutions of the problems of nonlinear oscillators. The application of this method is used in [26, 61, 149].

#### 312 5.1 Basic idea of Iteration Perturbation Method

Many researchers have devoted their attention to obtaining approximate solution of nonlinear equations in the form:

$$\ddot{u} + u + \varepsilon f(u, \dot{u}) = 0, \tag{5.1}$$

<sup>315</sup> Subject to the following initial conditions:

$$u(0) = A, \quad \dot{u}(0) = 0$$
 (5.2)

We rewrite Eq. (5.1) in the following form:

$$\ddot{u} + u + \varepsilon u.g(u, \dot{u}) = 0, \tag{5.3}$$

317 Where  $g(u, \dot{u}) = f/u$ .

318 We construct an iteration formula for the above equation:

$$\ddot{u}_{n+1} + u_{n+1} + \varepsilon u_{n+1} \cdot g(u_n, \dot{u}_n) = 0, \tag{5.4}$$

Where we denote by  $u_n$  the *n* th approximate solution. For nonlinear oscillation, Eq. (5.4) is of Mathieu type. We will use the perturbation method to find approximately  $u_{n+1}$  the technique is called iteration perturbation method.

In order to assess the advantages and the accuracy of the iteration perturbation method we will consider the following examples.

Here, we will introduce a nonlinear oscillator with discontinuity in several different forms:

$$\frac{d^{2}u}{dt^{2}} + h(u) + \beta sgn(u)u = 0,$$
(5.5)

325 Or

$$\frac{d^2 u}{dt^2} + h(u) + \beta u |u| = 0,$$
(5.6)

326 With initial conditions

$$u(0) = A, \frac{du(0)}{dt} = 0 \tag{5.7}$$

In this work, we assume that h(u) is in a polynomial form. The reason for this assumption is that the discontinuity equations found in the literature belong to this family. Since there are no small parameters in Eq. (5.6) the traditional perturbation methods cannot be applied directly. In the following example, we assume a linear form h(u).

#### 331 5.2 Application of Iteration Perturbation Method

#### 332 Example1

We let  $h(u) = \alpha u$ , in Eq. (5.6).

We can rewrite Eq. (5.6) in the following form;

$$u'' + \alpha . u + \beta u \left| u \right| = 0 \tag{5.8}$$

To apply the Iteration Perturbation Method, the solution is expanded and the series of  $\varepsilon$ is introduced as follows:

$$u = u_0 + \sum_{i=0}^n \varepsilon^i u_i \tag{5.9}$$

$$\alpha = \omega^2 + \sum_{i=0}^n \varepsilon^i a_i \tag{5.10}$$

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$$\beta = \sum_{i=0}^{n} \varepsilon^{i} d_{i} \tag{5.11}$$

Substituting Eqs. (5.9), (5.10) and (5.11) into Eq. (5.8) and equating the terms with the identical powers of  $\varepsilon$ , a series of linear equations are obtained. Expanding the first two linear terms becomes as follows;

 $\varepsilon^{0}: \ddot{u}_{0} + \omega^{2} u_{0} = 0 , \quad u_{0}(0) = A , \quad \dot{u}_{0}(0) = 0$  (5.12)

$$\varepsilon^{1}: \quad u_{1}^{\prime\prime} + \omega^{2} u_{1} + a_{1} u_{0} + d_{1} u_{0} \mid u_{0} \mid = 0 \quad , \quad u_{1}(0) = 0 \quad , \quad \dot{u}_{1}(0) = 0 \quad (5.13)$$

Substituting the solution into Eq. (5.12), e.g.  $u_0 = A\cos(\omega t)$ , the deferential equation for  $u_1$  becomes;

$$u_1'' + \omega^2 u_1 + a_1 A \cos(\omega t) + d_1 A \cos(\omega t) |A \cos(\omega t)| = 0,$$
  

$$u_1(0) = 0, u_1'(0) = 0$$
(5.14)

#### <sup>342</sup> Note that the following Fourier series expansion is valid.

$$|A\cos(\omega t)|\cos(\omega t)^{2n-1} = \sum_{k=0}^{\infty} c_{2k+1}\cos((2k+1)\omega t)$$
  
=  $c_1\cos(\omega t) + c_3\cos(3\omega t) + \dots$  (5.15)

Where  $c_i$  can be determined by Fourier series, for example,

$$c_{1} = \frac{2}{\pi} \int_{0}^{\pi} |\cos(\omega t)|^{2n} \cos(\omega t) d(\omega t)$$
$$= \frac{2}{\pi} \left( \int_{0}^{\frac{\pi}{2}} \cos(\omega t)^{2n+1} d(\omega t) - \int_{0}^{\pi} \cos(\omega t)^{2n+1} d(\omega t) \right)$$
$$= \frac{2}{\sqrt{\pi}} \frac{\Gamma(n+1)}{\Gamma(n+3/2)}$$
(5.16)

Eq. (5.16) in Eq. (5.14) gives

$$u_1'' + \omega^2 u_1 + a_1 A \cos(\omega t) + d_1 A \sum_{k=0}^{\infty} c_{2k+1} \cos((2k+1)\omega t) = 0$$
(5.17)

345 Avoiding the presence of a secular term requires that

$$a_1 + d_1 c_1 A^2 = 0 \tag{5.18}$$

Also, substituting  $\varepsilon = 1$ , into Eqs. (5.9) and (5.10) gives:

$$\alpha = \omega^2 + a_1 \tag{5.19}$$

$$\beta = d_1 \tag{5.20}$$

From Eqs. (5.18), (5.19) and (5.20), the first-order approximation to the angular frequency is:

$$\omega = \sqrt{\alpha + \frac{8\varepsilon A}{3\pi}} \tag{5.21}$$

349 Case 1:

If  $\alpha = 1$ , we have

 $\omega_{IPM} = \sqrt{1 + \frac{8\varepsilon A}{3\pi}} \tag{5.22}$ 

It is the same as that obtained by the Homotopy perturbation method and the Variational method [95, 182].

353 Case 2:

If  $\alpha = 0$ , we have

$$\omega_{IPM} = \sqrt{\frac{8\varepsilon A}{3\pi}} \tag{5.23}$$

The obtained frequency in Eq. (5.23) is valid for the whole solution domain  $0 < A < \infty$ .

356

357 Example 2

358 If  $h(u) = \alpha u^3$ , in Eq. (5.6).

359 Then we have

$$\frac{d^2u}{dt^2} + \alpha . u^3 + \beta u |u| = 0$$
(5.24)

To apply the Iteration Perturbation Method, the solution is expanded and the series of  $\varepsilon$ is introduced as follows:

$$u = u_0 + \sum_{i=0}^{n} \varepsilon^i u_i \tag{5.25}$$

$$0 = \omega^2 + \sum_{i=0}^n \varepsilon^i a_i \tag{5.26}$$

$$1 = \sum_{i=0}^{n} \varepsilon^{i} d_{i} \tag{5.27}$$

Substituting Eqs. (5.25),(5.26) and (5.27) into Eq. (5.24) and equating the terms with the identical powers of  $\varepsilon$ , a series of linear equations are obtained. Expanding the first two linear terms becomes as follows;

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$$\varepsilon^{0}: \ddot{u}_{0} + \omega^{2} u_{0} = 0 , \quad u_{0}(0) = A , \quad \dot{u}_{0}(0) = 0$$
 (5.28)

$$\varepsilon^{1}: \quad u_{1}'' + \omega^{2}u_{1} + a_{1}u_{0} + d_{1}\alpha u_{0}^{3} + \beta u_{0} |A\cos(\omega t)| = 0, \quad u_{1}(0) = 0, \quad \dot{u}_{1}(0) = 0$$
(5.29)

Substituting the solution into Eq. (5.28), e.g.  $u_0 = A\cos(\omega t)$ , the deferential equation for u<sub>1</sub> becomes;

$$u_1'' + \omega^2 u_1 + a_1 A \cos(\omega t) + d_1 \alpha A^3 \cos^3(\omega t) + \beta A \cos(\omega t) |A \cos(\omega t)| = 0$$
(5.30)

<sup>367</sup> We have the following identity;

$$\cos^{3}(\omega t) = \frac{3}{4}\cos(\omega t) + \frac{1}{4}\cos(3\omega t)$$
(5.31)

368 Note that the following Fourier series expansion is valid.

$$|A\cos(\omega t)|^{2n-1}\cos(\omega t) = \sum_{k=0}^{\infty} c_{2k+1}\cos((2k+1)\omega t)$$
  
=  $c_1\cos(\omega t) + c_3\cos(3\omega t) + \dots$  (5.32)

 $c_i$  can be determined by Fourier series, for example :

$$c_{1} = \frac{2}{\pi} \int_{0}^{\pi} |\cos(\omega t)|^{2n} \cos(\omega t) d(\omega t)$$
$$= \frac{2}{\pi} \left( \int_{0}^{\frac{\pi}{2}} \cos(\omega t)^{2n+1} d(\omega t) - \int_{0}^{\pi} \cos(\omega t)^{2n+1} d(\omega t) \right)$$
(5.33)

$$= \frac{2}{\sqrt{\pi}} \frac{\Gamma(n+1)}{\Gamma(n+3/2)}$$

 $_{370}$  By means of Eqs. (5.31),(5.32) and (5.33) we find that

$$u_1'' + \omega^2 u_1 + (a_1 + d_1 A^2 \frac{3}{4}) A \cos(\omega t) + d_1 A^3 \frac{1}{4} \cos(3\omega t)) + A^2 \sum_{k=0}^{\infty} c_{2k+1} \cos((2k+1)\omega t) = 0$$
(5.34)

#### $_{371}$ No secular term in $u_1$ requires that

$$a_1 + d_1 \alpha A^2 \frac{3}{4} + \beta A \frac{8}{3\pi} = 0 \tag{5.35}$$

Also, substituting  $\varepsilon = 1$ , into Eqs. (5.26) and (5.27) gives:

$$0 = \omega^2 + a_1 + \dots \tag{5.36}$$

$$1 = d_1 \tag{5.37}$$

From Eqs. (5.35) ,(5.36) and (5.37), the first-order approximation to the angular frequency is:

$$\omega_{IPM} = \sqrt{\frac{3\alpha A^2}{4} + \frac{8\beta A}{3\pi}} \tag{5.38}$$

375 Case 1: 376 If  $\alpha = \beta, \beta = \varepsilon$  we have

 $\omega_{IPM} = \sqrt{\frac{3\beta A^2}{4} + \frac{8\varepsilon A}{3\pi}} \tag{5.39}$ 

This agrees well with that obtained by the Homotopy perturbation method and the Variational method [95, 182].

379 And its period is given by

$$T_{IPM} = \frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{3\beta A^2}{4} + \frac{8\varepsilon A}{3\pi}}}$$
(5.40)

380 Case 2 :

If  $\varepsilon = 0$ , its period can be written as;

$$T_{IPM} = \frac{4\pi}{\sqrt{3}} \beta^{-\frac{1}{2}} A^{-1} \tag{5.41}$$

The exact period was obtained by Acton and Squire in 1985 [2].

$$T_{ex} = 7.4164\beta^{-\frac{1}{2}}A^{-1} \tag{5.42}$$

The maximal relative error is less than 2.2% for  $all\beta > 0!$ 

#### 384 6 ENERGY BALANCE METHOD (EBM)

Nonlinear oscillator models have been widely used in many areas of physics and engineering 385 and are of significant importance in mechanical and structural dynamics for the comprehensive 386 understanding and accurate prediction of motion. This method was proposed by He [90] in 387 2002. This method can be seen as a Ritz method and leads to a very rapid convergence of 388 the solution, and can be easily extended to other nonlinear oscillations. In short, this method 389 yields extended scope of applicability, simplicity, flexibility in application, and avoidance of 390 complicated numerical and analytical integration as compared to others among the previous 391 approaches, such as, the perturbation methods, and so could widely applicable in engineering 392 and science. Energy balance method used heavily in the literature in [17, 19, 22, 25, 55, 56, 58, 393 60, 65–67, 116, 120, 141, 150, 178, 209 and the references therein. 394

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#### 395 6.1 Basic idea of Energy Balance Method

<sup>396</sup> In the present paper, we consider a general nonlinear oscillator in the form [90]:

$$\ddot{u} + f(u(t)) = 0$$
 (6.1)

In which u and t are generalized dimensionless displacement and time variables, respectively. Its variational principle can be easily obtained:

$$J(u) = \int_0^t \left(-\frac{1}{2}\dot{u}^2 + F(u)\right) dt$$
(6.2)

Where  $T = \frac{2\pi}{\omega}$  is period of the nonlinear oscillator,  $F(u) = \int f(u) du$ . Its Hamiltonian, therefore, can be written in the form;

$$H = \frac{1}{2}\dot{u}^2 + F(u) + F(A)$$
(6.3)

401 Or

$$R(t) = -\frac{1}{2}\dot{u}^{2} + F(u) - F(A) = 0$$
(6.4)

<sup>402</sup> Oscillatory systems contain two important physical parameters, i.e.  $\omega$  is the frequency and <sup>403</sup> A is the amplitude of the oscillation. So let us consider such initial conditions:

$$u(0) = A, \quad \dot{u}(0) = 0 \tag{6.5}$$

404 We use the following trial function to determine the angular frequency  $\omega$ 

$$u(t) = A\cos\omega t \tag{6.6}$$

Substituting (6.6) into u term of (6.4), yield:

$$R(t) = \frac{1}{2}\omega^2 A^2 \sin^2 \omega \ t + F(A \cos \omega \ t) - F(A) = 0$$
(6.7)

If, by chance, the exact solution had been chosen as the trial function, then it would be possible to make R zero for all values of t by appropriate choice of  $\omega$ . Since Eq. (6.6) is only an approximation to the exact solution, R cannot be made zero everywhere. Collocation at  $\omega t = \frac{\pi}{4}$  gives:

$$\omega = \sqrt{\frac{2(F(A)) - F(A\cos\omega t)}{A^2 \sin^2 \omega t}}$$
(6.8)

410 Its period can be written in the form:

$$T = \frac{2\pi}{\sqrt{\frac{2(F(A)) - F(A\cos\omega t)}{A^2\sin^2\omega t}}}$$
(6.9)

#### 411 6.2 Application of Energy Balance Method

#### 412 Example 1

- <sup>413</sup> In this section, we will consider the system with linear and nonlinear springs in series.
- In Eq. (4.35), Its Variational principle can be easily obtained:

$$J(u) = \int_0^t \left( -\frac{1}{2} \dot{u}^2 \left( 1 + \frac{3}{2} \varepsilon \eta \, u^2 \right) + \omega_0^2 \left( \frac{1}{2} u^2 + \frac{1}{4} \varepsilon u^4 \right) \right) dt \tag{6.10}$$

415 Its Hamiltonian, therefore, can be written in the form:

$$H = \frac{1}{2}\dot{u}^{2} \left(1 + \frac{3}{2}\varepsilon \eta u^{2}\right) + \omega_{0}^{2} \left(\frac{1}{2}u^{2} + \frac{1}{4}\varepsilon u^{4}\right)$$
$$= \frac{1}{2}\omega_{0}^{2}A^{2} + \frac{1}{4}\omega_{0}^{2}\varepsilon A^{4}$$
(6.11)

416 OT

$$R(t) = \frac{1}{2}\dot{u}^{2} \left(1 + \frac{3}{2}\varepsilon \eta u^{2}\right) + \omega_{0}^{2} \left(\frac{1}{2}u^{2} + \frac{1}{4}\varepsilon u^{4}\right) -\frac{1}{2}\omega_{0}^{2}A^{2} - \frac{1}{4}\omega_{0}^{2}\varepsilon A^{4} = 0$$
(6.12)

<sup>417</sup> Oscillatory systems contain two important physical parameters, i.e. the frequency  $\omega$  and <sup>418</sup> the amplitude of oscillation, A. So let us consider such initial conditions:

$$u(0) = A, \quad \dot{u}(0) = 0$$
 (6.13)

Assume that its initial approximate guess can be expressed as:

$$u(t) = A\cos\omega t \tag{6.14}$$

420 Substituting Eq. (6.14) into Eq. (6.12), yields:

$$R(t) = \frac{1}{2} (-A\omega \sin \omega t)^2 (1 + \frac{3}{2}\varepsilon \eta (A\cos \omega t)^2) + \omega_0^2 (\frac{1}{2} (A\cos \omega t)^2) + \frac{1}{4}\varepsilon (A\cos \omega t)^4) - \frac{1}{2}\omega_0^2 A^2 - \frac{1}{4}\omega_0^2 \varepsilon A^4 = 0$$
(6.15)

421 Which trigger the following result:

$$\omega = \frac{\omega_0 \sqrt{2}}{A \sin \omega t} \sqrt{\frac{-\left(\frac{1}{2} \left(A \cos \omega t\right)^2 + \frac{1}{4} \varepsilon \left(A \cos \omega t\right)^4\right) + \frac{1}{2} A^2 + \frac{1}{4} \varepsilon A^4}{\left(1 + \frac{3}{2} \varepsilon \eta \left(A \cos \omega t\right)^2\right)}}$$
(6.16)

422 If we collocate at  $\omega t = \frac{\pi}{4}$ , we obtain:

$$\omega_{EBM} = \frac{\omega_0 \sqrt{(4+3A^2\varepsilon\eta)\left(4+3A^2\varepsilon\right)}}{4+3A^2\varepsilon\eta},\tag{6.17}$$

423 Its period can be written in the form:

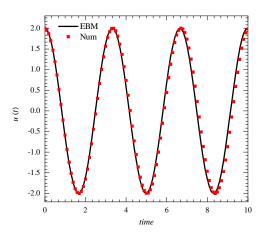


Figure 6.1 Comparison between approximate solutions and numerical solutions for  $m = 1, A = 2, \varepsilon = 0.5, k_1 = 5, k_2 = 5$ 

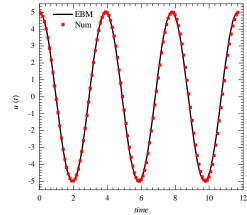


Figure 6.2 Comparison between approximate solutions and numerical solutions for m = 3, ~A = 5,  $~\varepsilon$  = 1,  $~k_1$  = 8,  $~k_2$  = 16

$$T_{EBM} = \frac{2\pi \left(4 + 3A^2 \varepsilon \eta\right)}{\omega_0 \sqrt{\left(4 + 3A^2 \varepsilon \eta\right) \left(4 + 3A^2 \varepsilon\right)}} \tag{6.18}$$

To further illustrate and verify the accuracy of this approximate analytical approach, comparison of the time history oscillatory displacement responses for the system with linear and nonlinear springs in series with numerical solutions are depicted in Figures 6.1 and 6.2. Figures 6.1 and 6.2 represent the displacements of u(t) for a mass with different initial conditions and spring stiffnesses.

# 430 Example 2

429

From Hamden [79], it is known that the free vibrations of an autonomous conservative oscillator with inertia and static type fifth-order non-linearties is expressed by

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$$\ddot{x} + \lambda x + \varepsilon_1 x^2 \ddot{x} + \varepsilon_1 x \dot{x}^2 + \varepsilon_2 x^4 \ddot{x} + 2\varepsilon_2 x^3 \dot{x}^2 + \varepsilon_3 x^3 + \varepsilon_4 x^5 = 0, \qquad (6.19)$$

433 With the initial conditions:

$$x(0) = A \quad \dot{x}(0) = 0 \tag{6.20}$$

Motion is assumed to start from the position of maximum displacement with zero initial velocity.  $\lambda$  is an integer which may take values of  $\lambda = 1,0$  or -1, and  $\varepsilon_1, \varepsilon_2, \varepsilon_3$  and  $\varepsilon_4$  are positive parameters.

<sup>437</sup> The solution of nonlinear equation with the Energy Balance method is:

$$\ddot{x} + \lambda x + \varepsilon_1 x^2 \ddot{x} + \varepsilon_1 x \, \dot{x}^2 + \varepsilon_2 x^4 \ddot{x} + 2\varepsilon_2 x^3 \dot{x}^2 + \varepsilon_3 x^3 + \varepsilon_4 x^5 = 0, \tag{6.21}$$

in which x and t are generalized dimensionless displacement and time variables, respectively. Its Variational principle can be easily obtained:

$$x(0) = A, \quad \dot{x}(0) = 0$$
 (6.22)

in which x and tare generalized dimensionless displacement and time variables, respectively.
Its Variational principle can be easily obtained:

$$J(x) = \int_0^t \left( -\frac{1}{2} \dot{x}^2 \left( 1 + \varepsilon_1 x^2 + \varepsilon_2 x^4 \right) + \frac{\lambda}{2} x^2 + \frac{\varepsilon_3}{4} x^4 + \frac{\varepsilon_4}{6} x^6 \right) dt$$
(6.23)

442 Its Hamiltonian, therefore, can be written in the form:

$$H = \frac{1}{2}\dot{x}^{2}\left(1 + \varepsilon_{1}x^{2} + \varepsilon_{2}x^{4}\right) + \frac{\lambda}{2}x^{2} + \frac{\varepsilon_{3}}{4}x^{4} + \frac{\varepsilon_{4}}{6}x^{6} = \frac{\lambda}{2}A^{2} + \frac{\varepsilon_{3}}{4}A^{4} + \frac{\varepsilon_{4}}{6}A^{6}$$
(6.24)

443 Or

$$R(t) = \frac{1}{2}\dot{x}^{2} \left(1 + \varepsilon_{1}x^{2} + \varepsilon_{2}x^{4}\right) + \frac{\lambda}{2}x^{2} + \frac{\varepsilon_{3}}{4}x^{4} + \frac{\varepsilon_{4}}{6}x^{6} - \frac{\lambda}{2}A^{2} - \frac{\varepsilon_{3}}{4}A^{4} - \frac{\varepsilon_{4}}{6}A^{6} = 0$$
(6.25)

Oscillatory systems contain two important physical parameters, i.e. the frequency  $\omega$  and the amplitude  $x(t) = A \cos \omega t$  of oscillation, A. So let us consider such initial conditions:

$$x(0) = A, \quad \dot{x}(0) = 0$$
 (6.26)

Assume that its initial approximate guess can be expressed as:

$$x(t) = A\cos\omega t \tag{6.27}$$

Substituting Eq. (6.27) into Eq. (6.25) yields:

$$R(t) = \frac{1}{2} (-A\sin\omega t)^2 (1 + \varepsilon_1 (A\cos\omega t)^2 + \varepsilon_2 (A\cos\omega t)^4) + \frac{\lambda}{2} (A\cos\omega t)^2 + \frac{\varepsilon_3}{4} (A\cos\omega t)^4 + \frac{\varepsilon_4}{6} (A\cos\omega t)^6 - \frac{\lambda}{2} A^2 - \frac{\varepsilon_3}{4} A^4 - \frac{\varepsilon_4}{6} A^6 = 0$$

$$(6.28)$$

448 Which trigger the following results

$$\omega = \frac{\sqrt{2}}{A\sin\omega t} \sqrt{\frac{\frac{\lambda}{2} \left(A^2 - \left(A\cos\omega t\right)^2\right) + \frac{\varepsilon_3}{4} \left(A^4 - \left(A\cos\omega t\right)^4\right) + \frac{\varepsilon_4}{6} \left(A^6 - \left(A\cos\omega t\right)^6\right)}{1 + \varepsilon_1 \left(A\cos\omega t\right)^2 + \varepsilon_2 \left(A\cos\omega t\right)^4}} \tag{6.29}$$

449 If we collocate at  $\omega t = \frac{\pi}{4}$ , we obtain:

$$\omega_{EBM} = \frac{\sqrt{3}}{3} \sqrt{\frac{12\lambda + 9\varepsilon_3 A^2 + 7\varepsilon_4 A^4}{4 + 2\varepsilon_1 A^2 + \varepsilon_2 A^4}} \tag{6.30}$$

450 Substituting Eq. (6.30) into Eq. (6.27) yields:

$$x(t) = A\cos\left(\frac{\sqrt{3}}{3}\sqrt{\frac{12\lambda + 9\varepsilon_3 A^2 + 7\varepsilon_4 A^4}{4 + 2\varepsilon_1 A^2 + \varepsilon_2 A^4}} \quad t\right)$$
(6.31)

# 451 The numerical solution with Runge-Kutta method for nonlinear equation is:

$$\dot{x}_1 = x_2 \ x_1(0) = A \tag{6.32}$$

452 And

$$\dot{x}_{2} = -\frac{1}{1+\varepsilon_{1}x_{1}^{2}+\varepsilon_{2}x_{1}^{4}} \left(\lambda x_{1}+\varepsilon_{1}x_{1}x_{2}^{2}+2\varepsilon_{2}x_{1}^{3}x_{2}^{2}+\varepsilon_{3}x_{1}^{3}+\varepsilon_{4}x_{1}^{5}\right), \quad x_{2}(0) = 0 \quad (6.33)$$

<sup>453</sup> Motion is assumed to start from the position of maximum displacement with zero initial <sup>454</sup> velocity.  $\lambda$  Is an integer which may take values of  $\lambda = 1, 0 \text{ or} -1$ , and  $\varepsilon_1, \varepsilon_2, \varepsilon_3$  and  $\varepsilon_4$  are positive <sup>455</sup> parameters .The values of parameters  $\varepsilon_1, \varepsilon_2, \varepsilon_3$  and  $\varepsilon_4$  associated for a mode is shown in Table <sup>456</sup> 6.1.

Table 6.1 Values of dimensionless parameters  $\varepsilon_i$  in Eq. (6.31) for a mode

Mode	$\varepsilon_1$	$\varepsilon_2$	$\varepsilon_3$	$\varepsilon_4$
1	0.326845	$0.\ 129579$	$0.\ 232598$	0. 087584
2	1.642033	0.913055	0.313561	0.204297
3	4.051486	1.665232	0.281418	0.149677

It can be seen from Figures 6.3-6.4 EBM results have a good agreement with the numerical solution for 3 modes.Figures show the motion of the system is a periodic motion and the amplitude of vibration is a function of the initial conditions.

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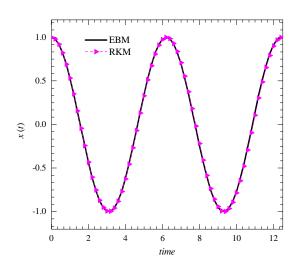


Figure 6.3 The Comparison between energy balance method solution and the numerical solution (Runge-Kutta method), with  $\lambda=1$ , A=1 for mode-1.

460

#### 461 Example 3

Consider a straight Euler-Bernoulli beam of length L, a cross-sectional area A, the mass per unit length of the beam m, a moment of inertia I, and a modulus of elasticity E that is subjected to an axial force of magnitude P as shown in Fig.6.6. The equation of motion including the effects of mid-plane stretching is given by:

$$m\frac{\partial^2 w'}{\partial t'^2} + EI\frac{\partial^4 w'}{\partial x'^2} + \bar{P}\frac{\partial^2 w'}{\partial x'^2} - \frac{EA}{2L}\frac{\partial^2 w'}{\partial x'^2} \int_0^L \left(\frac{\partial^2 w'}{\partial x'^2}\right)^2 dx' = 0$$
(6.34)

<sup>466</sup> For convenience, the following non-dimensional variables are used:

$$x = x'/L, w = w'/\rho, t = t'(EI/ml^4)^{1/2}, P = \bar{P}L^2/EI$$
(6.35)

Where  $\rho = (I/A)^{1/2}$  is the radius of gyration of the cross-section. As a result Eq. (6.34) can be written as follows:

$$\frac{\partial^2 w}{\partial t^2} + \frac{\partial^4 w}{\partial x^4} + P \frac{\partial^2 w}{\partial x^2} - \frac{1}{2} \frac{\partial^2 w}{\partial x^2} \int_0^L \left(\frac{\partial^2 w}{\partial x^2}\right)^2 dx = 0$$
(6.36)

Assuming  $w(x,t) = V(t) \phi(x)$  where  $\phi(x)$  is the first eigenmode of the beam [189] and applying the Galerkin method, the equation of motion is obtained as follows:

$$\frac{d^2 V(t)}{dt^2} + (\alpha_1 + P\alpha_2)V(t) + \alpha_3 V^3(t) = 0$$
(6.37)

The Eq. (6.37) is the differential equation of motion governing the non-linear vibration of Euler-Bernoulli beams. The center of the beam is subjected to the following initial conditions:

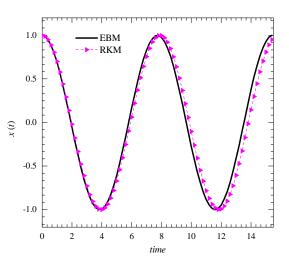


Figure 6.4 The comparison between energy balance method solution and the numerical solution (Runge-Kutta method), with  $\lambda$ =1, A=1 for mode-2.

$$V(0) = \Delta, \ \frac{dV(0)}{dt} = 0 \tag{6.38}$$

473 Where  $\Delta$  denotes the non-dimensional maximum amplitude of oscillation and  $\alpha_1, \alpha_2$  and 474  $\alpha_3$  are as follows:

$$\alpha_1 = \left( \int_0^1 \left( \frac{\partial^4 \phi(x)}{\partial x^4} \right) \phi(x) \, dx \right) \middle/ \int_0^1 \phi^2(x) \, dx \tag{6.39a}$$

$$\alpha_2 = \left( \int_0^1 \left( \frac{\partial^2 \phi(x)}{\partial x^2} \right) \phi(x) \, dx \right) \middle/ \int_0^1 \phi^2(x) \, dx \tag{6.39b}$$

$$\alpha_3 = \left( \left( -\frac{1}{2} \right) \int_0^1 \left( \frac{\partial^2 \phi(x)}{\partial x^2} \int_0^1 \left( \frac{\partial^2 \phi(x)}{\partial x^2} \right)^2 dx \right) \phi(x) dx \right) \Big/ \int_0^1 \phi^2(x) dx \tag{6.39c}$$

475 Variational formulation of Eq. (6.37) can be readily obtained as follows:

$$J(V) = \int_0^t \left( -\frac{1}{2} \frac{dV(t)}{dt} + \frac{1}{2} (\alpha_1 + P\alpha_2) V^2(t) + \alpha_3 V^4(t) \right) dt.$$
(6.40)

476 Its Hamiltonian, therefore, can be written in the form:

$$H = -\frac{1}{2} \frac{dV(t)}{dt} + \frac{1}{2} (\alpha_1 + P\alpha_2) V^2(t) + \alpha_3 V^4(t)$$
(6.41)

477 And

$$H_{t=0} = \frac{1}{2}\Delta^{2}(\alpha_{1} + P\alpha_{2}) + \frac{1}{4}\alpha_{4}\Delta^{4}$$
(6.42)

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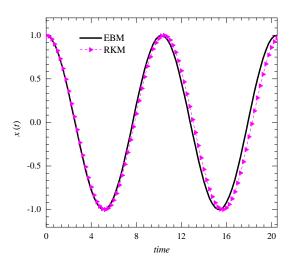


Figure 6.5 The comparison between energy balance method solution and numerical solution (Runge-Kutta method), with  $\lambda$ =1, A=1 for mode-3.

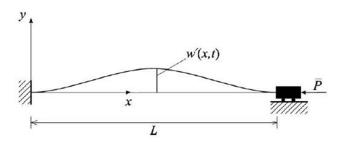


Figure 6.6 A schematic of an Euler-Bernoulli beam subjected to an axial load.

$$H_t - H_{t=0} = \frac{1}{2} \frac{dV(t)}{dt} + \frac{1}{2} (\alpha_1 + P\alpha_2) V^2(t) + \alpha_3 V^4(t) - \frac{1}{2} \Delta^2(\alpha_1 + P\alpha_2) - \frac{1}{4} \alpha_4 \Delta^4 \qquad (6.43)$$

478

$$V(t) = A\cos\omega t \tag{6.44}$$

If we substitute Eq. (6.46) into Eq. (6.45), it results the following residual equation

We will use the trial function to determine the angular frequency  $\omega$ , i.e.

$$\frac{1}{2} \left(-\Delta \omega \sin\left(\omega t\right)\right)^2 + \frac{1}{2} \left(\alpha_1 + P\alpha_2\right) \left(\Delta \cos\left(\omega t\right)\right)^2 + \frac{1}{2} \alpha_3 \left(\Delta \cos\left(\omega t\right)\right)^4 - \frac{1}{2} \Delta^2 \left(\alpha_1 + P\alpha_2\right) - \frac{1}{4} \alpha_3 \Delta^4 = 0$$

$$(6.45)$$

480 If we collocate at  $\omega t = \frac{\pi}{4}$  we obtain:

$$\frac{1}{4}\Delta^2 \omega^2 - \frac{1}{4}\Delta^2 (\alpha_1 + P\alpha_2) - \frac{3}{16}\alpha_3 \Delta^4 = 0$$
 (6.46)

<sup>481</sup> The non-linear natural frequency and the deflection of the beam center become as follows:

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$$\omega_{NL} = \frac{\sqrt{4\left(\alpha_1 + P\alpha_2\right) + 3\alpha_3\Delta^2}}{2} \tag{6.47}$$

According to Eq. (6.49) and Eq. (6.46), we can obtain the following approximate solution:

$$V(t) = \Delta \cos\left(\frac{\sqrt{4(\alpha_1 + P\alpha_2) + 3\alpha_3\Delta^2}}{2}t\right)$$
(6.48)

483 Non-linear to linear frequency ratio is:

$$\frac{\omega_{NL}}{\omega_L} = \frac{1}{2} \frac{\sqrt{4\left(\alpha_1 + p\alpha_2\right) + 3\alpha_3 \Delta^2}}{\sqrt{\alpha_1 + p\alpha_2}} \tag{6.49}$$

Table 6.2 shows the comparison of non-linear to linear frequency ratio ( $\omega_{NL}/\omega_L$ )

$\Delta$	Present Study	Exact	Pade approximate	Pade approximate	Error %
	(EBM)	solution	$P{4,2}[12]$	$P\{6,4\}[12]$	$\left(\omega_{EBM}-\omega_{ex} ight)/\omega_{ex}$
0.2	1.044031	1.0438823	1.0438824	1.0438823	0.014211
0.4	1.16619	1.1644832	1.1644868	1.1644832	0.146604
0.6	1.345362	1.3397037	1.3397374	1.3397039	0.422385
0.8	1.56205	1.5505542	1.5506741	1.5505555	0.741395
1	1.802776	1.7844191	1.7846838	1.7844228	1.028712
1.5	2.462214	2.4254023	2.4261814	2.4254185	1.517775
2	3.162278	3.1070933	3.1084562	3.1071263	1.776077

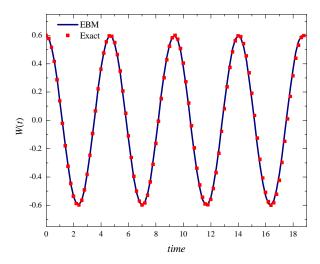


Figure 6.7 Comparison of analytical solution of W(t) based on timewith the exact solution for simply supported beam,  $\Delta = 0.6$ ,  $\alpha_1 = 1$ ,  $\alpha_2 = 0$ ,  $\alpha_3 = 3$ 

To show the accuracy of Energy Balance Method (EBM), comparisons of the time history oscillatory displacement response for Euler-Bernoulli beams with exact solutions are presented in Figs. 6.7 and 6.8.

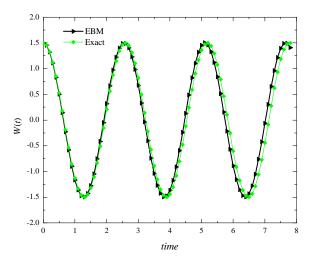


Figure 6.8 Comparison of analytical solution of W(t) based on timewith the exact solution for simply supported beam,  $\Delta = 1.5$ ,  $\alpha_1 = 1$ ,  $\alpha_2 = 0$ ,  $\alpha_3 = 3$ 

It can be observed that the results of EBM require smaller computational effort and only a first-order approximation leads to accurate solutions. The Influence of  $\alpha_3$  on nonlinear to linear frequency and  $\alpha_1$  are presented in figures 6.9 and 6.10. It has illustrated that Energy Balance Method is a very simple method and quickly convergent and valid for a wide range of vibration amplitudes and initial conditions. The accuracy of the results shows that the Energy Balance Method can be potentiality used for the analysis of strongly nonlinear oscillation problems accurately.

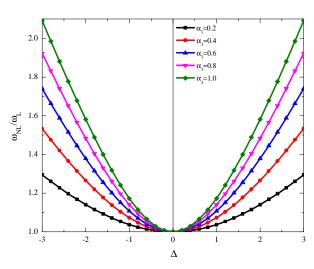


Figure 6.9 Influence of  $\alpha_3$  on nonlinear to linear frequency base on  $\Delta$  for  $\alpha_1 = 1$ ,  $\alpha_2 = 0.5$ , p = 2

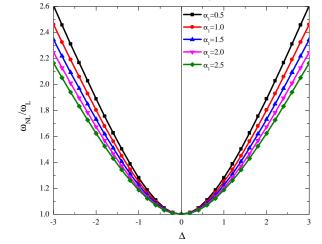


Figure 6.10 Influence of  $\alpha_3$  on nonlinear to linear frequency base on  $\Delta$  for  $\alpha_2 = 1$ ,  $\alpha_3 = 3$ , p = 3

## 494 7 PARAMETER – EXPANSION METHOD (PEM)

Various perturbation methods have been applied frequently to analyze nonlinear vibration equations. These methods are characterized by expansions of the dependent variables in power series in a small parameter, resulting in a collection of linear deferential equations which can be solved successively. He proposed the parameter expanding method for the first time in his review article [100]. The main property of the method is to use parameter-expansion technique to eliminate the secular terms and to achieve the frequency. PEM was successfully applied to various engineering problems [8, 42, 69, 97, 103, 118, 134, 147, 161, 190, 195–197, 201].

# 502 7.1 Basic idea of Parameter–Expansion Method

<sup>503</sup> In order to use the PEM, we rewrite the general form of Duffing equation in the following <sup>504</sup> form[100]:

$$\ddot{u} + \varepsilon u + 1 \cdot N(u, t) = 0. \tag{7.1}$$

<sup>505</sup> Where N(u,t) includes the nonlinear term. Expanding the solution  $u,\varepsilon$  as a coefficient of <sup>506</sup> u, and 1 as a coefficient of N(u,t), the series of p can be introduced as follows:

$$u = u_0 + p u_1 + p^1 u_2 + p^2 u_3 + \dots$$
(7.2)

$$\varepsilon = \omega^2 + p \, d_1 + p^1 \, d_2 + p^2 \, d_3 + \dots \tag{7.3}$$

$$1 = p a_1 + p^1 a_2 + p^2 a_3 + \dots (7.4)$$

Substituting (7.2)-(7.4) into (7.1) and equating the terms with the identical powers of p, we have

$$p^0: \ddot{u}_0 + \omega^2 u_0 = 0 \quad , \tag{7.5}$$

$$p^{1}: \ddot{u}_{1} + \omega^{2} u_{1} + d_{1} u_{0} + a_{1} N(u_{0}, t) = 0 ,$$
  

$$\vdots$$
(7.6)

Considering the initial conditions  $u_0(0) = A$  and  $\dot{u}_0(0) = 0$ , the solution of (7.5) is  $u_0 = A \cos(\omega t)$ . Substituting  $u_0$  into (7.6), we obtain

$$p^{1}: \ddot{u}_{1} + \omega^{2} u_{1} + d_{1} A \cos(\omega t) + a_{1} N(A \cos(\omega t), t) = 0 \quad .$$
(7.7)

<sup>511</sup> For achieving the secular term, we use Fourier expansion series as follows:

$$N(A\cos(\omega t), t) = \sum_{n=0}^{\infty} b_{2k+1} \cos((2k+1)\omega t).$$
(7.8)

Substituting (7.8) into(7.7) yields;

$$p^{1}: \ddot{u}_{1} + \omega^{2} u_{1} + (d_{1} A + a_{1} b_{1}) \cos(\omega t) = 0 \quad .$$
(7.9)

513 For avoiding secular term, we have

$$(d_1 A + a_1 b_1) = 0 \quad . \tag{7.10}$$

514 Setting p = 1 in (7.3) and (7.4), we have:

$$d_1 = \varepsilon - \omega^2 A = 0 , \qquad (7.11)$$

$$a_1 = 1.$$
 (7.12)

Substituting (7.11) and (7.12) into (7.10), we will achieve the first-order approximation frequency (7.1). Note that, from (7.4) and (7.12), we can find that  $a_i = 0$  for all i = 1, 2, 3, 4, ...

## 517 7.2 Application of Parameter – Expansion Method

#### 518 Example 1

To illustrate the basic solution procedure, we consider the following nonlinear oscillator:

$$\ddot{u} + \alpha \, u + \beta \, u^3 = F_0 \cos \omega \, t \quad , \, u(0) = A \quad , \, \dot{u}(0) = 0.$$
(7.13)

520 We rewrite it in this form

$$\ddot{u} + \alpha . u + 1.(\beta u^3 - F_0 \cos \omega t) = 0.$$
(7.14)

Assume that the solution can be expressed as a power series in an artificial Parameter to p

$$u = u_0 + pu_1 + p^2 u_2 + \dots, (7.15)$$

522 Where p is a bookkeeping parameter.

We assume that the coefficients  $\alpha$  and 1 on the left side of Eq.(7.14) can be respectively expanded into a series in p:

$$\alpha = \omega^2 + p\omega_1 + p^2\omega_2 + \dots, \qquad (7.16)$$

$$1 = a_1 p + a_2 p^2 + \dots (7.17)$$

Substituting Eqs.(7.16) and (7.17) into Eq. (7.14) and equating the terms with the identical powers p, we have:

$$p^{0}: \ddot{u}_{0} + \omega^{2} u_{0} = 0, \quad u_{0}(0) = A, \dot{u}_{0}(0) = 0,$$
 (7.18)

$$p^{1}: \ddot{u}_{1} + \omega^{2} u_{1} + \omega_{1} u_{0} + a_{1} \beta \, u_{0}^{3} - a_{1} F_{0} \cos \omega \, t = 0$$
(7.19)

Solving Eq.(7.18), we have:

$$u_0 = A\cos\omega t \tag{7.20}$$

<sup>528</sup> Substituting the result into Eq. (7.19), we have:

$$\ddot{u}_1 + \omega^2 u_1 + \omega_1 A \cos \omega t + a_1 \beta A^3 \cos^3 \omega t - a_1 F_0 \cos \omega t = 0$$
(7.21)

529 We have the following identity

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$$\cos^{3}(\omega t) = \frac{3}{4}\cos(\omega t) + \frac{1}{4}\cos(3\omega t)$$
(7.22)

530 And

$$\ddot{u}_1 + \omega^2 u_1 + (\omega_1 A + \frac{3}{4} a_1 \beta A^3 - a_1 F_0) \cos \omega t + \frac{A^3}{4} \cos 3\omega t = 0$$
(7.23)

<sup>531</sup> No secular terms in  $u_1$  requires

$$\omega_1 A + \frac{3}{4} a_1 \beta A^3 - a_1 F_0 = 0.$$
(7.24)

If the first-order approximation is sufficient, then we set p = 1 and from (7.16) and (7.17) we have:

$$\alpha = \omega^2 + \omega_1, \tag{7.25}$$

$$1 = a_1$$
. (7.26)

From Eqs. (7.24), (7.25), (7.26) we obtain;

$$\omega^2 = \sqrt{\alpha + \frac{3}{4}\beta A^2 - \frac{F_0}{A}} \tag{7.27}$$

If we assume  $\alpha = \omega_n^2$ ,  $\beta = \mu$ , we have:

$$\omega_{PEM} = \sqrt{\omega_n^2 + \frac{3}{4}\mu A^2 - \frac{F_0}{A}}$$
(7.28)

<sup>536</sup> The same result was obtained in [162].

#### 537

## 538 Example 2

 $_{539}$  Consider the following nonlinear oscillator [46, 132]:

$$\ddot{u} + \frac{u^3}{1+u^2} = 0, \quad u(0) = A, \ \dot{u}(0) = 0$$
 (7.29)

540 We rewrite it in the form

$$\ddot{u} + 0.\,u + 1.\ddot{u}u^2 + 1.u^3 = 0. \tag{7.30}$$

Assume that the solution can be expressed as a power series in an artificial parameter p:

$$u = u_0 + p \, u_1 + p^2 u_2 + \dots \tag{7.31}$$

<sup>542</sup> Where p is a bookkeeping parameter. We assume that the coefficients 0 and 1 on the left <sup>543</sup> side of Eq. (7.31) can be respectively expanded into a series in p

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$$0 = \omega^2 + p \,\omega_1 + p^2 \omega_2 + \dots \tag{7.32}$$

$$1 = a_1 p + a_2 p^2 + \dots (7.33)$$

$$1 = b_1 p + b_2 p^2 + \dots (7.34)$$

Substituting Eqs. (7.32), (7.33) and (7.34) into Eq. (7.30) and equating the terms with the identical powers of p, we have

$$p^{0}: \ddot{u}_{0} + \omega^{2} u_{0} = 0, \quad u_{0}(0) = A \quad , \ \dot{u}_{0}(0) = 0,$$

$$(7.35)$$

$$p^{1}: \ddot{u}_{1} + \omega^{2}u_{1} + \omega_{1}u_{0} + a_{1}u_{0} + a_{1}\ddot{u}_{0}u_{0}^{2} + b_{1}u_{0}^{3} = 0, \quad u_{1}(0) = 0 \quad , \ \dot{u}_{1}(0) = 0, \quad (7.36)$$

The solution of Eq. (7.35) can be easily obtained

$$u_0 = A\cos\omega t \tag{7.37}$$

Substituting the result into Eq. (7.36), we have:

$$p^{1}: \ddot{u}_{1} + \omega^{2}u_{1} + \left(\omega_{1}A + \frac{3}{4}b_{1}A^{3} - \frac{3}{4}a_{1}\omega^{2}A^{3}\right)\cos\left(\omega t\right) + \frac{1}{4}A^{3}\left(b_{1} - a_{1}\omega^{2}\right)\cos(3\omega t) = 0.$$
(7.38)

<sup>548</sup> Using Fourier series expansion, we have

549 No secular terms in  $u_1$  requires

$$\omega_1 A + \frac{3}{4} b_1 A^3 - \frac{3}{4} a_1 \omega^2 A^3 = 0.$$
(7.39)

If the first-order approximation is sufficient, then we set p = 1 and from (7.32) and (7.33) we have

$$0=\omega^2+\omega_1\tag{7.40}$$

$$1 = a_1.$$
 (7.41)

$$1 = b_1.$$
 (7.42)

From Eqs. (7.39), (7.40), (7.41) and (7.42), we have:

$$\omega_{PEM} = \sqrt{\frac{3A^2}{4+3A^2}}$$
(7.43)

553 Which agrees well with the exact solution The obtained frequency is valid for all  $0 < A < \infty$ .

Α	$\omega_{PEM}$	$\omega_{Exact}$	$\frac{\omega_{PEM} - \omega_{Exact}}{\omega_{Exact}} \times 100$
0.05	0.04232	0.04326	2.172908
0.1	0.08439	0.08628	2.190542
0.5	0.38737	0.39736	2.514093
1	0.63678	0.65465	2.729703
5	0.96698	0.97435	0.756402
10	0.99092	0.9934	0.249648

Table 7.1 Comparison of approximate and exact frequencies[73].

Which has an excellent agreement with the exact one for all  $0 < A < \infty [132]$ .

## 554 8 VARIATIONAL APPROACH (VA)

The study of nonlinear oscillators is an interest for many researchers, because there are many 555 practical engineering components consisting of vibrating systems that can be modeled using 556 oscillatory systems. Nonlinear analytical techniques for solving nonlinear problems have been 557 dominated by different methods of investigation of these problems which appeared in numerous 558 domains of physics and engineering. Overview of the literary texts with multiple mentions 559 has been given by many wordsmiths utilizing miscellaneous analytical methods for solving 560 nonlinear oscillation systems. Various variational methods have made, and will continue to 561 make, an impact in key areas for science and technology development. The method was 562 proposed by He in 2007[107]. He suggested a new variational method which is very effective 563 for nonlinear oscillators. The application of this method widely used in many scientific papers 564 [7, 16, 18, 21, 71, 119, 121, 135, 143, 151, 152, 154, 169, 175, 212].565

#### 566 8.1 Basic idea of Variational Approach

<sup>567</sup> He suggested a variational approach which is different from the known variational methods in <sup>568</sup> open literature [107]. Hereby we give a brief introduction of the method:

$$u'' + f(u) = 0 \tag{8.1}$$

<sup>569</sup> Its variational principle can be easily established utilizing the semi-inverse method:

$$J(u) = \int_0^{T/4} \left( -\frac{1}{2} u'^2 + F(u) \right) dt$$
(8.2)

Where T is period of the nonlinear oscillator,  $\partial F / \partial u = f$ . Assume that its solution can be expressed as

$$u(t) = A\cos(\omega t) \tag{8.3}$$

<sup>572</sup> Where A and  $\omega$  are the amplitude and frequency of the oscillator, respectively. Substituting <sup>573</sup> Eq.(8.3) into Eq.(8.2) results in:

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$$J(A,\omega) = \int_0^{T/4} \left( -\frac{1}{2} A^2 \omega^2 \sin^2 \omega t + F(A\cos\omega t) \right) dt$$
  
=  $\frac{1}{\omega} \int_0^{\pi/2} \left( -\frac{1}{2} A^2 \omega^2 \sin^2 t + F(A\cos t) \right) dt$  (8.4)  
=  $-\frac{1}{2} A^2 \omega \int_0^{\pi/2} \sin^2 t dt + \frac{1}{\omega} \int_0^{\pi/2} F(A\cos t) dt$ 

<sup>574</sup> Applying the Ritz method, we require:

$$\frac{\partial J}{\partial A} = 0 \tag{8.5}$$

$$\frac{\partial J}{\partial \omega} = 0 \tag{8.6}$$

575 But with a careful inspection, for most cases we find that

$$\frac{\partial J}{\partial \omega} = -\frac{1}{2}A^2 \int_0^{\pi/2} \sin^2 t dt - \frac{1}{\omega^2} \int_0^{\pi/2} F(A\cos t) dt < 0$$
(8.7)

Thus, we modify conditions Eq. (8.5) and Eq. (8.6) into a simpler form:

$$\frac{\partial J}{\partial \omega} = 0 \tag{8.8}$$

577 From which the relationship between the amplitude and frequency of the oscillator can be 578 obtained.

## 579 8.2 Application of Variational Approach

## 580 Example 1

We consider the physical model of nonlinear equation in the following figure with  $F(t) = F_0 \sin \omega_0 t$ , indicated in Fig.8.1.

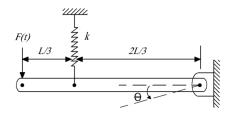


Figure 8.1 The physical model of nonlinear equation.

583 The motion equation is:

$$\ddot{\theta} + \frac{4k}{3m}\sin\theta - \frac{3F_0}{ml}\sin\omega_0 t = 0, \qquad \theta(0) = A \quad , \qquad \dot{\theta}(0) = 0$$
 (8.9)

This equation is as known as Mathieu equation or the system with dependent coefficients to time. In which  $\theta$  and t are generalized dimensionless displacements and time variables, respectively. And consider  $F = \frac{4}{3} \frac{k}{m}$  as constant.

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The approximation  $sin(\theta) = \theta - (1/6)\theta^3 + (1/120)\theta^5$  is used.

Its variational formulation can be readily obtained Eq. (8.9) as follows:

$$J(\theta) = \int_0^t \left(\frac{1}{2}\ddot{\theta}^2 + \frac{2}{3}\frac{k}{m}\theta^2 - \frac{1}{18}\frac{k}{m}\theta^4 + \frac{1}{540}\frac{k}{m}\theta^6 - \frac{3F_0\sin(\omega_0 t)}{ml}\theta\right)dt$$
(8.10)

Choosing the trial function  $\theta(t) = A \cos(\omega t)$  into Eq.(8.10) we obtain:

$$J(A) = \int_0^{T/4} \left( \begin{array}{c} \frac{1}{2} A^2 \omega^2 \sin^2(\omega t) + \frac{2}{3} \frac{k}{m} A^2 \cos^2(\omega t) - \frac{1}{18} \frac{k}{m} A^4 \cos^4(\omega t) \\ + \frac{1}{540} \frac{k}{m} A^6 \cos^6(\omega t) - \frac{3F_0 \sin(\omega_0 t)}{ml} A \cos(\omega t) \end{array} \right) dt$$
(8.11)

590 The stationary condition with respect to A leads to:

$$\frac{\partial J}{\partial A} = \int_0^{T/4} \left( \begin{array}{c} A\omega^2 \sin^2(\omega t) + \frac{4}{3}\frac{k}{m}A\cos^2(\omega t) - \frac{2}{9}\frac{k}{m}A^3\cos^4(\omega t) \\ + \frac{1}{90}\frac{k}{m}A^5\cos^6(\omega t) - \frac{3F_0\sin(\omega_0 t)}{ml}\cos(\omega t) \end{array} \right) dt = 0$$
(8.12)

591 Or

$$\frac{\partial J}{\partial A} = \int_0^{\pi/2} \left( \begin{array}{c} A\omega^2 \sin^2 t + \frac{4}{3} \frac{k}{m} A \cos^2 t - \frac{2}{9} \frac{k}{m} A^3 \cos^4 t \\ + \frac{1}{90} \frac{k}{m} A^5 \cos^6 t - \frac{3F_0 \sin(\omega_0 t)}{ml} \cos t \end{array} \right) dt = 0$$
(8.13)

Solving Eq.(8.13), according to  $\omega$ , we have:

$$\omega^{2} = \frac{\int_{0}^{\frac{\pi}{2}} \left(\frac{4}{3}\frac{k}{m}A\cos^{2}t - \frac{2}{9}\frac{k}{m}A^{3}\cos^{4}t + \frac{1}{90}\frac{k}{m}A^{5}\cos^{6}t - \frac{3F_{0}\sin(\omega_{0}t)}{ml}\cos t\right)dt}{\int_{0}^{\frac{\pi}{2}}A\sin^{2}t\,dt}$$
(8.14)

593 Then we have:

$$\omega_{VAM} = \frac{1}{12} \sqrt{\frac{1728F_0 \sin\left(\frac{1}{2}\pi\omega_0\right) - 1728F_0\omega_0 + kAl\pi\left(\omega_0^2 - 1\right)\left(192 + A^4 - 24A^2\right)}{(m\omega_0^2 - m)lA\pi}}$$
(8.15)

According to Eqs. (8.3) and (8.15), we can obtain the following approximate solution:

$$\theta(t) = A \cos\left(\frac{1}{12}\sqrt{\frac{1728F_0 \sin\left(\frac{1}{2}\pi\omega_0\right) - 1728F_0\omega_0 + kAl\pi\left(\omega_0^2 - 1\right)\left(192 + A^4 - 24A^2\right)}{(m\omega_0^2 - m)lA\pi}}t\right) \quad (8.16)$$

We compared the numerical solution and variational approach method for different parameters:

Figure 8.2 represents a comparison of analytical solution of  $\theta(t)$  based on time with the numerical solution and figure 8.3 shows comparison of analytical solution of  $d\theta/dt$  based on time with the numerical solution.

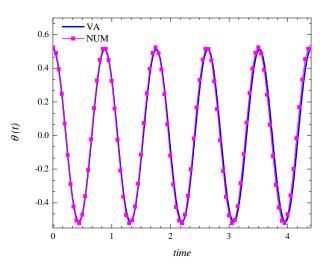


Figure 8.2 Comparison of analytical solution of  $\theta$  based on time with the numerical solution for L=0.5 m , m=20 kg , k=800 N/m , F\_0=1N ,  $\omega_0{=}2$  rad/sec , A= $\pi/6.$ 

600

## 601 Example 2

In this example, we consider the following nonlinear oscillator [71]:

$$\left(\frac{1}{12}l^2 + r^2\theta^2\right)\ddot{\theta} + r^2\theta\dot{\theta}^2 + rg\theta\cos\left(\theta\right) = 0$$
(8.17)

603 With the boundary conditions of:

$$\theta(0) = A, \quad \dot{\theta}(0) = 0$$
 (8.18)

In order to apply the variational approach method to solve the above problem, the approximation  $\cos \theta \approx 1 - \frac{1}{2}\theta^2 + \frac{1}{24}\theta^4$  is used.

606 Its variational formulation is:

$$J(\theta) = \int_0^{T/4} \left( -\frac{1}{24} l^2 \dot{\theta}^2 - \frac{1}{2} r^2 \theta^2 \dot{\theta}^2 + \frac{1}{2} r g \theta^2 - \frac{1}{8} r g \theta^4 + \frac{1}{144} g r \theta^6 \right) dt$$
(8.19)

607 Choosing the trial function  $\theta(t) = A\cos(\omega t)$  into Eq.(8.19) we obtain

$$J(A, \omega) = \int_{0}^{T/4} \left( \begin{array}{c} -\frac{1}{24}l^{2} \left(A \omega \sin(\omega t)\right)^{2} - \frac{1}{2}r^{2} \left(A \cos(\omega t)\right)^{2} \left(A \omega \sin(\omega t)\right)^{2} \\ +\frac{1}{2}rg \left(A \cos(\omega t)\right)^{2} - \frac{1}{8}rg \left(A \cos(\omega t)\right)^{4} + \frac{1}{144}gr \left(A \cos(\omega t)\right)^{6} \end{array} \right) dt$$
(8.20)

 $_{608}$  The stationary condition with respect to A reads:

$$\frac{\partial J}{\partial A} = \int_0^{T/4} \left( \begin{array}{c} -\frac{1}{12} l^2 \omega^2 A \sin^2(\omega t) - 2 r^2 \omega^2 A^3 \sin^2(\omega t) \cos^2(\omega t) \\ + r g A \cos^2(\omega t) - \frac{1}{2} r g A^3 \cos^4(\omega t) + \frac{1}{24} r g A^5 \cos^6(\omega t) \end{array} \right) dt = 0$$
(8.21)

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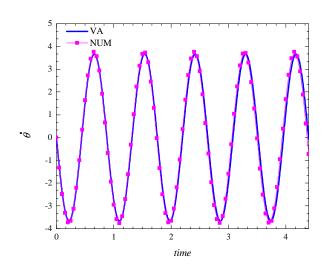


Figure 8.3 Comparison of analytical solution of  $\theta$  based on time with the numerical solution for L=0.5 m , m=20 kg , k=800 N/m , F\_0=1N ,  $\omega_0=2$  rad/sec , A= $\pi/6.$ 

609 Or

$$\frac{\partial J}{\partial A} = \int_0^{\pi/2} \left( \begin{array}{c} -\frac{1}{12} l^2 A \sin^2 t \, \omega^2 - 2 \, r^2 \, \omega^2 \, A^3 \sin^2 t \cos^2 t \\ + r \, g \, A \cos^2 t - \frac{1}{2} r \, g \, A^3 \cos^4 t + \frac{1}{24} r \, g \, A^5 \cos^6 t \end{array} \right) \, dt = 0 \tag{8.22}$$

610 Then we have ;

$$\omega^{2} = \frac{\int_{0}^{\pi/2} \left( r g A \cos^{2} t - \frac{1}{2} r g A^{3} \cos^{4} t + \frac{1}{24} r g A^{5} \cos^{6} t \right) dt}{\int_{0}^{\pi/2} \left( \frac{1}{12} l^{2} A \sin^{2} t + 2 r^{2} A^{3} \sin^{2} t \cos^{2} t \right) dt}$$
(8.23)

Solving Eq. (8.23), according to  $\omega$ , we have:

$$\omega = \frac{1}{4}\sqrt{\frac{rg \left(192 - 72A^2 + 5A^4\right)}{6A^2r^2 + l^2}} \tag{8.24}$$

<sup>612</sup> Hence, the approximate solution can be readily obtained:

$$\theta(t) = A\cos\left(\frac{1}{4}\sqrt{\frac{rg \left(192 - 72A^2 + 5A^4\right)}{6A^2r^2 + l^2}} t\right)$$
(8.25)

For comparison of the approximate solution, frequency obtained from solution of nonlinear equation with the Variational Approach is:

$$\omega_{VA} = \frac{\sqrt{6}}{12} \sqrt{\frac{r g \left(288 - 108A^2 + 7A^4\right)}{6A^2 r^2 + l^2}} \tag{8.26}$$

<sup>615</sup> The numerical solution (with Runge-Kutta method of order 4) for nonlinear equation is:

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$$\theta = y \qquad \qquad \theta(0) = A 
\dot{y} = -\frac{r^2 \theta u^2 + r g \theta \cos(\theta)}{\frac{1}{12} l^2 + r^2 \theta^2} \qquad \qquad y(0) = 0$$

$$(8.27)$$

<sup>616</sup> We compared the numerical solution with the variational approach in Figs 8.4 and 8.5:

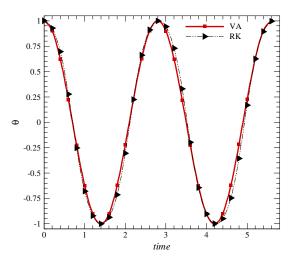


Figure 8.4 Comparison of ( $\theta$ )of the VA solution and Runge-Kutta solution I=2.5, r=0. 5, g=10 , A=1

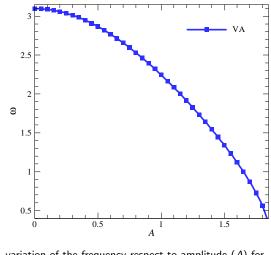


Figure 8.5 variation of the frequency respect to amplitude (A) for I=2.5, r=0. 5, g=10

Figs. 8.4 shows the displacement of the system for l=2.5, r=0.5, g=10, A=1.

Fig.8.5 represents the variation of frequency various parameters of amplitude (A).Comparing with the numerical results, it has been shown that the results of VA require smaller computational effort and only a first-order approximation of the VA leads to high accurate solutions.

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621

#### Example 3 622

The mathematical pendulum is considered again as an example. The differential equation 623 governing for the free oscillation of the mathematical pendulum is given by [138] 624

$$\ddot{\theta} - \Omega^2 \cos\left(\theta\right) \sin\left(\theta\right) + \frac{g}{r} \sin\left(\theta\right) = 0 \tag{8.28}$$

With the boundary conditions of: 625

$$\theta(0) = A, \quad \dot{\theta}(0) = 0$$
 (8.29)

In order to apply the variational approach method to solve the above problem, the approx-626 imation  $\cos\theta \approx 1 - \frac{1}{2}\theta^2 + \frac{1}{24}\theta^4$  and  $\sin\theta \approx \theta - \frac{1}{6}\theta^3$  is used. Its variational formulation can be readily obtained as follows: 627

628

$$J(\theta) = \int_0^{T/4} \left( -\frac{1}{2}\dot{\theta}^2 - \frac{1}{2}\Omega^2\theta^2 + \frac{1}{6}\Omega^2\theta^4 - \frac{1}{48}\Omega^2\theta^6 + \frac{1}{1152}\Omega^2\theta^8 + \frac{1}{2}\frac{g}{r}\theta^2 - \frac{1}{24}\frac{g}{r}\theta^4 \right) dt \quad (8.30)$$

629

Choosing the trial function 
$$\theta(t) = A\cos(\omega t)$$
 into Eq.(8.31) we obtain

$$J(A, \omega) = \int_{0}^{T/4} \begin{pmatrix} -\frac{1}{2} \left(A \omega \sin(\omega t)\right)^{2} - \frac{1}{2} \Omega^{2} \left(A \cos(\omega t)\right)^{2} + \frac{1}{6} \Omega^{2} \left(A \cos(\omega t)\right)^{4} \\ -\frac{1}{48} \Omega^{2} \left(A \cos(\omega t)\right)^{6} + \frac{1}{1152} \Omega^{2} \left(A \cos(\omega t)\right)^{8} + \left(\frac{1}{2}\right) \frac{g}{r} \left(A \cos(\omega t)\right)^{2} \\ -\left(\frac{1}{24}\right) \frac{g}{r} \left(A \cos(\omega t)\right)^{4} \end{pmatrix} dt$$

$$(8.31)$$

The stationary condition with respect to A reads: 630

$$\frac{\partial J}{\partial A} = \int_{0}^{T/4} \left( \begin{array}{c} -A\,\omega^{2}sin^{2}\left(\omega t\right) - \Omega^{2}Acos^{2}\left(\omega t\right) + \frac{2}{3}\Omega^{2}A^{3}cos^{4}\left(\omega t\right) - \frac{1}{8}\Omega^{2}A^{5}cos^{6}\left(\omega t\right) \\ + \frac{1}{144}\Omega^{2}A^{7}cos^{8}\left(\omega t\right) + \frac{g}{r}Acos^{2}\left(\omega t\right) - \frac{1}{6}\frac{g}{r}A^{3}cos^{4}\left(\omega t\right) \end{array} \right) dt = 0$$
(8.32)

631

$$\frac{\partial J}{\partial A} = \int_0^{\pi/2} \left( \begin{array}{c} -A\,\omega^2 \sin^2 t - \Omega^2 A \cos^2 t + \frac{2}{3}\Omega^2 A^3 \cos^4 t - \frac{1}{8}\Omega^2 A^5 \cos^6 t \\ +\frac{1}{144}\,\Omega^2 A^7 \cos^8 t + \frac{g}{r}\,A \cos^2 t - \frac{1}{6}\frac{g}{r}A^3 \cos^4 t \end{array} \right) \, dt = 0 \tag{8.33}$$

Then we have; 632

Or

$$\omega^{2} = \frac{\int_{0}^{\pi/2} \left(\begin{array}{c} -\Omega^{2}A\cos^{2}t + \frac{2}{3}\Omega^{2}A^{3}\cos^{4}t - \frac{1}{8}\Omega^{2}A^{5}\cos^{6}t + \frac{1}{144}\Omega^{2}A^{7}\cos^{8}t \\ + \frac{g}{r}A\cos^{2}t - \frac{1}{6}\frac{g}{r}A^{3}\cos^{4}t \\ A\int_{0}^{\pi/2}\sin^{2}t \, dt \end{array}\right) dt$$
(8.34)

Solving Eq. (8.34), according to  $\omega$ , we have: 633

$$\omega = \frac{1}{96}\sqrt{-9216\,\Omega^2 + 4608\,\Omega^2 A^2 - 720\,\Omega^2 A^4 + 35\,\Omega^2 A^6 + 9216\,\frac{g}{r} - 1152\,\frac{g}{r}A^2} \tag{8.35}$$

634

Hence, the approximate solution can be readily obtained:

$$\theta\left(t\right) = A\cos\left(\frac{1}{96}\sqrt{-9216\,\Omega^2 + 4608\,\Omega^2 A^2 - 720\,\Omega^2 A^4 + 35\,\Omega^2 A^6 + 9216\,\frac{g}{r} - 1152\,\frac{g}{r}A^2}\,t\right)\,(8.36)$$

To compare the results of VA, frequency obtained from VA is: 635

$$\omega_{VA} = \frac{\sqrt{6}}{96} \sqrt{-1536\,\Omega^2 + 768\Omega^2\,A^2 - 112\,\Omega^2\,A^4 + 5\,\Omega^2\,A^6 + 1536\,\frac{g}{r} - 192\,\frac{g}{r}A^2} \tag{8.37}$$

The numerical solution (with Runge-Kutta Method of order 4) for nonlinear equation is: 636

$$\dot{\theta} = y\theta(0) = A$$
  
$$\dot{y} = \Omega^2 \cos\left(\theta\right) \sin\left(\theta\right) - \frac{g}{r} \sin\left(\theta\right) y(0) = 0$$
(8.38)

Some comparisons are presented to show the accuracy of the method. Figures 8.6 and 8.7 637 show comparison of analytical solution of  $\theta$  and  $\dot{\theta}$  based on time with the numerical solution. 638 The variation of amplitude A on the frequency of the system is shown in figure 8.8. It can 639 be approved that VA is powerful in finding analytical solutions for a wide class of nonlinear 640 problems. 641

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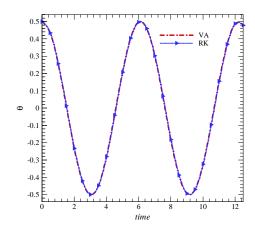


Figure 8.6 Comparison of displacement ( $\theta$ ) of the VA solution and Runge-kutta solution for  $\Omega = 1$ , r= 5, g=10, A=0.5

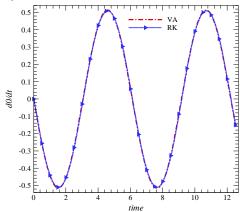


Figure 8.7 Comparison of velocity  $(\dot{\theta})$  of the VA solution and Runge-kutta solution for  $\Omega$  =1, r= 5, g=10, A=0.5

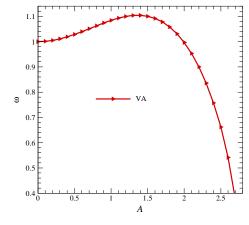


Figure 8.8 variation of the frequency respect to amplitude (A)for  $\Omega$  =1, r= 5, g=10

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## <sup>642</sup> 9 IMPROVED AMPLITUDE-FREQUENCY FORMULATION (IAFF)

Most of engineering problems, especially some oscillation equations are nonlinear, and in most 643 cases, it is difficult to solve such equations, especially analytically. One of the well-known 644 methods to solve nonlinear problems is improved amplitude frequency formulation (IAFF). He 645 in his previous review paper [100] in traduced the Ancient Chinese method including improved 646 amplitude frequency formulation (IAFF). Geng and Cai [74] found the method to be very 647 effective in solving strongly nonlinear oscillators. To illustrate the basic idea of the method, 648 we consider an algebraic equation, this method applied correctly in many open literatures 649 [1, 38, 52, 72, 106, 108, 109, 163-165, 182, 183, 200, 211, 214-216].650

## 651 9.1 Basic idea of Improved Amplitude-Frequency Formulation

<sup>652</sup> We consider a generalized nonlinear oscillator in the form [109]:

$$u'' + f(u) = 0, u(0) = A, u'(0) = 0,$$
(9.1)

<sup>653</sup> We use two following trial functions

$$u_1(t) = A\cos(\omega_1 t), \tag{9.2}$$

654 And

$$u_2(t) = A\cos(\omega_2 t), \tag{9.3}$$

655 The residuals are

$$R_1(\omega t) = -A\omega_1^2 \cos(\omega_1 t) + f(A\cos(\omega_1 t)), \qquad (9.4)$$

656 And

$$R_2(\omega t) = -A\omega_2^2 \cos(\omega_2 t) + f(A\cos(\omega_2 t)), \qquad (9.5)$$

<sup>657</sup> The original Frequency-amplitude formulation reads :

$$\omega^2 = \frac{\omega_1^2 R_2 - \omega_2^2 R_1}{R_2 - R_1},\tag{9.6}$$

<sup>658</sup> He used the following formulation [100] and Geng and Cai improved the formulation by <sup>659</sup> choosing another location point [74].

$$\omega^2 = \frac{\omega_1^2 R_2(\omega_2 t = 0) - \omega_2^2 R_1(\omega_1 t = 0)}{R_2 - R_1},$$
(9.7)

<sup>660</sup> This is the improved form by Geng and Cai.

$$\omega^{2} = \frac{\omega_{1}^{2} R_{2}(\omega_{2}t = \pi/3) - \omega_{2}^{2} R_{1}(\omega_{1}t = \pi/3)}{R_{2} - R_{1}},$$
(9.8)

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The point is: $\cos(\omega_1 t) = \cos(\omega_2 t) = k$ 

Substituting the obtained  $\omega$  into  $u(t) = A\cos(\omega t)$ , we can obtain the constant  $k \sin^2 \omega^2$ equation in order to have the frequency without irrelevant parameter.

<sup>664</sup> To improve its accuracy, we can use the following trial function when they are required.

$$u_1(t) = \sum_{i=1}^m A_i \cos(\omega_i t), and \quad u_2(t) = \sum_{i=1}^m A_i \cos(\Omega_i t)$$
(9.9)

665 OT

$$u_{1}(t) = \frac{\sum_{i=1}^{m} A_{i} \cos(\omega_{i}t)}{\sum_{j=1}^{m} B_{j} \cos(\omega_{j}t)}, and \quad u_{2}(t) = \frac{\sum_{i=1}^{m} A_{i} \cos(\Omega_{i}t)}{\sum_{j=1}^{m} B_{j} \cos(\Omega_{j}t)},$$
(9.10)

But in most cases because of the sufficient accuracy, trial functions are as follow and just the first term:

$$u_1(t) = A\cos t, and \ u_2(t) = a\cos(\omega t) + (A-a)\cos(\omega t),$$
 (9.11)

668 And

$$u_1(t) = A\cos t, and \quad u_2(t) = \frac{A(1+c)\cos(\omega t)}{1+c\cos(2\omega t)},$$
(9.12)

 $_{669}$  Where *a* and *c* are unknown constants. In addition we can set:

 $\cos t = k \text{ in } u_1, \text{ and } \cos (\omega t) = k \text{ in } u_2$ 

## 671 9.2 Application of Improved Amplitude-Frequency Formulation

<sup>672</sup> In this section, three practical examples are illustrated to show the applicability, accuracy and <sup>673</sup> effectiveness of the proposed approach.

674

675 Example1

A two-mass system connected with linear and nonlinear stiffnesses. Consider the two-mass system model as shown in Fig. (9.1). The equation of motion is given as [44];

$$m\ddot{x} + k_1(x-y) + k_2(x-y)^3 = 0$$
  

$$m\ddot{y} + k_1(y-x) + k_2(y-x)^3 = 0$$
(9.13)

678 With initial conditions

$$\begin{aligned} x(0) &= X_0, \quad \dot{x}(0) = 0, \\ y(0) &= Y_0, \quad \dot{y}(0) = 0, \end{aligned}$$
 (9.14)

Where double dots in Eq. (9.13) denote double differentiation with respect to time t,  $k_1$ and  $k_2$  are linear and nonlinear coefficients of the spring stiffness, respectively. Dividing Eq. (9.13) by mass m yields

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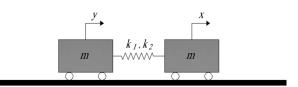


Figure 9.1 Two masses connected by linear and nonlinear stiffnesses.

$$\ddot{x} + \frac{k_1}{m}(x-y) + \frac{k_2}{m}(x-y)^3 = 0 \ddot{y} + \frac{k_1}{m}(y-x) + \frac{k_2}{m}(y-x)^3 = 0$$
(9.15)

Introducing intermediate variables u and  $\nu$  as follows [127]:

$$x \coloneqq u \tag{9.16}$$

$$y - x \coloneqq \nu \tag{9.17}$$

And transforming Eqs. (9.16) and (9.17) yields

$$\ddot{u} - \alpha \nu - \beta \nu^3 = 0 \tag{9.18}$$

$$\ddot{\nu} + \ddot{u} + \alpha \nu + \beta \nu^3 = 0 \tag{9.19}$$

Where  $\alpha = k_1/m$  and  $\alpha = k_2/m$  Eq. (9.18) is rearranged as follows:

$$\ddot{u} = \alpha \nu - \beta \nu^3. \tag{9.20}$$

Substituting Eq. (6.20) into Eq. (9.19) yields

$$\ddot{\nu} + 2\alpha\nu + 2\beta\nu^3 = 0 \tag{9.21}$$

686 With initial conditions

$$\nu(0) = y(0) - x(0) = Y_0 - X_0 = A, \quad \dot{\nu}(0) = 0$$
(9.22)

<sup>687</sup> We use trial functions, as follows:

$$\nu_1(t) = A\cos t,\tag{9.23}$$

688 And

$$\nu_2(t) = A\cos(2t), \tag{9.24}$$

Respectively, the residual equations are:

$$R_1(t) = A\cos(t) \left( -1 + 2\alpha + 2\beta A^2 \cos^2(t) \right), \qquad (9.25)$$

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690 And

$$R_2(t) = 2A\cos(2t)\left(-2 + \alpha + \beta A^2 \cos^2(2t)\right), \tag{9.26}$$

691 Considering  $\cos t_1 = \cos 2t_2 = k$ , we have:

$$\omega^2 = \frac{\omega_1^2 R_2 - \omega_2^2 R_1}{R_2 - R_1} = 2\alpha + 2\beta k^2 A^2, \qquad (9.27)$$

We can rewrite  $\nu(t) = A\cos(\omega t)$  in the form:

$$\nu(t) = A\cos\left(\sqrt{2\alpha + 2\beta k^2 A^2} t\right),\tag{9.28}$$

<sup>693</sup> In view of the approximate solution, we can rewrite the main equation in the form:

$$\ddot{\nu} + (2\alpha + 2\beta k^2 A^2)\nu = (2\beta k^2 A^2)\nu - 2\beta \nu^3$$
(9.29)

If by any chance  $\nu(t) = A \cos\left(\sqrt{2\alpha + 2\beta k^2 A^2} t\right)$  is the exact solution, then the right side of Eq. (9.29) vanishes completely. Considering our approach which is just an approximation one, we set:

$$\int_{0}^{T/4} \left( 2\beta k^2 A^2 \nu - 2\beta \nu^3 \right) \cos \omega t \, dt = 0, T = 2\pi/\omega$$
(9.30)

<sup>697</sup> Considering the term  $\nu(t) = A \cos\left(\sqrt{2\alpha + 2\beta k^2 A^2} t\right)$  and substituting the term to Eq. (9.30) <sup>698</sup> and solving the integral term, we have:

$$k = \frac{1}{2}\sqrt{3} \quad , \tag{9.31}$$

So, substituting Eq. (9.31) into Eq. (9.27), we have:

$$\omega_{IAFF} = \frac{1}{2}\sqrt{8\alpha + 6\beta A^2} \tag{9.32}$$

Table 9.1 Comparison of nonlinear frequencies in Eq. (9.32) with e exact solution

Constants					Results			
m	$k_1$	$k_2$	$X_0$	$Y_0$	IAFF solution $\omega$	Exact solution $\omega_{Exact}$	Relative error %	
1	5	5	5	1	11.4018	11.1921	1.873643	
1	1	1	10	-5	18.4255	18.0302	2.192433	
1	10	5	20	25	14.4049	14.1514	1.791342	
5	10	10	20	30	17.4356	17.0672	2.158526	
10	50	-0.01	-20	40	2.1448	2.0795	3.140178	

The first-order approximate solutions is of a high accuracy and the percentage error improves significantly from lower order to higher order analytical approximations for different parameters and initial amplitudes. Hence, it is concluded that excellent agreement with the

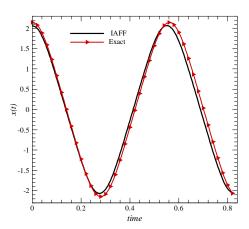


Figure 9.2 Comparison of the analytical approximates with the exact solution [44] for  $k_1 = 5, k_2 = 5$ , with x(0) = 5

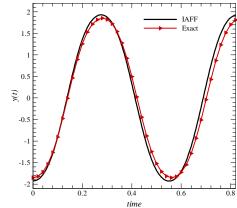


Figure 9.3 Comparison of the analytical approximates with the exact solution [44] for  $k_1 = 5, k_2 = 5$ , with y(0) = 1

exact so. Tables 9.1 gives the comparison of obtained results with the exact solutions for different m,  $k_1$ ,  $k_2$ , and initial conditions. The maximum relative error between the IAFF results and exact results is 3.140178%. A comparison of the time history oscillatory displacementresponse for the two masses with exact solutions presented in Figs. (9.2) to (9.5).

#### 707

## 708 Example 2

Consider a two-mass system connected with linear and nonlinear springs and fixed to a body at two ends as shown in Fig. (9.6)[43].

$$m\ddot{x} + k_1 x + k_2 (x - y) + k_3 (x - y)^3 = 0$$
  

$$m\ddot{y} + k_1 x + k_2 (y - x) + k_3 (y - x)^3 = 0$$
(9.33)

711 With initial conditions

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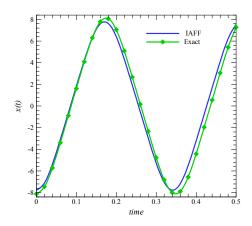


Figure 9.4 Comparison of the analytical approximates with the exact solution [44] for  $k_1 = 5$ ,  $k_2 = 5$ , with x(0) = 10

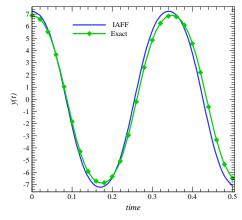


Figure 9.5 Comparison of the analytical approximates with the exact solution [44] for  $k_1 = 5$ ,  $k_2 = 5$ , with y(0) = -5

$$\begin{aligned} x(0) &= X_0, \quad \dot{x}(0) = 0, \\ y(0) &= Y_0, \quad \dot{y}(0) = 0, \end{aligned}$$
(9.34)

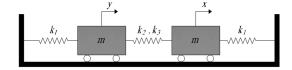


Figure 9.6 Two-mass system connected with the fixed bodies.

<sup>712</sup> Where double dots in Eq. (9.33) denote double differentiation with respect to time,  $k_1$  and <sup>713</sup>  $k_2$  are linear and nonlinear coefficients of the spring stiffness and  $k_3$  is the nonlinear coefficient <sup>714</sup> of the spring stiffness. Dividing Eq. (9.33) by mass m yields

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$$\ddot{x} + \frac{k_1}{m}x + \frac{k_2}{m}(x-y) + \frac{k_3}{m}(x-y)^3 = 0$$
  
$$\ddot{y} + \frac{k_1}{m}x + \frac{k_2}{m}(y-x) + \frac{k_3}{m}(y-x)^3 = 0$$
(9.35)

Like in Example1, transforming the above equations using intermediate variables in Eqs. (9.16) and (9.17) yields;

$$\ddot{u} + \alpha u - \beta \nu - \xi \nu^3 = 0 \tag{9.36}$$

$$\ddot{u} + \ddot{\nu} + \alpha u - \alpha \nu + \beta \nu + \xi \nu^3 = 0 \tag{9.37}$$

Where  $\alpha = k_1/m, \beta = k_2/m$  and  $\xi = k_3/m$ . Eq. (9.36) is rearranged as follows:

$$\ddot{u} = -\alpha u + \beta \nu + \xi \nu^3 \tag{9.38}$$

Substituting Eq. (9.38) into Eq. (9.37) yields

$$\ddot{\nu} + (\alpha + 2\beta)\nu + 2\xi\nu^3 = 0 \tag{9.39}$$

719 With initial conditions

$$\nu(0) = y(0) - x(0) = Y_0 - X_0 = A, \quad \dot{\nu}(0) = 0 \tag{9.40}$$

720 We use trial functions, as follows:

$$\nu_1(t) = A\cos t,\tag{9.41}$$

721 And

$$\nu_2(t) = A\cos(2t), \tag{9.42}$$

Respectively, the residual equations are:

$$R_1(t) = A\cos(t) \left( -1 + \alpha + 2\beta + 2\xi A^2 \cos^2(t) \right), \qquad (9.43)$$

723 And

$$R_2(t) = A\cos(2t) \left(-4 + \alpha + 2\beta + 2\xi A^2 \cos^2(2t)\right), \qquad (9.44)$$

Considering  $\cos t_1 = \cos 2t_2 = k$ , we have:

$$\omega^2 = \frac{\omega_1^2 R_2 - \omega_2^2 R_1}{R_2 - R_1} = \alpha + 2\beta + 2\xi k^2 A^2, \qquad (9.45)$$

We can rewrite  $\nu(t) = A \cos(\omega t)$  in the form:

$$\nu(t) = A\cos\left(\sqrt{\alpha + 2\beta + 2\xi k^2 A^2} t\right),\tag{9.46}$$

<sup>726</sup> In view of the approximate solution, we can rewrite the main equation in the form:

$$\ddot{\nu} + (\alpha + 2\beta + 2\xi k^2 A^2) \nu = (2\xi k^2 A^2) \nu - 2\xi \nu^3$$
(9.47)

<sup>727</sup> If by any chance Eq. (9.46) is the exact solution, then the right side of Eq. (9.47) vanishes <sup>728</sup> completely. Considering our approach which is just an approximation one, we set:

$$\int_{0}^{T/4} \left( 2\xi k^2 A^2 \nu - 2\xi \nu^3 \right) \cos \omega t \, dt = 0 \qquad T = 2\pi/\omega$$
(9.48)

<sup>729</sup> Considering the term  $\nu(t) = A \cos\left(\sqrt{2\alpha + 2\beta k^2 A^2} t\right)$  and substituting the term to Eq. (9.48) <sup>730</sup> and solving the integral term, we have:

$$k = \frac{1}{2}\sqrt{3} \ , \tag{9.49}$$

So, substituting Eq. (9.49) into Eq. (9.45), we have:

$$\omega_{IAFF} = \frac{1}{2}\sqrt{4\alpha + 8\beta + 6\xi A^2} \tag{9.50}$$

Table 9.2 Comparison of angular frequencies in Eq. (9.50) with exact solution.

Constants						Results			
m	$k_1$	$k_2$	$k_3$	$X_0$	$Y_0$	IAFF solution $\omega$	Exact solution $\omega_{Exact}$	Relative error	
1	1	1	1	5	1	5.1961	5.1078	1.728729	
1	1	1	5	5	10	13.8022	13.5121	2.146965	
1	25	20	-0.05	-10	10	1.8708	1.8413	1.602129	
5	10	20	30	-10	10	60.0833	58.7856	2.207513	
10	50	70	90	20	-40	220.4972	215.7113	2.21866	

Table 9.2 shows an excellent agreement of the IAFF and exact solutions. From the Figs. 9.7 to 9.10, motions of the systems are periodic motions and the amplitude of vibrations is function of the initial conditions. These expressions are valid for a wide range of vibration amplitudes and initial conditions. The proposed methods are quickly convergent and can also be readily generalized to two-degree-of-freedom oscillation systems with quadratic nonlinearity by combining the transformation technique.

#### 738

#### 739 Example 3

In order to assess the advantages and the accuracy of Improved Amplitude-frequency Formulation for solving nonlinear oscillator, we will consider the following nonlinear oscillator;

$$\ddot{u} + a\,u\dot{u}^2 + au\ddot{u} + \alpha_1 u + \alpha_2 u^3 + \alpha_3 u^5 = 0, \tag{9.51}$$

742 with the initial conditions of:

$$u(0) = A$$
,  $\dot{u}(0) = 0$ , (9.52)

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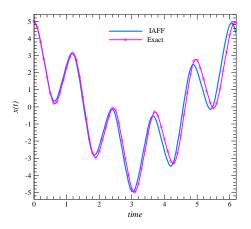


Figure 9.7 Comparison of the analytical approximates with the exact solution [43] for  $k_1 = 5, k_2 = 5, k_3 = 1 \text{ with } x(0) = 5$ 

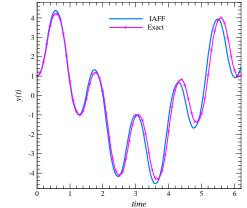


Figure 9.8 Comparison of the analytical approximates with the exact solution [43] for  $k_1 = 5, k_2 = 5, k_3 = 1 \text{ with } y(0) = 1$ 

#### 743 We use trial functions, as follows:

$$u_1(t) = A\cos t, \tag{9.53}$$

744 And

$$u_2(t) = A\cos(2t),$$
 (9.54)

<sup>745</sup> Respectively, the residual equations are:

$$R_1(t) = A\cos(t) \left(-2aA^2\cos^2(t) + aA^2 - 1 + \alpha_1 + \alpha_2 A^2\cos^2(t) + \alpha_3 A^4\cos^4(t)\right), \quad (9.55)$$

746 And

$$R_2(t) = A\cos(2t) \left(-8aA^2\cos^2(2t) + 4aA^2 - 4 + \alpha_1 + \alpha_2 A^2\cos^2(2t) + \alpha_3 A^4\cos^4(2t)\right), \quad (9.56)$$

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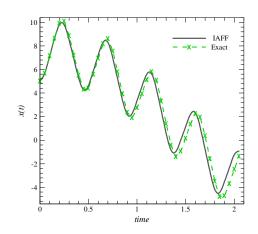


Figure 9.9 Comparison of the analytical approximates with the exact solution [43]for  $k_1 = 5$ ,  $k_2 = 5$ ,  $k_3 = 5$  with x(0) = 5

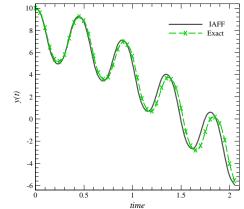


Figure 9.10 Comparison of the analytical approximates with the exact solution [43] for  $k_1 = 1, k_2 = 1, k_3 = 5$  with y(0) = 10

Considering  $\cos t = \cos 2t = k$ , we have:

$$\omega^{2} = \frac{\omega_{1}^{2}R_{2} - \omega_{2}^{2}R_{1}}{R_{2} - R_{1}} = \frac{\alpha_{1} + \alpha_{2}A^{2}k^{2} + \alpha_{3}A^{4}k^{4}}{2aA^{2}k^{2} - aA^{2} + 1},$$
(9.57)

<sup>748</sup> We can rewrite  $u(t) = A \cos(\omega t)$  in the form:

$$u(t) = A\cos\left(\sqrt{\frac{\alpha_1 + \alpha_2 A^2 k^2 + \alpha_3 f^4 k^4}{2aA^2 k^2 - aA^2 + 1}}t\right),\tag{9.58}$$

<sup>749</sup> In view of the approximate solution, we can rewrite the main equation in the form:

$$\ddot{u} + \frac{\alpha_1 + \alpha_2 A^2 k^2 + \alpha_3 f^4 k^4}{2aA^2 k^2 - aA^2 + 1} u = \frac{\alpha_1 + \alpha_2 A^2 k^2 + \alpha_3 f^4 k^4}{2aA^2 k^2 - aA^2 + 1} u - au\dot{u}^2 + u\ddot{u} - \alpha_1 u - \alpha_2 u^3 - \alpha_3 u^5,$$
(9.59)

If by any chance  $u(t) = A \cos \left( \sqrt{\frac{\alpha_1 + \alpha_2 A^2 k^2 + \alpha_3 A^4 k^4}{2aA^2 k^2 - aA^2 + 1}} t \right)$  is the exact solution, then the right side of Eq.(9.59) vanishes completely. Considering our approach which is just an approximation one, we set:

$$\int_{0}^{T} \left[ \begin{array}{c} \frac{\alpha_{1} + \alpha_{2} A^{2} k^{2} + \alpha_{3} f^{4} k^{4}}{2a A^{2} k^{2} - a A^{2} + 1} u \\ -a u \dot{u}^{2} + u \ddot{u} - \alpha_{1} u - \alpha_{2} u^{3} - \alpha_{3} u^{5} \end{array} \right] \cos(\omega t) dt = 0 \quad , \qquad T = \frac{2\pi}{\omega}, \tag{9.60}$$

Considering the term  $u(t) = A\cos(\omega t)$  and substituting the term to Eq. (9.61) and solving the integral term, we have:

$$\begin{aligned} k^{4} &= \frac{1}{16} \frac{1}{A^{4} \alpha_{3}^{2} (aA^{2}+2)^{2}} \left( \begin{array}{c} 5A^{4} \alpha_{3}a + 8\alpha_{1}a + 4A^{2} \alpha_{2}a - 4\alpha_{2} \\ &+ \left( \begin{array}{c} 5A^{8} \alpha_{3}^{2}a^{2} + 32A^{4} \alpha_{3}a^{2} \alpha_{1} + 16A^{6} \alpha_{3}a^{2} \alpha_{2} - 64A^{4} \alpha_{3}a \alpha_{2} + 64\alpha_{1}^{2}a^{2} + 64\alpha_{1}a^{2}A^{2} \alpha_{2} - 64\alpha_{1}a \alpha_{2} \\ &+ 16A^{4} \alpha_{2}^{2}a^{2} - 32A^{2} \alpha_{2}^{2}a + 16\alpha_{2}^{2} - 20A^{6} \alpha_{3}^{2}a + 48A^{2} \alpha_{3} \alpha_{2} + 40A^{4} \alpha_{3}^{2} - 96A^{2} \alpha_{3} \alpha_{1}a \right)^{\frac{1}{2}} \right)^{2} , \end{aligned}$$

$$(9.61)$$

So, substituting Eq. (9.61) into Eq. (9.57), we have:

$$\omega = \frac{1}{2} \sqrt{\frac{5 A^4 \alpha_3 + 6 A^2 \alpha_2 + 8 \alpha_1}{a A^2 + 2}},$$
(9.62)

<sup>756</sup> We can obtain the following approximate solution:

$$u(t) = A\cos\left(\frac{1}{2}\sqrt{\frac{5A^4\alpha_3 + 6A^2\alpha_2 + 8\alpha_1}{aA^2 + 2}}t\right),\tag{9.63}$$

Figs. 9.11 and 9.12 represent a comparison of the analytical solution of u(t) based on time with the numerical solution. The time history diagram of u(t) starts without an observable deviation with A = 0.5 and A = 2. The behavior of the system is a periodic motion and the amplitude of vibration is a function of the initial conditions. The best accuracy can be seen at extreme points. Although deviations of solutions are expected to increase as time progresses, the analytical solutions have adequate accuracy for the period shown

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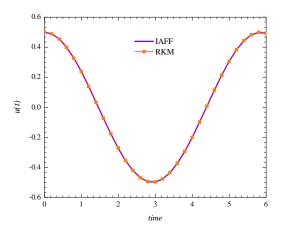


Figure 9.11 Comparison of displacement u(t) of the IAFF solution with the RKM solution A = 0.5 , a = 0.5 ,  $\alpha_1$  = 1 ,  $\alpha_2$  = 1 ,  $\alpha_3$  = 1

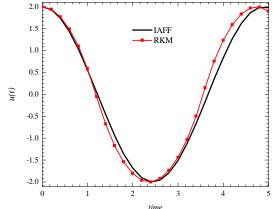


Figure 9.12 Comparison of u(t) of the IAFF solution with the RKM solution  $A=2~,~a=0.8~,\alpha_1=0.5~,~\alpha_2=0.6~,~\alpha_3=0.2$ 

## 763 10 MAX-MIN APPROACH (MMA)

In this section, we consider a novel method called Max-Min Approach (MMA). Maximal and 764 minimal solution thresholds of a nonlinear problem can be easily found, and an approximate 765 solution of the nonlinear equation can be easily deduced using He Chengtian's interpolation, 766 which has millennia history. Some examples are illustrated to show the efficiency and accuracy 767 of the proposed method for high nonlinear vibration problems. This methodology has been uti-768 lized to achieve approximate solutions for nonlinear free vibration of conservative thick circular 769 sector slabs. In Max-Min Approach (MMA), contrary to the conventional methods, only one 770 iteration leads to high accuracy of solutions. Max-Min Approach (MMA) operates very well in 771 the whole range of the parameters involved. Excellent agreement of the approximate frequen-772 cies and periodic solutions with the exact ones could be established. Some patterns are given to 773 illustrate the effectiveness and convenience of the methodology. It has been indicated that the 774 numerical results have same conclusion; while MMA is much easier, more convenient and more 775

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efficient than other approaches. The MMA is a novel method which alleviates drawbacks of the traditional numerical techniques. The method first was proposed by He [110]. The application of this method widely used in many scientific papers [13, 20, 23, 70, 73, 171, 188, 207].

## 779 10.1 Basic idea of Max-Min Approach

780 We consider a generalized nonlinear oscillator in the form

$$\ddot{u} + u f(u) = 0, u(0) = A, \dot{u}(0) = 0, \tag{10.1}$$

<sup>781</sup> Where f(u) is a non-negative function of u. According to the idea of the max-min method, <sup>782</sup> we choose a trial-function in the form

$$u(t) = A\cos\left(\omega t\right),\tag{10.2}$$

783 Where  $\omega$  the unknown frequency to be further is determined.

Observe that the square of frequency,  $\omega^2$ , is never less than that in the solution

$$u_1(t) = A\cos\left(\sqrt{f_{\min}}t\right),\tag{10.3}$$

785 of the following linear oscillator

$$\ddot{u} + u f_{\min} = 0, u(0) = A, \dot{u}(0) = 0, \tag{10.4}$$

Where  $f_{\min}$  is the minimum value of the function f(u).

In addition,  $\omega^2$  never exceeds the square of frequency of the solution

$$u_1(t) = A\cos\left(\sqrt{f_{\max}}t\right),\tag{10.5}$$

788 of the following oscillator

$$\ddot{u} + u f_{\max} = 0, u(0) = A, \dot{u}(0) = 0,$$
(10.6)

789 Where  $f_{\text{max}}$  is the maximum value of the function f(u).

<sup>790</sup> Hence, it follows that

$$\frac{f_{\min}}{1} < \omega^2 < \frac{f_{\max}}{1}.$$
 (10.7)

According to He Chentian interpolation [110, 112], we obtain

$$\omega^2 = \frac{m f_{\min} + n f_{\max}}{m + n},\tag{10.8}$$

792 Or

$$\omega^2 = \frac{f_{\min} + k f_{\max}}{1 + k},\tag{10.9}$$

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Where m and n are weighting factors, k = n/m. So the solution of Eq. (10.1) can be expressed 793 794 as

$$u(t) = A \cos \sqrt{\frac{f_{\min} + k f_{\max}}{1 + k}} t,$$
 (10.10)

The value of k can be approximately determined by various approximate methods [105, 795 110, 112]. Among others, hereby we use the residual method [110]. Substituting (10.10) into 796 (10.1) results in the following residual: 797

$$R(t;k) = -\omega^2 A \cos(\omega t) + (A \cos(\omega t)) \cdot f(A \cos(\omega t))$$
(10.11)

798

Where  $\omega = \sqrt{\frac{f_{\min} + k f_{\max}}{1+k}}$ If, by chance, Eq. (10.10) is the exact solution, then R(t;k) is vanishing completely. Since 799 our approach is only an approximation to the exact solution, we set 800

$$\int_{0}^{T} R(t;k) \cos \sqrt{\frac{f_{\min} + k f_{\max}}{1+k}} t \, dt = 0, \qquad (10.12)$$

where  $T = 2\pi/\omega$ . Solving the above equation, we can easily obtain 801

$$k = \frac{f_{\max} - f_{\min}}{1 - \sqrt{\frac{A}{\pi} \int_0^{\pi} \cos^2 x \cdot f} (A \cos x) \, dx}.$$
 (10.13)

Substituting the above equation into Eq. (10.10), we obtain the approximate solution of 802 Eq. (10.1). 803

#### 10.2 **Application of Max-Min Approach** 804

In this section, three examples are illustrated and solved to show the applicability, accuracy 805 and effectiveness of Max-Min Approach. 806

807

#### Example 1 808

We can re-write Eq. (9.21) from the previous section in the following form; 809

$$\ddot{\nu} + (2\alpha + 2\beta\nu^2)\nu = 0. \tag{10.14}$$

We choose a trial-function in the form 810

$$\nu = A\cos\left(\omega t\right) \tag{10.15}$$

Where  $\omega$  the frequency to be is determined the maximum and minimum values of  $2\alpha + 2\beta\nu^2$ 811 will be  $2\alpha + 2\beta A^2$  and  $2\alpha$  respectively, so we can write: 812

$$\frac{2\alpha}{1} < \omega^2 = 2\alpha + 2\beta\nu^2 < \frac{2\alpha + 2\beta A^2}{1}$$
(10.16)

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According to He Chengtian's inequality, we have

$$\omega^{2} = \frac{m.2\alpha + n.(2\alpha + 2\beta A^{2})}{m+n} = 2\alpha + 2k \ \beta A^{2}$$
(10.17)

Where m and n are weighting factors, k = n/m + n. Therefore the frequency can be approximated as:

$$\omega = \sqrt{2\alpha + 2k\ \beta A^2} \tag{10.18}$$

<sup>816</sup> Its approximate solution reads

$$\nu = A \cos \sqrt{2\alpha + 2k \ \beta A^2} t \tag{10.19}$$

In view of the approximate solution, Eq.(10.19) we re-write Eq.(10.14) in the form

$$\ddot{\nu} + (2\alpha + 2k \ \beta A^2)\nu = (2\alpha + 2k \ \beta A^2)\nu - 2\beta\nu^3$$
(10.20)

If by any chance Eq.(10.19) is the exact solution, then the right side of Eq.(10.20) vanishes completely. Considering our approach which is just an approximation one, we set:

$$\int_{0}^{T/4} \left( 2k \ \beta A^2 \nu - 2\beta \nu^3 \right) \cos \omega t \, dt = 0 \tag{10.21}$$

Where  $T = 2\pi/\omega$ . Solving the above equation, we can easily obtain

$$k = \frac{3}{4} \tag{10.22}$$

<sup>821</sup> Finally the frequency is obtained as

$$\omega = \frac{1}{2}\sqrt{8\alpha + 6\beta A^2} \tag{10.23}$$

According to Eqs. (10.15) and (10.23), we can obtain the following approximate solution:

$$\nu(t) = A \cos\left(\frac{1}{2}\sqrt{8\alpha + 6\beta A^2}t\right) \tag{10.24}$$

The first-order analytical approximation for u(t) is

$$u(t) = \iint (\alpha \nu + \beta \nu^3) dt dt = -\frac{1}{9\omega^2} A \cos(\omega t) \left(9\alpha + 6\beta A^2 + A\beta \cos^2(\omega t)\right).$$
(10.25)

Therefore, the first-order analytical approximate displacements x(t) and y(t) are

$$x(t) = u(t)$$
  

$$x(t) = u(t) + A\cos(\omega t)$$
(10.26)

С	onstar	nt par	amete	rs	Approximate Solution	Exact solution	Relative error $\%$
$\overline{m}$	$k_1$	$k_2$	$X_0$	$Y_0$	$\omega_{MMA}$	$\omega_{Exact}[44]$	$\frac{\omega_{MMA} - \omega_{Ex}}{\omega_{Ex}}$
1	0.5	0.5	1	5	3.605551	3.539243	1.873506
1	1	1	5	1	5.09902	5.005246	1.873506
5	2	0.5	5	10	4.421538	4.333499	2.031592
10	5	5	10	20	8.717798	8.533586	2.158667
20	40	50	20	10	19.46792	19.05429	2.17082
_50	100	50	-10	20	36.79674	36.00234	2.206522

Table 10.1 Comparison of frequency corresponding to various parameters of the system.

From table 10.1, the relative error of the MMA is 2.2065% for the first-order analytical 825 approximations, for different values of  $m, k_1, k_2, X_0$  and  $Y_0$ . The first-order approximate so-826 lution gives an excellent agreement with the exact one. To further illustrate and verify the 827 accuracy of this approximate analytical approach, a comparison of the time history oscillatory 828 displacement and velocity responses for the two masses with exact solutions is depicted in Fig. 829 10-1 and 10.2. Figs. 10.3 and 10.4 represent the effects of amplitude on the phase plan of the 830 system. It is apparent that the first-order analytical approximations show excellent agreement 831 with the exact solution using the Jacobi elliptic function. 832

## 834 Example 2

833

A two-mass system connected with linear and nonlinear stiffnesses fixed to the body was solved by IAFF is considered again in this section. We can re-write Eq. (9.39) in the following form;

$$\ddot{\nu} + ((\alpha + 2\beta) + 2\xi\nu^2)\nu = 0 \tag{10.27}$$

<sup>838</sup> We choose a trial-function in the form

$$\nu = A \cos\left(\omega t\right) \tag{10.28}$$

Where  $\omega$  the frequency to be is determined the maximum and minimum values of  $\alpha + 2\beta + 2\xi\nu^2$  will be  $\alpha + 2\beta + 2\xi A^2$  and  $\alpha + 2\beta$  respectively, so we can write:

$$\frac{\alpha + 2\beta}{1} < \omega^2 = \alpha + 2\beta + 2\xi\nu^2 < \frac{\alpha + 2\beta + 2\xi A^2}{1}$$
(10.29)

According to He Chengtian's inequality, we have

$$\omega^{2} = \frac{m.(\alpha + 2\beta) + n.(\alpha + 2\beta + 2\xi A^{2})}{m+n} = \alpha + 2\beta + 2\xi kA^{2}$$
(10.30)

Where m and n are weighting factors, k = n/m + n. Therefore the frequency can be approximated as:

$$\omega = \sqrt{\alpha + 2\beta + 2\xi k A^2} \tag{10.31}$$

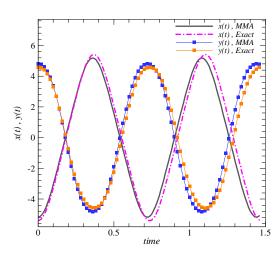


Figure 10.1 Comparison of analytical solution of displacement x(t) and y(t) based on time twith the exact solution[44] for m = 10,  $k_1 = 5$ ,  $k_2 = 5$ ,  $X_0 = 10$ ,  $Y_0 = 20$ 

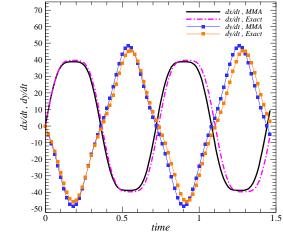


Figure 10.2 Comparison of analytical solution of dx/dt and dy/dt based on time t with the exact solution [44] for  $m = 10, k_1 = 5, k_2 = 5 X_0 = 10, Y_0 = 20$ 

844 Its approximate solution reads

$$\nu = A \cos \sqrt{\alpha + 2\beta + 2\xi k A^2} t \tag{10.32}$$

In view of the approximate solution, Eq. (10.31) we re-write Eq. (10.27) in the form;

$$\ddot{\nu} + (\alpha + 2\beta + 2\xi kA^2)\nu = (2\xi kA^2)\nu - 2\xi\nu^3$$
(10.33)

If by any chance Eq. (10.32) is the exact solution, then the right side of Eq.(10.33) vanishes completely. Considering our approach which is just an approximation one, we set:

$$\int_0^{T/4} \left( 2\xi k A^2 \nu - 2\xi \nu^3 \right) \cos \omega t \, dt = 0 \tag{10.34}$$

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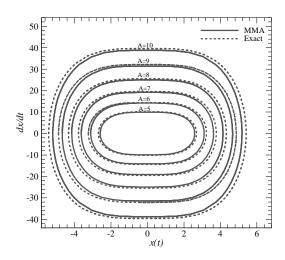


Figure 10.3 Comparison of analytical solution of dx/dt based on x(t) with the exact solution [44] for  $m = 10, k_1 = 5, k_2 = 5$ 

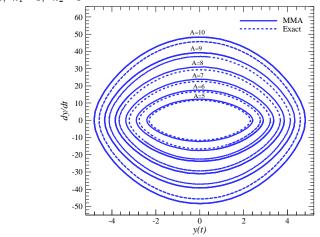


Figure 10.4 Comparison of analytical solution of dy/dt based on y(t) with the exact solution [44] for  $m = 10, k_1 = 5, k_2 = 5$ 

Where  $T = 2\pi/\omega$ . Solving the above equation, we can easily obtain

$$k = \frac{3}{4} \tag{10.35}$$

<sup>849</sup> Finally the frequency is obtained as

$$\omega = \frac{1}{2}\sqrt{4\alpha + 8\beta + 6\xi A^2} \tag{10.36}$$

According to Eqs. (10.36) and (10.28), we can obtain the following approximate solution:

$$\nu(t) = A \cos\left(\frac{1}{2}\sqrt{4\alpha + 8\beta + 6\xi A^2}t\right)$$
(10.37)

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The first-order analytical approximation for u(t) is

$$u(t) = \frac{-\cos(\sqrt{\alpha}t)(-X_0 \alpha^2 + 10X_0 \alpha \omega^2 - 9X_0 \omega^4 + \xi A^3 \alpha - 7\xi A^3 \omega^2 - 9A\beta \omega^2 + A\alpha\beta)}{\alpha^2 - 10\alpha \omega^2 + 9\omega^4} - \frac{27A(\cos(\omega t)((\xi A^2 + \frac{4}{3}\beta)(\omega^2 - \frac{1}{9}\alpha)) + \cos(3\omega t)(\frac{1}{27}\xi A^2(\omega^2 - \alpha)))}{4\alpha^2 - 40\alpha \omega^2 + 36\omega^4}$$
(10.38)

Therefore, the first-order analytical approximate displacements x(t) and y(t) are

$$x(t) = u(t)$$
  

$$x(t) = u(t) + A\cos(\omega t)$$
(10.39)

Table 10.2 Comparison of frequency corresponding to various parameters of system

	Constant parameters					Approximate Solution	Exact Solution	Relative error %
m	$k_1$	$k_2$	$k_3$	$X_0$	$Y_0$	$\omega_{MMA}$	$\omega_{Exact}[43]$	$\frac{\omega_{MMA} - \omega_{Ex}}{\omega_{Ex}}$
1	0.5	0.5	0.5	1	5	3.674235	3.611743	1.730234
1	1	1	2	5	1	7.141428	7.004694	1.952045
5	2	0.5	5	5	10	6.17252	6.042804	2.146618
10	5	5	10	10	20	12.30853	12.04665	2.173874
20	40	50	50	20	10	19.54482	19.13632	2.134672
50	100	50	100	-10	20	52.00000	50.87391	2.213492

Table 10.2 gives the comparison of obtained results with exact ones are tabulated in Table 10.2 for different value of  $m, k_1, k_2, k_3$  and initial conditions. Comparisons of results for different parameters via numerical and MMA are presented in Figures 10.5 to 10.8. From figures 10.5 and 10.6, it is obvious that the motion of the system is periodic. Figures 10.7 and 10.8 represent comparison of analytical solution of dx/dt and dy/dt based on time with the numerical solution for different parameters of the system.

# 860 Example 3

859

We consider geometrically non-linear Tapered beams. In dimensionless form, Goorman is given the governing differential equation corresponding to fundamental vibration mode of a tapered beam [78]:

$$\left(\frac{d^2u}{dt^2}\right) + \varepsilon_1 \left(u^2 \left(\frac{d^2u}{dt^2}\right) + u \left(\frac{du}{dt}\right)^2\right) + u + \varepsilon_2 u^3 = 0$$
(10.40)

Where u is displacement and  $\varepsilon_1$  and  $\varepsilon_2$  are arbitrary constants. Subject to the following initial conditions:

$$u(0) = A, \qquad \frac{du(0)}{dt} = 0$$
 (10.41)

We can re-write Eq. (10.40) in the following form

$$\left(\frac{d^2u}{dt^2}\right) + \left(\frac{1 + \varepsilon_1 \left(\frac{du}{dt}\right)^2 + \varepsilon_2 u^2}{1 + \varepsilon_1 u^2}\right) u = 0$$
(10.42)

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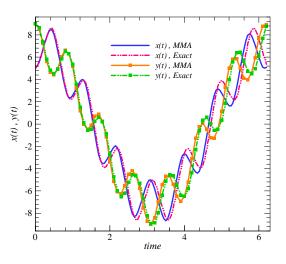


Figure 10.5 Comparison of analytical solution of displacement x(t) and y(t) based on time t with the exact solution [43] for m = 1,  $k_1 = 1$ ,  $k_2 = 1$ ,  $k_3 = 2$ ,  $X_0 = 5$ ,  $Y_0 = 1$ 

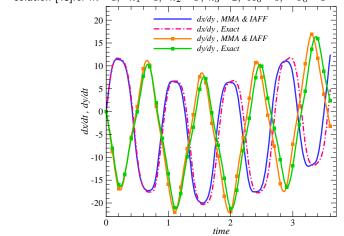


Figure 10.6 Comparison of analytical solution of dx/dt and dy/dt based on time t with the exact solution [43]for m = 1,  $k_1 = 1$ ,  $k_2 = 1$ ,  $k_3 = 2$ ,  $X_0 = 5$ ,  $Y_0 = 1$ 

<sup>867</sup> We choose a trial-function in the form

$$u = A\cos\left(\omega t\right) \tag{10.43}$$

<sup>868</sup> Where  $\omega$  the frequency to be is determined.

By using the trial-function, the maximum and minimum values of  $\omega^2$  will be:

$$\omega_{\min} = \frac{1+\varepsilon_1 A^2 \omega^2}{1},$$
  

$$\omega_{\max} = \frac{1+\varepsilon_2 A^2}{1+\varepsilon_1 A^2}.$$
(10.44)

So we can write:

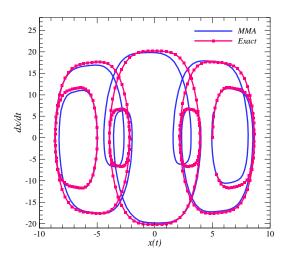


Figure 10.7 Comparison of analytical solution of dx/dt based on x(t) with the exact solution [43]for m = 1,  $k_1 = 1$ ,  $k_2 = 1$ ,  $k_3 = 2$ ,  $X_0 = 5$ ,  $Y_0 = 1$ 

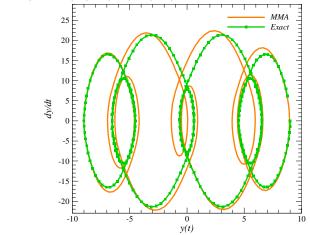


Figure 10.8 Comparison of analytical solution of dy/dt based on y(t) with the exact solution [43]for m = 1,  $k_1 = 1$ ,  $k_2 = 1$ ,  $k_3 = 2$ ,  $X_0 = 5$ ,  $Y_0 = 1$ 

$$\frac{1+\varepsilon_1 A^2 \omega^2}{1} < \omega^2 < \frac{1+\varepsilon_2 A^2}{1+\varepsilon_1 A^2}$$
(10.45)

## According to the Chengtian's inequality , we have

$$\omega^{2} = \frac{m \cdot \left(1 + \varepsilon_{1} A^{2} \omega^{2} + \varepsilon_{2} A^{2}\right) + n \cdot \left(1 + \varepsilon_{1} A^{2} \omega^{2}\right)}{m + n} = 1 + \varepsilon_{1} A^{2} \omega^{2} + k \ \varepsilon_{2} A^{2} \tag{10.46}$$

Where m and n are weighting factors, k = n/m + n. Therefore the frequency can be approximated as:

$$\omega = \sqrt{\frac{1+k\ \varepsilon_2 A^2}{1-\varepsilon_1 A^2}} \tag{10.47}$$

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874 Its approximate solution reads

$$u = A \cos \sqrt{\frac{1+k \ \varepsilon_2 A^2}{1-\varepsilon_1 A^2}} t \tag{10.48}$$

In view of the approximate solution, Eq. (10.42), we re-write Eq.(10.42) in the form

$$\frac{d^2u}{dt^2} + \left(\frac{1+k}{1-\varepsilon_1 A^2}\right)u = \left(\frac{d^2u}{dt^2}\right) + \varepsilon_1 \left(u^2 \left(\frac{d^2u}{dt^2}\right) + u \left(\frac{du}{dt}\right)^2\right) + u + \varepsilon_2 u^3 + \Psi$$
(10.49)

$$\Psi = \left(\frac{1+k}{1-\varepsilon_1 A^2}\right)u - \varepsilon_1 u^2 \left(\frac{d^2 u}{dt^2}\right) - \varepsilon_1 u \left(\frac{d u}{dt}\right)^2 - u - \varepsilon_2 u^3$$
(10.50)

Substituting the trial function into Eq. (10.50), and using Fourier expansion series, it is obvious that:

$$\Psi = \left(\frac{1+k}{1-\varepsilon_1 A^2}\right) (A\cos\omega t) - \left(2\omega^2 \varepsilon_1 A^2 \cos^2(\omega t) - \varepsilon_1 A^2 \omega^2 - 1 - \varepsilon_2 A^2 \cos^2(\omega t)\right) A\cos(\omega t)$$
  
$$= \sum_{n=0}^{\infty} b_{2n+1} \cos\left[(2n+1)\omega t\right] = b_1 \cos(\omega t) + b_3 \cos(3\omega t) + \dots \approx b_1 \cos(\omega t)$$
(10.51)

For avoiding secular term we set  $b_1 = 0$ 

$$\int_{0}^{T/4} \left( \left( \frac{1+k \ \varepsilon_2 A^2}{1-\varepsilon_1 A^2} \right) - \left( 2\omega^2 \varepsilon_1 A^2 \cos^2(\omega t) - \varepsilon_1 A^2 \omega^2 - 1 - \varepsilon_2 A^2 \cos^2(\omega t) \right) \right) A \cos(\omega t) \, dt = 0$$

$$(10.52)$$

Where  $T = 2\pi/\omega$ . Solving the above equation, we can easily obtain

$$k = -\frac{\left(\varepsilon_1\omega^2 - \varepsilon_1^2 A^2 \omega^2 + 3\varepsilon_1 - 2\varepsilon_2 + 2\varepsilon_2 A^2 \varepsilon_1\right)}{3\varepsilon_2} \tag{10.53}$$

## Substituting Eq. (10.53) into Eq. (10.47), yields

$$\omega = \frac{\sqrt{(3+\varepsilon_1 A^2) \left(2\varepsilon_2 A^2+3\right)}}{(3+\varepsilon_1 A^2)} \tag{10.54}$$

According to Eqs. (10.54) and (10.43), we can obtain the following approximate solution:

$$u(t) = A \cos\left(\frac{\sqrt{(3+\varepsilon_1 A^2)(2\varepsilon_2 A^2+3)}}{(3+\varepsilon_1 A^2)}t\right)$$
(10.55)

The exact frequency  $\omega_e$  for a dynamic system governed by Eq. (10.40) can be derived, as shown in Eq. (10.56), as follows:

$$\omega_{Exact} = 2\pi \left/ 4\sqrt{2} A \int_0^{\pi/2} \frac{\sqrt{1 + \varepsilon_1 A^2 \cos^2 t} \sin t}{\sqrt{A^2 (1 - \cos^2 t) (\varepsilon_2 A^2 \cos^2 t + \varepsilon_2 A^2 + 2)}} dt$$
(10.56)

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To demonstrate the accuracy of the MMA, the procedures explained in previous sections are applied to obtain natural frequency and corresponding displacement of tapered beams. A comparison of obtained results from the Max-Min Approach and the exact one is tabulated in table 10.3 for different parameters  $A, \varepsilon_1$  and  $\varepsilon_2$ .

Constant parameters			Approximate solution	Exact solution	Relative error $\%$
A	$\varepsilon_1$	$\varepsilon_2$	$\omega_{MMA}$	$\omega_{Exact}$	$\frac{\omega_{MMA} - \omega_{Ex}}{\omega_{Ex}}$
2	0.1	0.5	1.43486	1.44100	0.42665
2	0.5	1	1.48323	1.44506	2.64192
2	5	10	1.8996	1.85323	2.50516
2	10	50	3.06138	3.0103	1.69512
10	0.1	0.5	2.81479	2.73523	2.90861
10	0.5	1	1.95708	1.92710	1.55604
10	5	10	1.99552	1.98950	$0.\ 1842$
10	10	50	3.15801	3.15265	0.17001

Table 10.3 Comparison of frequency corresponding to various parameters of system

Figs. 10.9 and 10.10 represent the high accuracy of the MMA with the exact one for  $\varepsilon_1 = 0.1 \varepsilon_2 = 0.5$  and  $\varepsilon_1 = 0.5 \varepsilon_2 = 0.1$ . The effect of small parameters  $\varepsilon_2$  and  $\varepsilon_1$  on the frequency corresponding to various parameters of amplitude (A) has been studied in Figs. 10.11 and 10.12. It is evident that MMA shows excellent agreement with the numerical solution using the exact solution and quickly convergent and valid for a wide range of vibration amplitudes and initial conditions.

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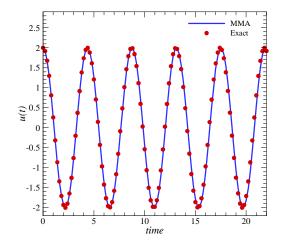


Figure 10.9 Comparison of analytical solutions of  $u(t){\rm based}$  on  $t{\rm with}$  the exact solution for  $\varepsilon_1$  =  $0.1\,\varepsilon_2$  =  $0.5\,A$  = 2

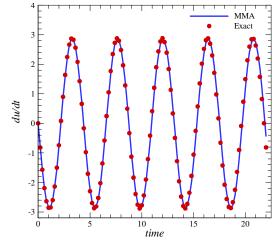


Figure 10.10 Comparison of analytical solutions of du/dt based on time with the exact solution for  $\varepsilon_1 = 0.5$ ,  $\varepsilon_2 = 0.1$ , A = 2,

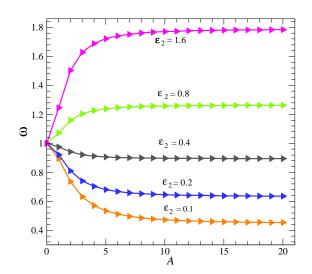


Figure 10.11 Comparison of frequency corresponding to various parameters of amplitude (A) and  $\varepsilon_1$  = 1

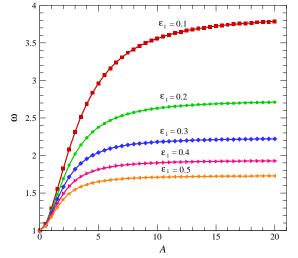


Figure 10.12 Comparison of frequency corresponding tovarious parameters of amplitude (A) and  $\varepsilon_2$  = 1

# <sup>894</sup> 11 HAMILTONIAN APPROACH (HA)

Investigate of nonlinear problems which are arisen in many areas of physics and engineering, 895 especially some oscillation equations are nonlinear, and in most cases it is difficult to solve such 896 equations, especially analytically. Previously, He had introduced the Energy Balance method 897 based on collocation and the Hamiltonian. This approach is very simple but strongly depends 898 upon the chosen location point. Recently, He [111] has proposed the Hamiltonian approach to 899 overcome the shortcomings of the energy balance method. This approach is a kind of energy 900 method with a vast application in conservative oscillatory systems. Application of this method 901 can be found in many literatures [124, 140, 198, 199, 203–205]. 902

### 903 11.1 Basic idea of Hamiltonian Approach

<sup>904</sup> In order to clarify this approach, consider the following general oscillator;

$$\ddot{u} + f(u, \dot{u}, \ddot{u}) = 0$$
 (11.1)

905 With initial conditions:

$$u(0) = A, \, , \dot{u}(0) = 0.$$
 (11.2)

Oscillatory systems contain two important physical parameters, i.e. the frequency  $\omega$  and the amplitude of oscillation A. It is easy to establish a variational principle for Eq. (11.1), which reads;

$$J(u) = \int_0^{T/4} \left\{ -\frac{1}{2} \dot{u}^2 + F(u) \right\} dt$$
(11.3)

Where T is period of the nonlinear oscillator,  $\frac{\partial F}{\partial \mu} = f$ .

In the Eq (11.3),  $\frac{1}{2}\dot{u}^2$  is kinetic energy and F(u) potential energy, so the Eq (11.3) is the least Lagrangian action, from which we can immediately obtain its Hamiltonian, which reads ;

$$H(u) = \frac{1}{2}\dot{u}^2 + F(u) = \text{constant}$$
(11.4)

913 From Eq. (11.4), we have;

$$\frac{\partial H}{\partial A} = 0 \tag{11.5}$$

Introducing a new function,  $\overline{H}(u)$ , defined as;

$$\bar{H}(u) = \int_{0}^{T/4} \int \left\{ \frac{1}{2} \dot{u}^2 + F(u) \right\} dt = \frac{1}{4} T H$$
(11.6)

Eq. (11.5) is, then, equivalent to the following one;

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$$\frac{\partial}{\partial A} \left( \frac{\partial \bar{H}}{\partial T} \right) = 0 \tag{11.7}$$

916 OT

$$\frac{\partial}{\partial A} \left( \frac{\partial \bar{H}}{\partial (1/\omega)} \right) = 0 \tag{11.8}$$

From Eq.(11.8) we can obtain approximate frequency-amplitude relationship of a nonlinear oscillator.

# 919 **11.2** Application of Hamiltonian Approach

We have considered three examples in this section to show the application of the proposed method.

#### 922 923 Example 1

To illustrate the basic procedure of the present method, we consider an  $u^{1/3}$  force nonlinear oscillator:

$$\ddot{u} + au + bu^3 + cu^{1/3} = 0, \qquad u(0) = A, \ \dot{u}(0) = 0$$
 (11.9)

<sup>926</sup> The Hamiltonian of Eq. (11.9) is constructed as:

$$H = \frac{1}{2}\dot{u}^2 + \frac{1}{2}au^2 + \frac{1}{4}bu^4 + \frac{3}{4}cu^{4/3}$$
(11.10)

Integrating Eq.(11.10) with respect to t from 0 to T/4, we have;

$$\bar{H} = \int_0^{T/4} \left( \frac{1}{2} \dot{u}^2 + \frac{1}{2} a u^2 + \frac{1}{4} b u^4 + \frac{3}{4} c u^{4/3} \right) dt$$
(11.11)

Assume that the solution can be expressed as:

$$u(t) = A\cos(\omega t) \tag{11.12}$$

Substituting Eq.(11.12) into Eq. (11.11), we obtain:

$$\begin{split} \bar{H} &= \int_{0}^{T/4} \left( \frac{1}{2} A^{2} \omega^{2} \sin^{2} \left( \omega t \right) + \frac{1}{2} a A^{2} \cos^{2} \left( \omega t \right) + \frac{1}{4} b A^{4} \cos^{4} \left( \omega t \right) + \frac{3}{4} c A^{4/3} \cos^{4/3} \left( \omega t \right) \right) dt \\ &= \int_{0}^{\pi/2} \left( \frac{1}{2} A^{2} \omega \sin^{2} t + \frac{1}{2\omega} a A^{2} \cos^{2} t + \frac{1}{4\omega} b A^{4} \cos^{4} t + \frac{3}{4\omega} c A^{4/3} \cos^{4/3} t \right) dt \\ &= \frac{1}{8} \omega A^{2} \pi + \frac{1}{8} a A^{2} \frac{\pi}{\omega} + \frac{3}{64} b A^{4} \frac{\pi}{\omega} + 0.12267 c A^{4/3} \frac{\pi^{3/2}}{\omega} \end{split}$$
(11.13)

930 Setting:

$$\frac{\partial}{\partial A} \left( \frac{\partial \bar{H}}{\partial (1/\omega)} \right) = -\frac{1}{4} \omega^2 A \,\pi + \frac{1}{4} a \,A \,\pi + \frac{3}{64} b A^4 \pi + 0.16356 \,\mathrm{c} \,A^{1/3} \pi^{3/2} \tag{11.14}$$

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<sup>931</sup> Solving the above equation, an approximate frequency as a function of amplitude equals;

$$\omega_{HA} = \sqrt{a + \frac{3}{4}A^2b + \frac{0.654236\,c\sqrt{\pi}}{A^{2/3}}} \tag{11.15}$$

<sup>932</sup> Hence, the approximate solution can be readily obtained;

$$u(t) = A\cos\left(\sqrt{a + \frac{3}{4}A^2b + \frac{0.654236\,c\,\sqrt{\pi}}{A^{2/3}}} t\right)$$
(11.16)

<sup>933</sup> The same result was obtained by He [107].

#### 934

## 935 Example 2

<sup>936</sup> Considering the governing equation of motion for the Duffing-harmonic oscillator:

$$\ddot{u} + \frac{u^3}{1+u^2} = 0, \qquad u(0) = A, \ \dot{u}(0) = 0$$
(11.17)

<sup>937</sup> The Hamiltonian of Eq. (11.17) is constructed as:

$$H = \frac{1}{2}\dot{u}^2 + \frac{1}{2}u^2 - \frac{1}{2}\log\left(1+u^2\right)$$
(11.18)

Integrating Eq.(11.18) with respect to t from 0 to T/4, we have;

$$\bar{H} = \int_0^{T/4} \left( \frac{1}{2} \dot{u}^2 + \frac{1}{2} u^2 - \frac{1}{2} \log\left(1 + u^2\right) \right) dt \tag{11.19}$$

Assume that the solution can be expressed as:

$$u(t) = A\cos(\omega t) \tag{11.20}$$

Substituting Eq.(11.20) into Eq. (11.19), we obtain:

$$\bar{H} = \int_{0}^{T/4} \left( \frac{1}{2} A^{2} \omega^{2} \sin^{2} \left( \omega t \right) + \frac{1}{2} A^{2} \cos^{2} \left( \omega t \right) - \frac{1}{2} \log \left( 1 + A^{2} \cos^{2} \left( \omega t \right) \right) \right) dt 
= \int_{0}^{\pi/2} \left( \frac{1}{2} A^{2} \omega \sin^{2} t + \frac{1}{2\omega} A^{2} \cos^{2} t - \frac{1}{2\omega} \log \left( 1 + A^{2} \cos^{2} t \right) \right) dt$$
(11.21)

941 Setting:

$$\frac{\partial}{\partial A} \left( \frac{\partial \bar{H}}{\partial (1/\omega)} \right) = 0 \tag{11.22}$$

942

2 Solving the above equation, an approximate frequency as a function of amplitude equals;

$$\omega_{HA} = \sqrt{\frac{\int_0^{\pi/2} \left\{\frac{\cos^2 t}{1+A^2 \cos^2 t}\right\} dt}{\int_0^{\pi/2} \sin^2 t \, dt}}$$
(11.23)

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<sup>943</sup> The exact frequency is given by [132]:

$$\omega_{Ex} = \frac{2\pi}{4\int_0^A \frac{du}{\sqrt{[\log(A^2+1) - \log(u^2+1)]}}}$$
(11.24)

Table 11.1 Comparison of frequency Hamiltonian approach and exact solution

А	$\omega_{ex}$	$\omega_{HA}$	Relative error (%)
0.01	0.00847	0.00865	2.12515
0.1	0.08439	0.08624	2.192203
1	0.63678	0.64359	1.06944
10	0.99092	0.99095	0.00303
100	0.9999	0.9999	0.0001

From Table 11.1, the maximum relative error is 2.192203%.

#### 944

### 945 Example 3

<sup>946</sup> The Hamiltonian of Eq. (10.40) is constructed as;

$$H = \frac{1}{2} \left(\frac{du}{dt}\right)^2 + \frac{1}{2} \varepsilon_1 \left(\frac{du}{dt}\right)^2 u^2 + \frac{1}{2} u^2 + \frac{1}{4} \varepsilon_2 u^4$$
(11.25)

Integrating Eq. (11.25) with respect to t from 0 to T/4, we have;

$$\bar{H} = \int_0^{T/4} \left( \frac{1}{2} \left( \frac{du}{dt} \right)^2 + \frac{1}{2} \varepsilon_1 \left( \frac{du}{dt} \right)^2 u^2 + \frac{1}{2} u^2 + \frac{1}{4} \varepsilon_2 u^4 \right) dt$$
(11.26)

Assume that the solution can be expressed as;

$$u(t) = A\cos(\omega t) \tag{11.27}$$

Substituting Eq. (11.27) into Eq. (11.26), we obtain;

$$\begin{split} \bar{H} &= \int_0^{T/4} \left( \frac{1}{2} \mathbf{A}^2 \,\omega^2 \sin^2\left(\omega t\right) + \frac{1}{2} \varepsilon_1 \,\mathbf{A}^4 \,\omega^2 \sin^2\left(\omega t\right) \cos^2\left(\omega t\right) + \frac{1}{2} \mathbf{A}^2 \,\cos^2\left(\omega t\right) + \frac{1}{4} \varepsilon_2 \mathbf{A}^4 \,\cos^4\left(\omega t\right) \right) \,dt \\ &= \int_0^{\pi/2} \left( \frac{1}{2} \mathbf{A}^2 \,\omega \sin^2 t + \frac{1}{2} \varepsilon_1 \,\mathbf{A}^4 \,\omega \sin^2 t \,\cos^2 t + \frac{1}{2\omega} \,\mathbf{A}^2 \,\cos^2 t + \frac{1}{4\omega} \,\varepsilon_2 \mathbf{A}^4 \,\cos^4 t \right) \,dt \\ &= \frac{1}{8} \omega A^2 \pi + \frac{1}{32} \omega A^4 \varepsilon_1 \pi \frac{1}{8\omega} A^2 \pi + \frac{3}{64\omega} A^4 \varepsilon_2 \pi \end{split}$$
(11.28)

950 Setting:

$$\frac{\partial}{\partial A} \left( \frac{\partial \bar{H}}{\partial (1/\omega)} \right) = -\frac{1}{4} A \pi \omega^2 - \frac{1}{8} \varepsilon_1 A^3 \pi \omega^2 + \frac{1}{4} A \pi + \frac{3}{16} \varepsilon_2 A^3 \pi$$
(11.29)

951

$$\omega_{HA} = \frac{\sqrt{2}}{2} \frac{\sqrt{(\varepsilon_1 A^2 + 2) (3 \varepsilon_2 A^2 + 4)}}{(\varepsilon_1 A^2 + 2)}$$
(11.30)

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Hence, the approximate solution can be readily obtained;

$$u(t) = A\cos\left(\frac{\sqrt{2}}{2}\frac{\sqrt{(2+\varepsilon_1 A^2)(4+3\varepsilon_2 A^2)}}{(2+\varepsilon_1 A^2)} t\right)$$
(11.31)

Constant parameters			Approximate solution	Exact solution	Relative error %
A	$\varepsilon_1$	$\varepsilon_2$	$\omega_{HA}$	$\omega_{Exact}$	$\frac{\omega_{EX} - \omega_{HA}}{\omega_{Ex}}$
0.1	0.1	0.1	1.0001	1.0005	0.0374
0.1	1	0.2	0.9983	0.9983	0.0002
0.5	0.5	1	1.0572	1.0573	0.0084
0.5	1	0.5	0.9860	0.9870	0.1018
1	1	1	1.0801	1.0904	0.9382
1	0.5	0.2	0.9592	0.9623	0.3262
2	0.4	0.2	0.9428	0.9593	1.7212
2	1	0.8	1.0646	1.0917	2.4853
2	1	0.2	0.7303	0.7504	2.6846

The maximum relative error of Hamiltonian approach 2.6846 % for different values of  $A, \varepsilon_1, \varepsilon_2$  in comparison with the exact one.

# 953 12 HOMOTOPY ANALYSIS METHOD (HAM)

Homotopy analysis is a general analytic method for solving the non-linear differential equations. 954 The HAM transforms a non-linear problem into an infinite number of linear problems with 955 embedding an auxiliary parameter (q) that typically ranges from zero to one. As q increases 956 from 0 to 1, the solution varies from the initial guess to the exact solution. By suitable choice of 957 the auxiliary parameter (q), we can obtain reasonable solutions for large modulus. This method 958 is a strong and easy-to-use analytic tool for investigating nonlinear problems, which does not 959 need small parameters. In 1992, Liao employed the basic ideas of homotopy in topology to 960 propose a general analytic method for nonlinear problems, namely homotopy analysis method 961 (HAM) [128]. This method has been successfully applied to solve many types of nonlinear 962 problems by others [4, 6, 40, 41, 49, 51, 53, 114, 126, 129–131, 155–159, 172, 193, 194, 213]. 963 The basic idea of HAM is introduced and then its application in nonlinear vibration is studied. 964

### 965 12.1 Basic idea of Homotopy Analysis Method

<sup>966</sup> To illustrate the basic ideas of the HAM, consider the following non-linear differential equation:

$$N[u(t)] = 0, (12.1)$$

Where N is a nonlinear operator, t denotes the independent variable and u(t) is an unknown variable. The homotopy function is constructed as follows:

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$$\bar{H}(\phi;q,\hbar,H(t)) = (1-q)L[\phi(t;q) - u_0(t)] - q\hbar H(t)N[\phi(t;q)]$$
(12.2)

where  $\phi$ ,  $\hbar$  and H(t) are a function of t and q, the non-zero auxiliary parameter, is a non-zero auxiliary function, respectively. The parameter L denotes an auxiliary linear operator. As qincreases from 0 to 1, the  $\phi(t;q)$  varies from the initial approximation to the exact solution. In the other words,  $\phi(t;0) = u_0(t)$  is the solution of the  $\bar{H}(\phi,q,\hbar,H(t))|_{q=0} = 0$  and  $\phi(t;1) = u_0(t)$ is the solution of the  $\bar{H}(\phi,q,\hbar,H(t))|_{q=1} = 0$ . Enforcing  $\bar{H}(\phi,q,\hbar,H(t)) = 0$ , the zero-order deformation is constructed as:

$$(1-q)L[\phi(t,q) - u_0(t)] = q\hbar H(t)N[\phi(t,q)], \qquad (12.3)$$

<sup>975</sup> with the following initial conditions:

$$\phi(0;q) = a , \quad \frac{d\phi(0,q)}{dt} = 0.$$
 (12.4)

The functions  $\phi(t,q)$  and  $\omega(q)$  can be expanded as power series of q using Taylor's theorem as;

$$\phi(t,q) = \phi(t,0) + \sum_{m=1}^{\infty} \frac{1}{m!} \frac{\partial^m \phi(t;q)}{\partial q^m} |_{q=0} q^m = u_0(\tau) + \sum_{m=1}^{\infty} u_m(t) q^m$$
(12.5)

$$\omega(q) = \omega_0 + \sum_{m=1}^{\infty} \frac{1}{m!} \frac{\partial^m \omega(q)}{\partial q^m} |_{q=0} q^m = \omega_0 + \sum_{m=1}^{\infty} \omega_m q^m$$
(12.6)

Where  $u_m(t)$  and  $\omega_m$  are called the m-order deformation derivations.

Differentiating zero-order deformation equation with respect to q and the setting q = 0, yields the first order deformation equation (m = 1) which gives the first-order approximation of the u(t) as follows:

$$L[u_1(t)] = \hbar H(t) N[u_0(t), \omega_0]|_{q=0} , \qquad (12.7)$$

<sup>982</sup> with the following initial conditions:

$$u_1(0) = 0$$
,  $\dot{u}_1(0) = 0$  (12.8)

The higher order approximations of the solution can be obtained by calculating the morder (m>1) deformation equation. The m-order deformation equation can be calculated by differentiating Eqs. (12.5) and (12.6) m times with respect to q as follows:

$$L[u_m(t) - u_{m-1}] = \hbar H(t) R_m(\vec{u}_{m-1}, \vec{\omega}_{m-1}), \qquad (12.9)$$

Where the  $\vec{u}_{m-1}, \vec{\omega}_{m-1}$  and  $R_m(\vec{u}_{m-1}, \vec{\omega}_{m-1})$  are defined as follows:

$$R_m(\vec{u}_{m-1}, \vec{\omega}_{m-1}) = \frac{1}{(m-1)!} \frac{\partial^{m-1} N\left[\phi(t,q)\right], \omega(q)}{\partial q^{m-1}} \bigg|_{q=0},$$
(12.10)

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$$\vec{u}_{m-1} = \{ \vec{u}_0, \vec{u}_1, \vec{u}_2, \dots, \vec{u}_{m-1} \}$$
(12.11)

$$\vec{\omega}_{m-1} = \{\omega_0, \omega_1, \omega_2, \dots, \omega_{m-1}\}$$
(12.12)

987 Subject to the following initial conditions:

$$u_m(0) = \dot{u}_m(0) = 0. \tag{12.13}$$

# 988 12.2 Application of Homotopy Analysis Method

#### 989 Example 1

<sup>990</sup> Consider the following Duffing equation ;

$$\ddot{u} + \alpha u + \beta u^3 = 0 \quad u(0) = A \quad , \ \dot{u}(0) = 0 \tag{12.14}$$

Under the transformation  $\tau = \omega t$  and  $W(\tau) = u(t)$  Eq. (12.14) becomes as follows:

$$\omega^2 \ddot{W} + \alpha W + \beta W^3 = 0 \tag{12.15}$$

<sup>992</sup> The zero-order deformation equation can be written as below:

$$(1-q) L [\phi(\tau;q) - W_0(\tau)] = qhh(\tau) N [\phi(\tau;q)]$$
(12.16)

993 In which;

$$N[\phi(\tau;q)] = \omega^2 \frac{\partial^2 \phi(\tau;q)}{\partial \tau^2} + \alpha \phi(\tau;q) + \beta \phi(\tau;q)^3 = 0$$
(12.17)

<sup>994</sup> We chose the following auxiliary linear operator as:

$$L[\phi(\tau;q)] = \omega_0^2 \left[ \frac{\partial^2 \phi(\tau;q)}{\partial \tau^2} + \phi(\tau;q) \right]$$
(12.18)

We employ Taylor expansion series for 
$$\phi(t;q)$$
 and  $\omega(q)$  as

$$\phi(\tau;q) = \phi(\tau;0) + \sum_{m=1}^{\infty} \frac{1}{m!} \frac{\partial^m \phi(t;q)}{\partial q^m} |_{q=0} q^m = W_0(\tau) + \sum_{m=1}^{\infty} W_m(\tau) q^m$$
(12.19)

$$\omega(q) = \omega_0 + \sum_{m=1}^{\infty} \frac{1}{m!} \frac{\partial^m \omega(q)}{\partial q^m} |_{q=0} q^m = \omega_0 + \sum_{m=1}^{\infty} \omega_m q^m$$
(12.20)

In order to satisfy the initial conditions, the initial guess of  $W(\tau)$  is chosen as follows:

$$\omega_0(\tau) = W_{\max} \cos(\tau) \tag{12.21}$$

In our case, to obtain the first-order approximation, the function of  $W_1(\tau)$  can be expressed as

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$$L[W_1(t)] = h\hbar(t)N[\phi(t;q)]|_{q=0}$$
(12.22)

$$W_1(0) = 0$$
,  $\frac{dW_1(0)}{dt} = 0$  (12.23)

Assuming  $\hbar_1 = -1$ , h(t) = 1 and after substituting Eq. (12.21) in Eq. (12.22), one would get:

$$\omega_0^2(\ddot{W}_1 + W_1) = W_{\max}\cos(\tau)(\omega_0^2 - \alpha - \frac{3}{4}\beta W_{\max}^2) - \frac{\beta W_{\max}^3}{4}\cos(3\tau)$$
(12.24)

$$W_1(0) = 0 , \dot{W}_1(0) = 0$$
 (12.25)

1001 Eliminating the secular term, we have:

$$\omega_0 = \sqrt{\alpha + \frac{3}{4}\beta W_{\max}^2} \tag{12.26}$$

<sup>1002</sup> The same result was obtained in the first example of section 2.

Solving Eqs. (12.24) and (12.25), the  $W_1(\tau)$  is obtained as follows:

$$W_1(\tau) = -\frac{1}{32\omega_0^2} \beta W_{\max}^3(\cos(\tau) - \cos(3\tau))$$
(12.27)

1004 Thus the first-order approximation of the  $W(\tau)$  yields to:

$$W(\tau) = W_0(\tau) + W_1(\tau)$$
(12.28)

1005 In which:

$$\tau = \omega t , \ \omega = \omega_0 \tag{12.29}$$

## 1006 13 CONCLUSIONS

It has reviewed new asymptotic methodologies throughout numerous examples. The analytical
solutions yield a thoughtful and insightful understanding of the effect of system parameters
and initial conditions. Also, Analytical solutions give a reference frame for the verification and
validation of other numerical approaches.

Variational Iteration Method (VIM),Homotopy Perturbation Method (HPM), Energy Balance Method (EBM),Parameter-Expansion Method (PEM),Variational Approach (VA),Improved Amplitude Frequency Formulation (IAFF),Max-Min Approach (MMA),Hamiltonian Approach (HA) and Homotopy Analysis Method (HAM) are suitable not only for weak nonlinear problems, but also for strong nonlinear problems as it is indicated in this review. The most significant feature of those methods is their excellent accuracy for the whole range of oscillation

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amplitude values. Also, it can be used to solve other conservative truly nonlinear oscillators 1017 with complex nonlinearities. The solutions are quickly convergent and its components can be 1018 simply calculated. Also, compared to other analytical methods, it can be observed that the 1019 results of those methods require smaller computational effort and only the one iteration leads 1020 to accurate solutions. The successful implementations of the mentioned methods for the large 1021 amplitude nonlinear oscillation problem were considered in this review. All reviewed methods 1022 can be applied to various kinds of weak and strong nonlinear problems, and the examples 1023 studied in this review can be utilized as paradigms for oscillator problems. Through nonlinear 1024 oscillators, all the reviewed methods yield high accurate approximate periods which indicated 1025 above. 1026

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