Characterization of Plasma-deposited a-C:H:Si:F:N Films

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Thin a-C:H:Si:F:N films were studied as a function of the partial pressure of SF₆ in plasma feed, R_{sF^3} together with tetramethylsilane and N₂. Deposition rates varied from ~4 to ~19 nm.min⁻¹. Surface roughnesses were typically less than 35 nm. Surface contact angles with water droplets, measured using goniometry, were all around 90°. Scanning electron micrography revealed surface particles, probably formed in the gas phase, of typical diameters ~8 µm. As revealed by Fourier transform infrared spectroscopy and energy dispersive x-ray spectroscopy, the films are plasma polymers with a carbon and silicon network. Most of the films contain ~ 60 at.% C, ~ 10 at.% Si, 20 at.% O and ~5 to 14 at.% N. Film doping with F rises to ~2 at.% as R_{sF} is increased. The Tauc gap, calculated from ultraviolet-visible near infrared spectroscopic data, is controllable in the range of ~3.5 to 4.1 eV by a suitable choice of R_{sF} . Fluorination causes the films to be softer and less stiff. Total deformation and stored energies are reduced compared to those of the film deposited at $R_{sF} = 0\%$. The modulus of dissipation increases from ~8% to a maximum of ~65% for the fluorinated films.

Keywords: PECVD, a-C:H:Si:F:N, thin films, optical properties.

1. Introduction

Diverse amorphous films containing some of the elements – C, H, Si, N and F – have been studied in recent decades. For example, amorphous hydrogenated carbon films also containing nitrogen and fluorine, designated a-C:H:N:F, were produced in a parallel-plate, capacitively coupled reactor by Liu et al.¹ from CH_4 -N₂-NF₃ mixtures. As the concentration of nitrogen and fluorine increases in the films the sp²/sp³ ratio increases at the expense of the hydrogen content. The resulting films showed improved thermal stability of their electrical conductivity. Additional studies by the same research group indicate that the Tauc gap decreases and the Urbach energy increases as film [N] and [F] increase, producing defect states within the gap².

Owing to their low dielectric constants, SiOF films find possible application as interlayer dielectrics³. Plasma enhanced chemical vapor deposition (PECVD) has been used to produce a-Si:N:F films from SiH₄, N₂, Ar and NF₃ mixtures⁴. The refractive index of the films fell from about 2.2 to 1.6, while the gap increased from roughly 2.2 to 5.7 eV as the NF₃ flow rate was increased from 0 to 2 sccm. Despite its absence from the reactor feed, oxygen was incorporated into the deposited material. Film density fell as the NF₃ flow rate increased from 0.5 to 2 sccm.

Nanometric fluorinated silicon nitride films were produced at 350 °C in the down flow of an electron cyclotron resonance PECVD reactor fed NH₃-SiF₄ mixtures⁵. Such films, which exhibit extremely low leakage currents, may serve as gate dielectrics. Plasma immersion ion implantation and deposition (PIIID) has been used to deposit a-C:H:Si:O:F films from hexamethyldisiloxane (HMDSO)-SF₆-Ar mixtures⁶. The films showed hardnesses of \sim 1.5 GPa.

Despite such studies, there is little extant literature on a-C:H:Si:F:N films. In this study we characterize films deposited from cold plasmas fed tetramethylsilane (TMS)-SF₆-N₂ mixtures.

2. Materials and Methods

The deposition system is shown in Figure 1. Films were deposited in a cylindrical glass chamber, containing two circular, horizontal, parallel-plate electrodes. Radiofrequency (13.56 MHz) power was fed from a supply (TOKYO HY-POWER, MB-300) at 70 W to the lower electrode via a matching network, used to minimize the reflected power. The upper electrode was earthed. Pressure was monitored using a Pirani gauge (AGILENT, PCG-750). Nitrogen and sulfur hexafluoride gases (99.95% pure, WHITE MARTINS, Brazil) were admitted to the chamber from cylinders via precision leak valves (EDWARDS, LV10-K). For tetramethylsilane (TMS), vapor was introduced from a vial of the liquid reagent. For depositions, the chamber was evacuated continuously using a rotary vane pump (EDWARDS, E2M18). A TMS partial pressure of 96 mTorr was maintained for all depositions. The total pressure of nitrogen and sulfur hexafluoride was 24 mTorr. For all depositions, a time of 30 min was used. The stoichiometry of the films was altered by increasing the partial pressure of SF₆ in the feed, R_{sF} and decreasing that of nitrogen by the same amount.

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Figure 1. PECVD system.

Substrates, placed on the lower electrode, were of glass, polished stainless steel, and quartz. The glass substrates were used for films examined by Profilometry and Goniometry. Polished stainless-steel substrates were used for films examined by Infrared Reflection Absorption Spectroscopy (IRRAS), Scanning Electron Microscopy (SEM) and Energy-dispersive X-ray Spectrometry (EDS). Quartz substrates were employed for films examined by Ultraviolet-visible Near Infrared Spectroscopy (UVS) and nanoindentation.

Film deposition rates were calculated using Equation 1, where R is the deposition rate, h is the film thickness and t the deposition time.

$$R = h/t \tag{1}$$

Film thickness was measured from a film deposited onto a glass slide partially covered by an adhesive tape. Subsequent removal of the tape produced a well-defined film edge, which was measured using Profilometry (VEECO DekTak 150). Film surface roughness was calculated using the arithmetic method from film surface profiles. Surface morphology was examined using SEM (JEOL JSM-6010LA) and elemental analysis carried out using an EDS accessory (DRY SD Hyper (EX 94410T1L11)).

For Infrared Reflection Absorption Spectroscopy (IRRAS) a JASCO FTIR-410 spectrometer operating over the wavenumber range from 400 to 4000 cm⁻¹ was used. A resolution of 4 cm⁻¹ was achieved. Each spectrum was obtained using 128 scans.

From film thickness measurements and transmission UVS spectra obtained with a PERKIN ELMER LAMBDA 750, refractive indices and optical gaps were calculated using procedures described in detail elsewhere^{7,8}. Surface contact angles were measured on drops of distilled deionized water and diiodomethane using a KRÜSS DSA25E Goniometer. For each of three drops placed at different positions on the film, ten measurements were taken. The hardness, elastic modulus, and stiffness of the deposited material were calculated from force-depth plots obtained using a HYSITRON Triboindenter⁹. A normal force was applied to a pyramidal Berkovich diamond tip in the range 150 to 3000 μ N. Twenty indentations at each of at least 10 points were made. The three mechanical properties were calculated using the method developed by Oliver and Pharr¹⁰. Mean values and standard deviations of the hardnesses obtained at 15% of the film thickness are presented.

3. Results and Discussion

Figure 2 shows the deposition rate as a function of the partial pressure of sulfur hexafluoride in the feed, R_{SF} . Film thicknesses are given in the figure caption. The rise and subsequent fall in R as a function of R_{SF} is typical of systems in which the fluorine or fluorine-containing component of the chamber feed is increased. Initially, the fluorine released in the plasma causes extensive fragmentation of the monomer producing film precursors such as CH_x and CF_x as well as volatile HF, but at greater R_{SF} etching begins to dominate and the deposition rate falls. Hydrocarbon polymers are readily etched in oxygen-containing plasmas via reactions such as that shown in Equation 2:

$$C_x H_y(s) + O_2(g) \to CO(g) + H_2O(g) \tag{2}$$

Polymers containing Si, however, are more readily etched in fluorine/oxygen plasmas, such as CF_4/O_2 or SF_6/O_2^{11} . Etching of polymers containing C and Si is likely via reactions (3) to (5), with the overall reaction being summarized by Equation 6.

$$Si + mF \rightarrow SiF_m, m = 1 \text{ to } 4$$
 (3)

$$C + mF \to CF_m \tag{4}$$

$$C + nO \to CO_n, n = 1 \text{ to } 2 \tag{5}$$

 $2SiC + 3mF + nO \rightarrow 2SiF_m + CO_n + CF_m \tag{6}$

These reactions are given by Yih et al.² for etching of SiC. In the present case the plasmas are depositing and causing etching. Although not deliberately introduced into the reactor feed, some residual oxygen is present. Silicon, hydrogen, and nitrogen are present in the chamber feed. Fluorine is present in the plasmas for which R_{sF} is not zero.

Post-deposition reactions between free radicals trapped in the film and ambient oxygen and water vapor are known to occur in plasma polymers^{13, 14}, thus attaching O and OH to the film surface. The initial base pressure also represents a possible source of oxygen for the plasma. In addition, despite extensive cleaning of the reactor before each deposition, degasification from the chamber walls is another possible source of oxygen.

Sulfur was not detected in the films by EDS. As SF_n (n = 1 to 6) species are present in the plasma, sulfur may be removed as volatile products, such as SOF and SO_2 , formed by reactions that occur in SF_6 plasmas¹⁵, and described in Equations 7 and 8.

$$SF_2 + O \rightarrow SOF + F$$
 (7)

$$SOF + O \rightarrow SO_2 + F$$
 (8)

An additional factor influencing the plasma conditions is that the electron energy distribution function and density depend on the components of the plasma feed. As revealed by optical emission spectroscopy, the species H, CH and CN are present in cold plasmas fed TMS-N₂-He-Ar¹⁶. It is well known that the presence of dangling bonds on the film surface probably enhances the sticking probability of carbon-containing radicals. Plasma F radicals in plasmas containing fluorine remove hydrogen, leaving dangling bonds, while CF_x radicals contribute to film growth.

Figure 3 shows the surface roughness as a function of R_{sF} . There is no systematic variation, but all the roughnesses have small absolute values, being less than 40 nm. Roughnesses of about 5 to 80 nm were observed for PECVD films produced from HMDSO-SF₆-Ar mixtures⁶.

The surface contact angle, θ , of all the films, shown as a function of R_{sF} in Figure 4, is fairly uniform, remaining close to 90°, i.e. close to the region defining hydrophobic surfaces. Although θ is not a strong function of R_{sF} it shows increases and decreases that match the behavior of the roughness (Figure 3). Therefore, despite the expected structural and compositional changes in the films as R_{sF} increases, together with modification of the surface roughness, all of which can influence θ , little net change in θ is produced. The water surface contact angle of all the films is greater (~100°) than that of glass (~60°). For hydrophobic material, greater fluorine content is expected to produce greater values of θ . As shown below, however, the films are only doped with fluorine to a maximum of about 2 at.%; therefore [F] does not greatly influence θ .

Total surface energy calculated from the contact angles of drops of distilled deionized water and diiodomethane are shown, together with the dispersive and polar components, as a function of R_{sF} in Figure 5. The surface energy of glass is greater than that of the films. Non-zero values of R_{sF} lead to lower polar but greater dispersive components.

Figure 6 shows scanning electron micrographs of films deposited at different R_{sr} . Each pair of micrographs (a, b) etc. shows a micrograph and at 2500X and at a suitable greater magnification to reveal details of a particle on the



Figure 2. Deposition rate as a function of R_{sF} . Film thicknesses (nm) for films at increasing values of R_{sF} : 245, 358, 564, 265, 163, 141.



Figure 3. Surface roughness as a function of R_{SF}.



Figure 4. Contact angle as a function of R_{SF}



Figure 5. Total surface energy, polar, and dispersive components as a function of $R_{\rm sr}{\rm \cdot}$



- (j) 4.8 mTorr SF₆ (EDS)
- (k) 6.0 mTorr SF₆

(I) 6.0 mTorr SF₆ (EDS)

Figure 6. Scanning electron micrographs in pairs, at 2500X and at a suitable greater magnification to show details of surface particles. The micrographs were obtained for depositions at different R_{sF} : (a, b) $R_{sF} = 0$ mTorr; (c, d) $R_{sF} = 1.2$ mTorr; (e, f) $R_{sF} = 2.4$ mTorr; (g, h) $R_{sF} = 3.6$ mTorr; (i, j) $R_{sF} = 4.8$ mTorr; (k, l) $R_{sF} = 6.0$ mTorr. In the second micrograph of each pair, the position at which the EDS analysis was undertaken is marked.

surface. The particles are roughly spherical, with diameters of about 8 μ m, others exhibit more complex geometries. Such particles are probably formed in the gas phase as discussed later, together with the results of the EDS analyses.

Figure 7 shows transmission IRRAS of films grown at different R_{SH} in the 400 to 4000 cm⁻¹ range. There is evidence of the presence of hydroxyl groups as indicated by the absorption at ~3310 cm⁻¹ in all the spectra, these being especially prominent for the film grown at 2.4 mTorr of SF₆. Each film contains CH₃ groups as revealed by the absorptions at ~2960 and 2870 cm⁻¹ attributed to sp³ CH₃ asymmetric vibrations and sp³ symmetric vibrations, respectively. These groups exist in the original TMS molecules, each of which contains four methyl groups. An absorption caused by Si-CH₃ at around 1260 cm⁻¹, visible in all the spectra, may also be readily formed by fragmentation of TMS molecules. The prominent absorption at around 1040 cm⁻¹ may be attributed to Si-O-Si, Si-O-C and Si-CH₂-Si structures.



Figure 7. IRRAS spectra off the films deposited at different R_{sr}

As the absorptions of these three groups fall closely in the same region, it is difficult to distinguish between them. The presence of Si-O-Si and Si-O-C, however, is supported by the small absorption around 460 cm⁻¹ observed in the spectra of all the films. As mentioned above, oxygen is usually present in plasma polymers even when no oxygen is deliberately introduced into the plasma feed. No absorptions caused by fluorinated or nitrogenated functionalities are evident in any of the spectra.

Figures 8 (a, b) show the elemental concentrations, [C], [O] and [Si], and [N] and [F], respectively, in the films as a function of R_{sF} as determined using EDS. Inspection of Fig. 8a reveals that the carbon content increases about 50% and the silicon content more than doubles as R_{sF} increases; thus the silicon content increases more relative to the carbon content. In the absence of SF₆ from the feed, there is negligible incorporation of oxygen. For non-zero R_{sF} , however, ~20 at. % oxygen is found in all the films. Thus the presence of fluorine in the plasma possibly promotes the incorporation of oxygen radicals into the growing film.

Figure 8b reveals that the nitrogen content varies between about 5 and 13 at.% as R_{sF} is varied. As R_{sF} increases, the partial pressure of nitrogen decreases, but only by a maximum of 6 mTorr. Thus [N] is reduced compared to that observed at R_{sF} of zero, but the decline is not monotonic. Indeed, after an initial fall, [N] increases beyond an R_{sF} of 2.4 mTorr. The minimum in [N] corresponds to the maximum deposition rate (Figure 2) at an R_{sF} of 2.4 mTorr.

Figure 8c shows [C], [O] and [Si] in the surface particles observed by SEM at different R_{SF} . Figure 8d shows [N] and [F] for the same particles. From Fig. 8c, the composition of the particles at $R_{SF} = 0\%$ is distinct, consisting almost entirely of C and O (and H). Thus in TMS-N₂ plasmas, there is strong oxygen incorporation, probably in the gas phase, since the particles have distinct compositions from the bulk of the film, together with deposition via CH_x precursors. The



Figure 8(a). Film [C], [O] and [Si], measured using EDS, as a function of R_{sF} . (b) Film [N] and [F], measured using EDS, as a function of R_{sF} . (c) Surface particle [C], [O] and [Si], measured using EDS for different R_{sF} . (d) Surface particle [N] and [F], measured using EDS for different R_{sF} .

particles deposited at non-zero R_{SF} , contain more C, Si, N and F, but less than half the [O] of the unfluorinated film.

The presence of SF₆ in the chamber feed leads to a doping of the film with F of up to about 2 at.%. Over the interval studied, [F] rises roughly linearly with increasing R_{SF} , i.e. with increasing supply of SF₆ to the chamber.

Figure 9 shows (where calculable) the refractive index as a function of R_{sF} . The fluorinated films exhibit lower values of n. This behavior is consistent with that observed for the refractive index of a-Si:N:F films deposited from SiH₄-N₂-Ar mixtures⁴.

The Tauc gap and that defined as the energy corresponding to an absorption of 10^4 cm⁻¹, which has also been used to characterize the gap of amorphous materials¹⁷, are shown in Figure 10 as a function of R_{SF}. For semiconductors the bandgap is the difference in energy between the valence and conduction bands, and indicates the range of forbidden energy values for electrons. The band gap calculated, in this case, according to the Tauc model by extrapolating the linear portion of $(\alpha E)^{1/2}$ versus E plots (where α is the absorption coefficient and E the photon energy) to its intersection with the x-axis (i.e. the axis showing E), is designated the Tauc gap. Although the absolute values of the gap differ slightly, the trends observed as a function of R_{sF} are very similar. The unfluorinated film has a gap of ~3.9 eV. Both greater and smaller gap values can be obtained by the choice of R_{sF} . Comparison of the behavior of film [N] (Figure 8b) and the optical gap (Figure 10) suggests that nitrogen introduces states into the gap, with greater film [N] tending to yield lower gaps. Together with the effect of nitrogen, doping with F increases steadily with R_{sF} tending to reduce the gap. Thus at high R_{sF} both effects combine, leading to the lowest gaps.

A typical plot of $\ln(\alpha(E))$ as a function of photon energy, E, used to calculate the Urbach energy, U_E (in this case of the film deposited at $R_{SF} = 0$) is shown in Figure 11. The parameter U_E reflects the degree of absorption edge spreading caused by structural disorder, which forms localized states within the band tails of electronic states. Figure 12 shows U_E as a function of the Tauc gap. The dependence of U_E on the gap has roughly the shape expected for a semiconductor, with U_E for a gap energy of 3.5 eV being lower than expected.

The hardness, elastic modulus and stiffness of the film material calculated from nanoindentation measurements are shown as a function of R_{sr} in Figures 13-15, respectively. All three properties are significantly lower for the fluorinated films.



Figure 9. Refractive index of the films as a function of R_{set}



Figure 10. The Tauc and E_{04} optical gaps as a function of R_{sF}



Figure 11. Example (of the unfluorinated film) of the graph allowing the calculation of the Urbach energy.



Figure 12. Urbach energy as a function of the Tauc gap.

The hardnesses of the fluorinated films are very close to those observed in a-C:H:Si:O:F produced by Plasma Immersion Ion Implantation and Deposition of HMDSO-SF₆-Ar mixtures, namely 1.5 + -0.1 GPa⁶. A hardness similar to that of quartz



Figure 13. Hardness as a function of R_{sF}.



Figure 14. Young's modulus as a function of R_{SF}



Figure 15. Stiffness as a function of R_{SF}

is observed for the unfluorinated film. A strong fall in hardness upon the incorporation of fluorine has been observed in a-C:H:F films produced from CH_a - CF_a plasmas¹⁸.

The parameters H/E and H³/E² are displayed as a function of R_{sF} in Figure 16. Both parameters are greatly reduced in the fluorinated films since H falls by a factor of about eight when SF₆ is introduced into the chamber feed. The H/E values are indicative of ease of plastic deformation and therefore the observed fall in this parameter suggests low wear resistance for the fluorinated films. H³/E² is proportional to the load at which the material deforms plastically¹⁹. Materials with high plastic deformation may be useful in certain applications, such as those used in nanoindentation lithography²⁰.

Figure 17 shows the elastic recovery and plastic deformation energy as a function of $R_{\rm SF}$. Relatively high elastic recoveries (>90%) are observed for all the films. The plastic deformation energy tends to fall with increasing $R_{\rm SF}$. Total deformation energy, stored and dissipated energy as a function of $R_{\rm SF}$ are shown in Figure 18. Total deformation and stored energies are reduced at $R_{\rm SF}$ >0%. The dissipated energy is greater at non-zero $R_{\rm SF}$ and greatest at $R_{\rm SF}$ = 2.4 mTorr, which also gives an almost unchanged total deformation energy compared to that of the film deposited at $R_{\rm SF}$ = 0%. The dependence of the modulus of dissipation on $R_{\rm SF}$ is



Figure 16. H/E and H^3/E^2 as a function of R_{sF}



Figure 17. Elastic recovery and plastic deformation energy as a function of $R_{\rm sr}$



Figure 18. Total deformation, stored, and dissipated energy as a function of $R_{\rm sr^{\rm r}}$



Figure 19. Modulus of dissipation as a function of R_{sF}

depicted in Figure 19. All the fluorinated films ($R_{sF} > 0$) show moduli of dissipation of about 45 to 65%, compared to < 10% for the unfluorinated film.

4. Conclusions

Amorphous hydrogenated carbon films also containing silicon and nitrogen, and doped with fluorine were obtained by the PECVD of TMS-N₂-SF₆ mixtures. As revealed by IRRAS, EDS and SEM, the films were complex plasma polymers, with surface particles of distinct elemental composition.

A maximum deposition rate of ~18 nm.min⁻¹ was obtained as the partial pressure of SF₆, R_{sF} was varied. Film roughness was less than 40 nm for all the films. Independently of R_{sF} , surface contact angles were all about 90°. Tauc gaps could be selected between 3.4 and 4.4 eV by a suitable choice of R_{sF} . As demonstrated by nanoindentation, the fluorinated films are softer, less rigid and show greater plastic deformation than the unfluorinated film.

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Erratum: Characterization of Plasma-deposited a-C:H:Si:F:N Films

In the article "Characterization of Plasma-deposited a-C:H:Si:F:N Films", with DOI: https://doi.org/10.1590/1980-5373-MR-2021-0016, published in Materials Research, 24(suppl. 1):e20210016, on page 6, Figs. 11 and 12, should be as shown below:



Figure 11. Example (of the unfluorinated film) of the graph allowing the calculation of the Urbach energy.



Figure 12. Urbach energy as a function of the Tauc gap. The partial pressure of SF₆ used for each film deposition is given.