

Estimating uniaxial compressive strength, density and porosity of rocks from the p-wave velocity measurements *in-situ* and in the laboratory

<http://dx.doi.org/10.1590/0370-44672021740022>

André Cezar Zingano^{1,3}

<https://orcid.org/0000-0002-3740-9104>

Paulo Salvadoretto^{1,4}

<https://orcid.org/0000-0002-6608-4038>

Rafael Ubirajara Rocha^{2,5}

<https://orcid.org/0000-0003-2015-4982>

João Felipe Coimbra Leite Costa^{1,6}

<https://orcid.org/0000-0003-4375-370X>

¹Universidade Federal do Rio Grande do Sul – UFRGS, Departamento de Engenharia de Minas, Porto Alegre – Rio Grande do Sul - Brasil.

²Universidade Federal do Rio Grande do Sul – UFRGS, Laboratório de Pesquisa Mineral e Planejamento Mineiro, Porto Alegre - Rio Grande do Sul - Brasil.

E-mails: ³andrezin@ufrgs.br, andre.zingano@gmail.com,

⁴paulo.salvadoretto@ufrgs.br, ⁵rafaelubir@gmail.com,

⁶jfelipe@ufrgs.br

Abstract

Knowledge of the physical properties of rock masses is fundamental for the economics and safety of mining projects. The determination of these properties in rock samples in the laboratory requires time, expensive equipment and qualified personnel, which considerably increases the information's cost. Indirect methods were developed to obtain properties related to rock masses, which have been shown to be a viable alternative to traditional procedures. The determination of the compressional mechanical wave velocity (V_p) and subsequent correlation with lithological mechanical properties are indirectly obtained. This study's objective was to obtain correlations between V_p and the resistance to uniaxial compression, UCS (Unconfined Compressive Strength), as well as the density and porosity of the siltstone and sandstone lithologies present in the coalfield of Candiota, located in the southern region of Rio Grande do Sul, Brazil. The V_p records were obtained in laboratory samples, using ultrasonic velocity sensors, and *in-situ* by geophysical well logging (directly in boreholes). The results indicate the possibility of using V_p to determine the physical parameters of the investigated lithologies. In the specific case of the correlations between V_p and Unconfined Compressive Strength, determination coefficients R^2 above 0.70 were obtained, indicating sufficiently high reliability for using this information (e.g. in roof support projects). The correlation between V_p and density was also high.

keywords: sonic logs; p-wave velocity; uniaxial compression strength.

1. Introduction

The mechanical and physical properties of rocks are vitally important in the planning of open-pit or underground excavations and analysis of the stability of slopes, caves and other geological structures. The determination of these properties through the testing of rock samples is a time-consuming and costly activity, which requires accuracy in obtaining, prepar-

ing, and testing the samples. Thus, there is a need for simple and reliable, indirect techniques to determine the mechanical and physical properties of rocks.

Determination of P-wave velocity (V_p) is an easily applied, non-destructive technique that has increased in its use in geotechnical engineering and can be used to determine geomechanical parameters,

either *in-situ* or in the laboratory. The P-wave velocity is strongly related to intact rock properties, in addition to its structure and texture. Among the parameters that influence P wave velocity are elastic modulus, density, porosity, shape, anisotropy, presence of water, confining pressure, temperature, and discontinuities.

Several studies present the principles

and applications of determining the P-wave velocity in the laboratory using ultrasonic transducers (source and sensors) for measuring V_p in rock samples, generally derived from sounding cores. Kahraman (2001) evaluated the correlations between uniaxial compressive strength (UCS) and other rock strength indicators with the P-wave velocity. Kahraman (2002) estimated the P-wave velocity in intact rock from indirect measurements in the laboratory. Khandelwal and Singh (2009) correlated V_p with different physical-mechanical properties (e.g. UCS, porosity, density) of the rocks present in coal deposits (coals, shales and sandstones). Khandelwal and Ranjith (2010) obtained correlations of V_p with properties of different lithological types. Kurtulus *et al.* (2012) studied the physical and mechanical properties of ultra-basic serpentinite rocks in Turkey. Fener (2011) studied the effect of the sample size of compact rocks of different types (sedimentary and igneous) and their influence on the measured values of V_p .

When it comes to determining the P-wave velocity directly in boreholes (i.e. *in-situ*), the sonic well logging technique (sonic log) is the resource to be used. Geophysical well logging is an indirect

method for obtaining petrophysical information in boreholes. Sensors inserted in the boreholes allow continuous determination of the physical properties of lithologies intercepted by them. Among the various types of well logging sensors available, the sonic log allows the recording of the P-wave velocity in the lithologies adjacent to the drill holes. A detailed description of this type of sensor, including its possible uses, can be seen in Hearst *et al.* (2000) and Ellis and Singer (2007). Specifically related to the use of sonic logs in carboniferous basins, they have routinely been used to estimate UCS in Australia's coal mines for roof support projects (McNally, 1987). Such estimates are obtained by measuring V_p in boreholes, which are correlated with UCS measured in rock samples from the same holes. The original study by McNally (1987) used sonic log data from 16 mines in Australia's coal deposits. Currently, most Australian mines have specific correlations (Zhou, 2001). The V_p can also be obtained in diamond drilling holes or in destructive drilling. In current practice, the extraction of cores has been reduced after the development of correlations. Examples of similar studies in North America are seen in Wade (1997),

Oyler *et al.* (2010), Karacan (2009a, b). In the latter, the use of full-wave probes is demonstrated, allowing the estimation of dynamic modulus (Young, Shear, Poisson, and Bulk) of the considered lithologies, depending on the determination of the S-wave velocity.

Within this context, the present study uses the determination of V_p in laboratory samples and by *in-situ* sonic logging in the rocks present in carboniferous basins (in this case, siltstones and sandstones), correlating these measurements with mechanical and physical properties of the lithologies (uniaxial compressive strength, density, and porosity). This study investigates how UCS versus V_p regressions obtained by sonic logging (similar to those reported by McNally, 1987) can be established in carboniferous basins in Brazil, with a coefficient greater than or equal to 0.70, which is considered acceptable from the point of view of international practice.

The V_p was correlated with UCS for sandstone and conglomerate rocks from copper and lead ore deposits (Freitas *et al.*, 2017). The species were prepared and the V_p and V_s were measured. The same species went to the frame machine for UCS tests.

2. Location of the study area

The present study was carried out at the Seival coalfield, located in Candiota,

Rio Grande do Sul State (Figure 1), in an area operated by Copelmi Mineração Ltda.

2.1 Geological setting

The Candiota deposit (in the geological context of the Seival Mine) is situated along the outcrop belt of the Paraná basin, located in the South American continent's central-eastern portion and distributed between Brazil, Uruguay, Paraguay, and Argentina. The

Paraná Basin is an intra-cratonic basin that developed under the continental crust (filled with sedimentary and volcanic rocks), dating from the Ordovician to the Cretaceous period.

The coal found in the region is attributed to the Rio Bonito Formation, which is

composed of river and marine sandstones, carbonaceous siltstones, and shales dating from the Lower Permian period. In the Seival deposit, there are 17 coal layers, with a more significant economic interest in the Candiota Superior, Banco Louco, and Candiota Inferior layers (Schneider *et al.*, 1974).

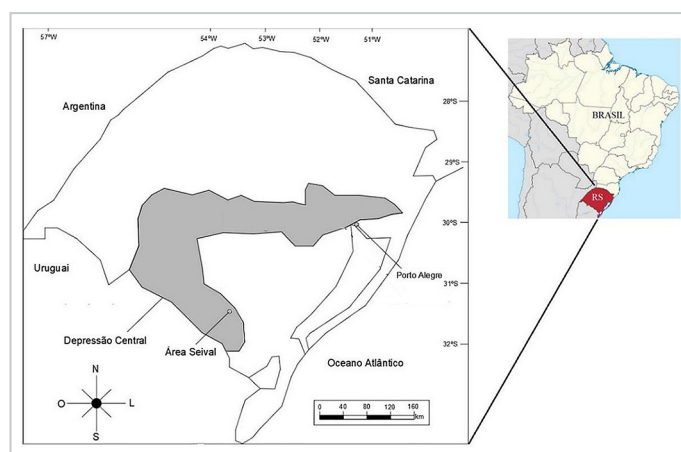


Figure 1 - Location map of the Seival Area, Candiota-RS.

3. Materials and methods

In this study, 46 samples of sandstones and siltstones were prepared. The rock specimens were obtained by diamond drilling (diameter NX), which generated samples of approximately

53.50 mm in diameter.

For determining the P-wave's ultrasonic velocity in laboratory samples (Figure 2), the Pundit PL 200 equipment (PROCEQ) was used. The acquisition of

sonic log data (Figure 3) was obtained with a SlimHole Fullwaveform Triple Sonic profiler (Robertson Geologging Ltd., UK). In the uniaxial compressive tests, a Control Advanced 9 hydraulic press was used.

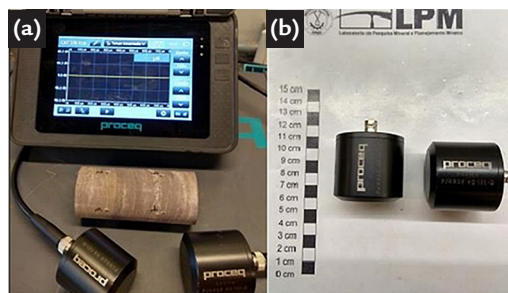


Figure 2 - (a) Pundit and transducers used in the V_p determination tests. (b) Detail of the 54 kHz frequency transducers used in data acquisition.

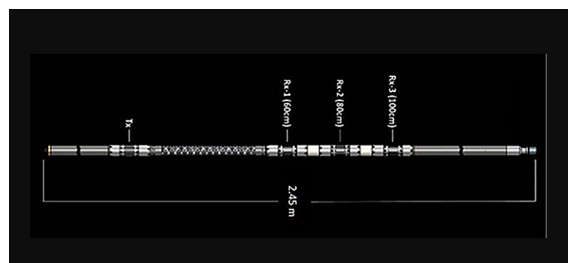


Figure 3 - Schematic diagram of the Slim-Hole Full Waveform Triple Sonic tool, showing the piezoelectric transducer positions (23 kHz) TX and RX1, RX2, RX3 (source and receivers, respectively). (Robertson Geologging Ltd., 2007).

3.1 Sample preparation

The drill cores were sawn to generate samples of the length required by the technical standard (ASTM, 2001). This

standard establishes an optimal relationship between the height and diameter of the specimen, 2.5 for cylindrical bodies.

It also establishes that the surfaces of the ends must not deviate perpendicularly by more than 0.25°.

3.2 Determination of V_p by sonic logging (V_{p_sonic})

The theoretical and practical aspects of using the sonic log are presented in Hearst *et al.* (2007) and Ellis and Singer (2007). The specific type of sonic profiling device used in this study is suitable for the mining industry, where boreholes are typically small in diameter (100 mm or smaller). It is a device with a transmitter and three receivers, which performs "non-compensated" readings of full waveforms recorded in each sensor, from a pulse of a few microseconds of duration and a frequency of 23 kHz, emitted by a piezoelectric transmitter. The mechanical waves from the transmitter propagate travel through the fluid and rocks adjacent to the device. They are registered in the sensors. The difference between wave ar-

rival times (transit) between two of these sensors is used to determine the velocity of the first compressional P-wave (V_p). Most sedimentary rocks have V_p velocities ranging from 2,000 to 7,000 m/s.

The sonic tool used here measured every centimetre along the borehole. However, it is essential to highlight the minimum vertical limit of detection, which in the specific case is 0.20 m, due to the distance between sensors in the equipment. In the present study, to obtain V_p , we used the difference in transit times of the acoustic wave verified in the RX2 and RX1 receivers. Thus, in sonic logging, the compressional wave transit time between two receivers represents an average of the rocks' behavior in the 0.20 m range.

Conversely, the samples used for UCS tests and ultrasonic tests are shorter (up to 135 mm). Even when the depths of the rock samples and the profiling records are perfectly correlated, the different sample supports produce dispersion in the correlations between UCS (or ultrasonic velocity) and V_p velocities obtained by the sonic log.

To obtain more representative measurements in this study, reducing the effects of the difference between vertical resolution of the sonic log and sample length (Oyler, 2010), we tried to analyse samples of homogeneous lithologies. In this case, the profiling readings were approximately constant and with thicknesses significantly more significant than the distance between the sonic tool's receivers.

3.3 Determination of V_p in laboratory samples (V_{p_Pundit})

For this test, the Pundit equipment was used, whose transducers (transmitter and receiver) are made of piezoelectric ceramic elements. The transducers operate

at 54 kHz and are capable of essentially generating compressional waves for measuring the compressional wave transit time.

The test was based on the interna-

tional standard (ASTM, 2008) and the transducers were positioned at the ends of the specimens. The transformation equation of the transit time to wave velocity V_p is:

$$V_p (\text{média}) = \frac{\Delta d}{\Delta t} \quad (1)$$

where Δd is the specimen's size, Δt is the transit time of the pulse in the specimen, and V_p is the P-wave velocity.

3.4 Determination of UCS

The uniaxial compression test (UCS) was performed using the standard ASTM (1995), which defines this test. Another standard (ASTM, 2001)

was used in sample preparation. A total of 42 specimens were prepared (by measuring and weighing) and then tested by the uniaxial compressive test,

performed on the Advanced 9 press. The test was carried out with a loading rate of 500 kN/s.

3.5 Determination of physical properties

The apparent densities and porosities of the samples were determined according to the Brazilian technical

standard ABNT (2010). It was not possible to apply this methodology to all samples, since this method presents a

stage in which the samples are immersed in water and some of them had degraded due to contact with fluid.

4. Results and discussion

The correlations obtained in this study involved wave velocities V_p (deter-

mined by sonic profiling and Pundit) and physical-mechanical properties (UCS

resistances, porosity, density) of sandstones and siltstones in the area of interest.

4.1 Correlation between V_p Sonic and V_p Pundit

Comparisons were made between the speeds of the sonic waves obtained through different tests. Since the dimensions of the samples used in the tests are different (the volume of rock involved in the measurement of V_p sonic is more significant than in V_p pundit), different values for V_p were also expected. A comparison was made of the average velocity for V_p Sonic for each sample (in the range of 200 mm vertical resolution of the sonic

profiling) with the V_p determined by Pundit (maximum sample length equal to 135 mm). Figure 4 shows this comparison; there was a tendency for ultrasonic velocity (V_p Pundit) to show the highest values. It is not the objective of this work to study these differences more deeply. However, among the factors that can explain these differences, it should be noted that: (a) as the volume of rock is different in each V_p measurement technique, the V_p sonic ve-

locity can be more affected by the presence of small fractures in the in-situ rock; (b) the frequency of the compressional wave generated in each measurement technique is different and the literature informs us that pulses with different frequencies also present a V_p that is different in solids (see Philippidis; 2005, for example); (c) the diameter of the specimens has an influence on the compressional velocity V_p Pundit (as shown in Fener; 2011, for example).

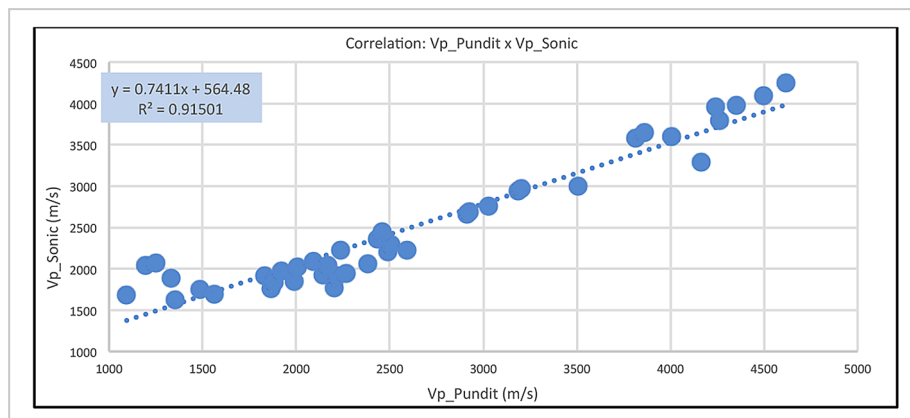


Figure 4 - Graph of the correlation between V_p Pundit and V_p Sonic for the set of samples used in the study.

4.2 UCS versus V_p sonic

Historically, correlations between UCS and V_p determined by sonic logs in coal deposits use the relationship

described in McNally (1987) and are presented in Equation (2), where a negative exponential function is used to model

the correlation between UCS and V_p . In Equation (2), t is the P-wave transit time (in $\mu\text{s}/\text{ft}$) and UCS is in psi.

$$\text{UCS} = 143000 e^{(-0.0035t)} \quad (2)$$

The present study preferred to use the $\text{UCS} = A \exp(B * V_p)$ ratio, where $V_p = 1/t$. The above equation is not the same as that used by McNally (1987). However, it describes UCS behaviour well,

concerning V_p obtained by sonic logging. It is also frequently used to model the correlations between UCS and the ultrasonic P-wave velocity of laboratory samples.

Figure 5 shows the correlation

between V_p obtained by sonic logging (V_p sonic) and UCS, expressed by Equation (3), not considering lithological distinction, using the exponential relation suggested above. The determination

coefficient obtained was $R^2 = 0.73$.

$$UCS = 3.9273 e^{(0.0008 Vp_sonic)} \quad (3)$$

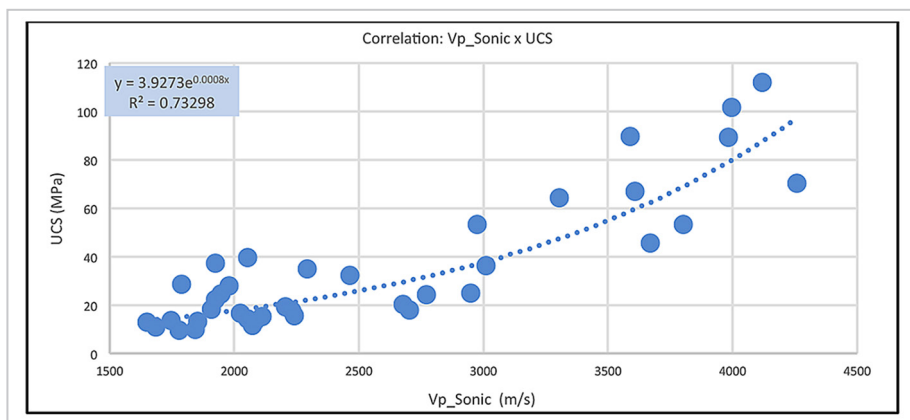


Figure 5 - Graph of general correlation between Vp_Sonic and UCS; it does not individualize the lithologies present.

Figure 6 shows the correlation Vp_Sonic versus UCS, but there is individualization of the lithologies present (sandstones and siltstones). For sandstones, the coefficient of determination was $R^2 = 0.88$, while the siltstone showed $R^2 = 0.40$. In this case, it appears that there is different behaviour between the two lithologies, which can be captured by individualized regressions. The sandstone itself presents different behaviour con-

cerning the higher values of Vp velocities. According to the geological description of cores, Vp values above 3,000 m/s were associated with cemented sandstones.

In siltstone, a lesser dispersion in UCS values (approximately 10 to 40 MPa), while sandstone assumes a greater range of values (10 to 115 MPa). On the other hand, siltstones have lower Vp , on average (below 3,000 m/s), while sandstones show a broader range of velocities

(between 2,000 m/s and 4,300 m/s). The low siltstone velocities can be justified by the high concentration of clay in their composition, which has a lower sonic velocity.

For the results mentioned above, it is advisable that individualized correlations are used whenever the lithological types are known. Individual correlation will allow an estimate of UCS from Vp with less error.

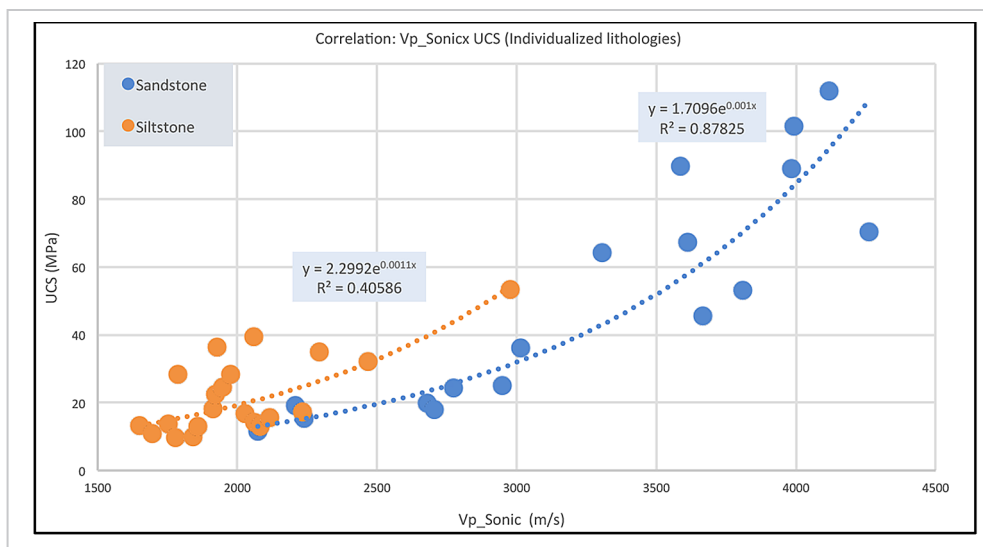


Figure 6 - Graph of correlation between Vp_Sonic and UCS, individualizing the lithologies present (sandstone and siltstone).

4.3 UCS versus Vp_Pundit

The general correlation (without individualization of lithologies) between Vp_Pundit and UCS (Figure 7) presents a determination index $R^2 = 0.74$. This is a reasonable value that exceeds the mini-

mum practical limit of 0.70.

After calculating the general correlation index, the samples were separated by lithology. The sandstone samples showed $R^2 = 0.89$, while the siltstone samples

showed $R^2 = 0.55$ (Figure 8). Again, the siltstone and sandstone samples behaved differently about Vp . Equations (4) and (5) are then obtained, respectively, with sandstones showing the best correlation.

$$UCS = 1.4811 e^{(0.0009 Vp_Pundit)} \quad (4)$$

$$UCS = 4.9617 e^{(0.0007 Vp_Pundit)} \quad (5)$$

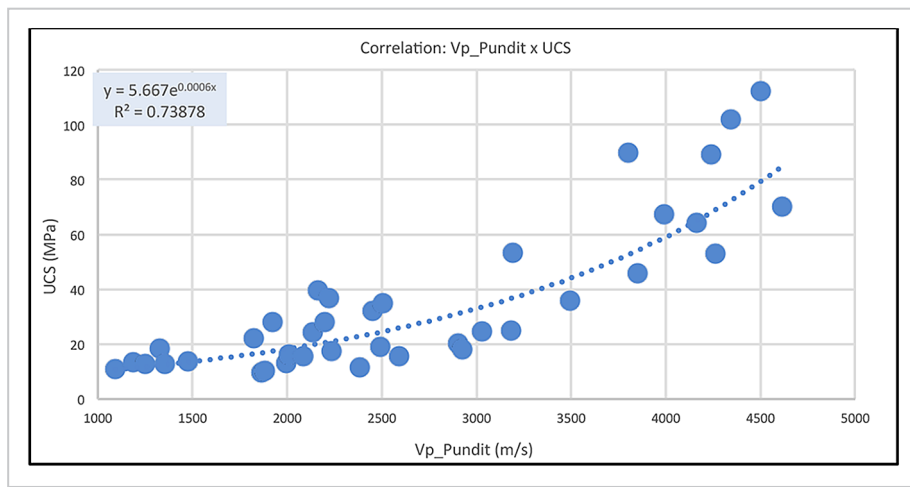


Figure 7 - General correlation graph between Vp_Pundit and UCS, not individualizing the lithologies present.

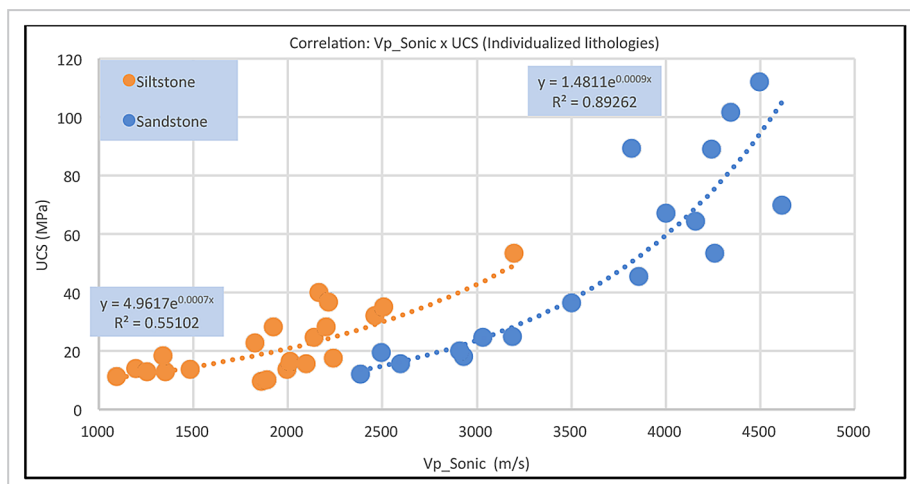


Figure 8 - Graph of correlation between Vp_Pundit and UCS, individualizing the lithologies present.

4.4 Vp from sonic logging versus Density

The relationship between Vp_Sonic and density, in this study, is consistent with the lithologies that address the subject. This relationship is generally increasing and linear. The density increases when the wave velocity increases, according to Figure 9, where

we perceive this correspondence.

By separating the results from each lithology, it can be seen that the degree of weathering of the sandstone samples has a direct link with density and sonic wave velocity. Figure 10 illustrates this situation, dividing the samples into silt-

stone, sandstone (with varying degrees of weathering) and sound sandstone.

The specific case of siltstone showed a different behaviour from sandstones, with an approximately constant density for all samples, without dependence on Vp .

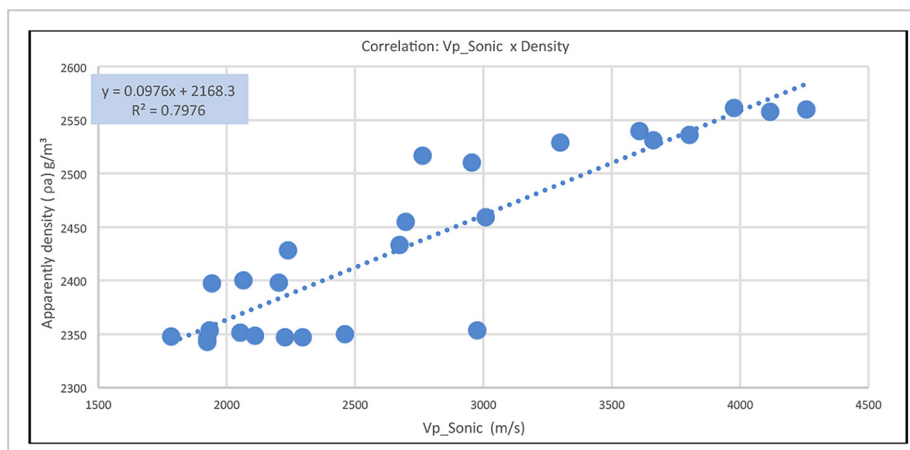


Figure 9 - Graph of correlation between Vp_Sonic and Density; it does not individualize the lithologies present.

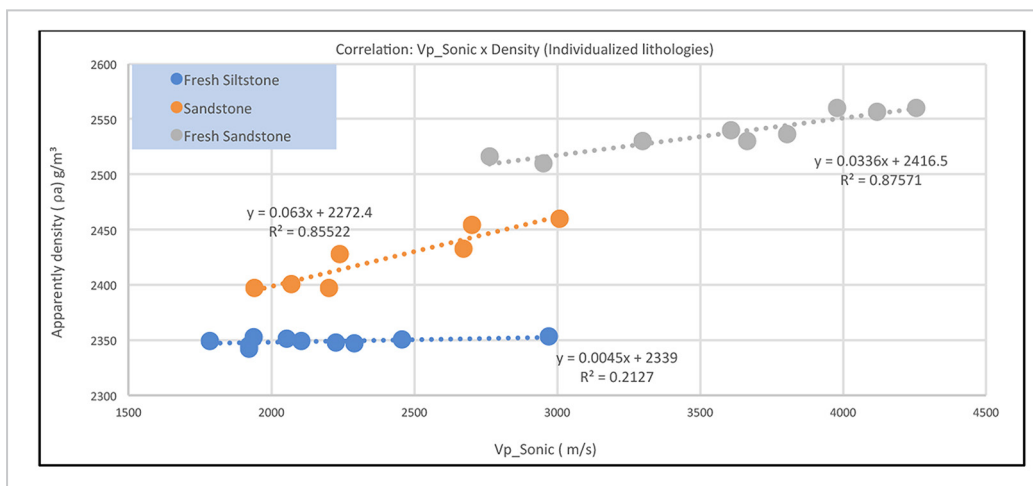


Figure 10 - Graph of correlation between Vp_Sonic and Density, individualizing the lithologies present.

4.5 Vp_Pundit versus Density

The responses of the correlation between Vp_Pundit and density were similar to those observed in sonic logging. This similarity between the responses provides reliability to the

results. Figure 11 shows the correlation graph Vp_Pundit versus Density.

Figure 12 illustrates the distribution of the samples according to the lithology and the degree of weathering. Once again,

this differentiation is very prominent. This duplicity of results reinforces the relationship between mineralogical constituents (lithology) and the degree of weathering with the sonic wave velocity.

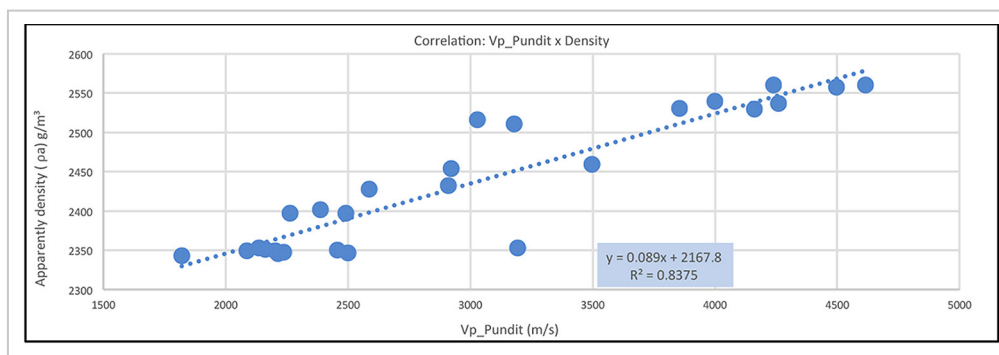


Figure 11 - General linear correlation graph between Vp_Pundit and Density, not individualizing the lithologies present.

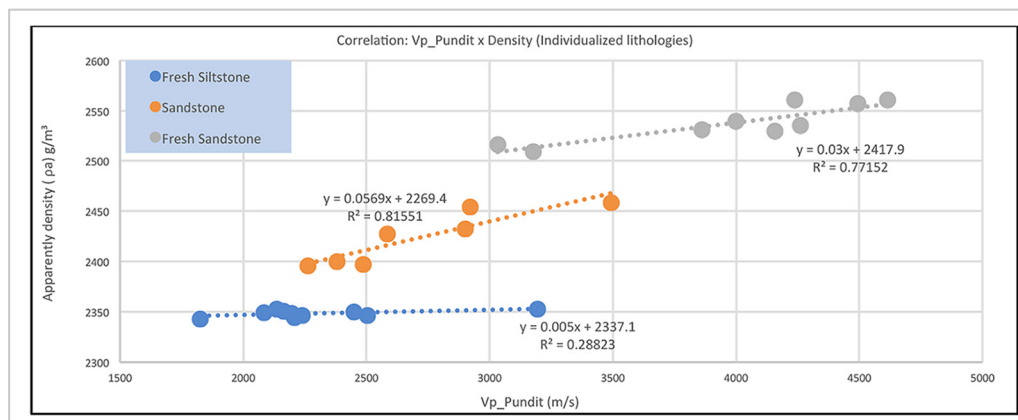


Figure 12 - Graph of correlation between Vp_Pundit and Density, individualizing the lithologies present.

4.6 Correlation between Vp and Porosity

The results obtained for the correlation between P-wave velocity and porosity show that these parameters behave in an

inversely proportional way. A high degree of linear correlation (for example, above $R^2 = 0.70$) was not obtained in both

methods. Similar results were obtained (low correlations) with individualized and non-individualized lithologies.

5. Conclusions

This study confirmed the usefulness of indirect methods (sonic logging and

ultrasonic P-wave velocity) to determine physical and mechanical parameters,

such as UCS, density and porosity, in the lithologies present in a coal deposit.

No coal samples were tested due to their unavailability. The possibility of estimating UCS (uniaxial compressive strength) from P-wave velocity is highlighted, with a high coefficient of determination (R^2 close to 0.90) for sandstones, using the

two indirect methods investigated.

The practical aspects of using geophysical profiling are emphasised, which dispenses sample preparation in the laboratory to determine the lithologies' V_p velocity. Denser, more competent, and

less porous rocks had a shorter P-wave transit time and, therefore, high V_p . The reverse occurred with less dense, less competent, and more porous massifs (possibly more weathered), presenting a smaller V_p .

References

- AMERICAN SOCIETY FOR TESTING AND MATERIALS. *ASTM. D4543-01*: Standard practices for preparing rock core specimens and determining dimensional and shape tolerances. West Conshohoken, PA: ASTM International, 2001.
- AMERICAN SOCIETY FOR TESTING AND MATERIALS. *ASTM. D2845-08*: Standard test method for laboratory determination of pulse velocities and ultrasonic elastic constants of rock (withdrawn 2017). West Conshohoken, PA: ASTM International, 2008.
- AMERICAN SOCIETY FOR TESTING AND MATERIALS. *ASTM. D2938-95 (2002)*: Standard test method for unconfined compressive strength of intact rock core specimens (withdrawn 2005). West Conshohoken, PA: ASTM International, 1995.
- ASSOCIAÇÃO BRASILEIRA DE NORMAS TÉCNICAS. *ABNT NBR 15845*: Rochas para revestimento – Métodos de ensaio. Rio de Janeiro: ABNT, 2010.
- ELLIS, V. D.; SINGER, M. J. *Well logging for earth scientists*. Dordrecht: Springer, 2007.
- FENER, M. The effect of rock sample dimension on the P-wave velocity. *Journal of Nondestructive Evaluation*, v.30, p.99–105, 2011.
- FREITAS, N. B. A., DANTAS, J. G. M., ZINGANO, A. C. Equação de correlação com ênfase na litologia para estimativa de resistência à compressão uniaxial através do uso de Pundit. In: SIMPÓSIO DE MINERAÇÃO, 18., 2017, São Paulo, Brazil. *Anais [...]*. São Paulo: ABM, 2017. p. 399-410.
- HEARST, R. J.; NELSON, H. P.; PAILLET, L. F. *Well logging for physical properties: a handbook for geophysicists, geologists and engineers*. 2nd ed. Chichester, New York: Wiley, 2000.
- KAHRAMAN, S. Evaluation of simple methods for assessing the uniaxial compressive strength of rock. *International Journal of Rock Mechanics and Mining Sciences*, v.38, p.981–94, 2001.
- KAHRAMAN, S. Estimating the direct P-wave velocity value of intact rock from indirect laboratory measurements. *International Journal of Rock Mechanics and Mining Science*, v.39, p.101–104, 2002.
- KHANDELWAL, M.; SINGH, T. N. Correlating static properties of coal measure rocks with P-wave velocity. *International Journal of Coal Geology*, v. 79, p. 55–60, 2009.
- KHANDELWAL, M.; RANJITH, P. G. Correlating index properties of rocks with P-wave measurements. *Journal of Applied Geophysics*, v. 71, p. 1–5, 2010.
- KARACAN, C. Ö. Elastic and shear moduli of coal measure rocks derived from basic well logs using fractal statistics and radial basis functions. *International Journal of Rock Mechanics and Mining Sciences*, v. 46, p. 1281–1295, 2009.
- KARACAN, C. Ö. Reservoir rock properties of coal measure strata of the Lower Monongahela Group, Greene County (Southwestern Pennsylvania), from methane control and production perspectives. *International Journal of Coal Geology*, v. 78, p. 47–64, 2009.
- KURTULUS, C.; BOZKURT, A.; ENDES, H. Physical and mechanical properties of serpentinized ultrabasic rocks in NW Turkey. *Pure and Applied Geophysics*, v. 169, p. 1205–1215, 2012.
- MCNALLY, G. H. Estimation of coal measure rock strength using sonic and neutron logs. *Geoexploration*, v. 24, p. 381–395, 1987.
- OYLER, D. C.; MARK, C.; MOLINDA, G. M. In situ estimation of roof rock strength using sonic logging. *International Journal of Coal Geology*, v. 83, p. 484–490, 2010.
- PHILIPPIDIS, T. P.; AGGELIS, D. G. Experimental study of wave dispersion and attenuation in concrete. *Ultrasonics*, v. 43, p. 584–595, 2005.
- ROBERTSON GEOLOGGING. *Full-Wave Triple Sonic sonde-operating and technical manual*. Deganwy, UK: Robertson Geologging, 2007.
- SCHNEIDER, R.; MÜHLMANN, H.; TOMMASI, E.; MEDEIROS, R. A.; DAEMON, R. F.; NOGUEIRA, A. A. Revisão estratigráfica da Bacia do Paraná. In: CONGRESSO BRASILEIRO DE GEOLOGIA, 28., 1974, Porto Alegre. *Anais [...]*. [S. l.]: Sociedade Brasileira de Geologia - SBG, 1974. p. 41–65.
- WADE, N. H.; HICKINBOTHAM, A. Geotechnical strength parameters from geophysical logs. *International Journal of Surface Mining, Reclamation and Environment*, v. 11, p. 27–32, 1997.
- ZHOU, B. *et al.* Automated geotechnical characterisation from geophysical logs: examples from Southern Colliery, Central Queensland. *Exploration Geophysics*, v. 32, p. 336–339, 2001.

Received: 26 April 2021 - Accepted: 9 July 2021.



All content of the journal, except where identified, is licensed under a Creative Commons attribution-type BY.